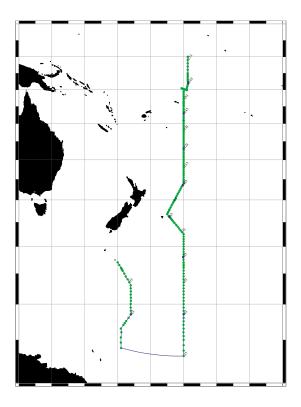
A. Cruise Narrative: P14S P15S



A.1. Highlights

WHP Cruise Summary Information

| WOCE section designation | P14S and P15S |
|--|--|
| Expedition designation (EXPOCODE) | 31DSCG96_1, 31DSCG96_2 |
| Chief Scientist(s) and their affiliation | John Bullister, NOAA-PMEL |
| Dates | Leg 1: 1996 JAN 05 - 1996 FEB 04 (Stns 1-93) |
| | Leg 2: 1996 FEB 12 - 1996 MAR 10 (Stns 94-182) |
| Ship | R/V DISCOVERER |
| Ports of call | Leg 1: Hobart, Tasmania- Wellington, NZ |
| | Leg 2: Wellington, NZ- Pago Pago Samoa |
| | 0°0.01' S |
| Geographic boundaries of the stations | 153°4.07' E 168°36.87' W |
| | 67°0.03′ S |
| Number of stations | 182 |
| Floats and drifters deployed | 14 ALACE floats deployed |
| Moorings deployed or recovered | none |
| Contributing Authors | John Bullister, Calvin Mordy |

WHP Cruise and Data Information

Instructions: Click on any item to locate primary reference(s) or use navigation tools above.

| Cruise Summary Information | Hydrographic Measurements |
|--|-----------------------------|
| | |
| Description of scientific program | CTD - general |
| | CTD - pressure |
| Geographic boundaries of the survey | CTD - temperature |
| Cruise track (figure) | CTD - conductivity/salinity |
| Description of stations | CTD - dissolved oxygen |
| Description of parameters sampled | |
| Bottle depth distributions (figure) | Salinity |
| Floats and drifters deployed | Oxygen |
| | Nutrients |
| | CFCs |
| Principal Investigators for all measurements | |
| Cruise Participants | |
| | |
| Problems and goals not achieved | CO2 system parameters |
| | Other parameters |
| | |
| Underway Data Information | |
| | |
| | References |
| Bathymetry | |
| Acoustic Doppler Current Profiler (ADCP) | DQE Reports |
| | · |
| | CTD |
| | S/O2/nutrients |
| Atmospheric chemistry data | CFCs |
| | |
| | |
| | Data Processing Notes |

Note: The following appendices are included with this file:

| APPENDIX 1 | CTD/Rosette Station Locations on P14S and P15S (CGC96) |
|--------------|---|
| APPENDIX 2 | ALACE Float Deployment Locations on P14S and P15S (CGC96) |
| APPENDIX 3 | CTD/O2 techniques on WOCE P14S and P15S (CGC96) |
| APPENDIX 4a | Oxygen Measurement techniques on WOCE P14S and P15S (CGC96) |
| APPENDIX 4b | Replicate Oxygen Measurements on WOCE P14S and P15S (CGC96) |
| APPENDIX 5 | Nutrient Measurement techniques on WOCE P14S and P15S (CGC96) |
| APPENDIX 6a | CFC-11 and CFC-12 Measurement techniques on WOCE P14S and P15S |
| APPENDIX 6b | CFC Air Measurements on P14S and P15S (interpolated to station locations) |
| APPENDIX 6c | Replicate CFC-11 measurements on P14S and P15S (CGC96) |
| APPENDIX 6d | Replicate CFC-12 measurements on P14S and P15S (CGC96) |
| APPENDIX 7 | Carbon Measurement techniques on P14S an P15S |
| APPENDIX 8 | Listing of Bottle problems |
| APPENDIX 9a | DQ Evaluation of WOCE P14S and P15S hydrographic data |
| APPENDIX 9b | Responses to WOCE DQE comments on .sea file |
| APPENDIX 10a | DQE Evaluation of CTD data for RV Discoverer Cruise (CGC96) |
| APPENDIX 10b | Response to DQE Evaluation of CTD data for RV Discoverer (CGC96) |
| APPENDIX 11 | Final CFC Data Quality Evaluation (DQE) Comments on P14SP15S |

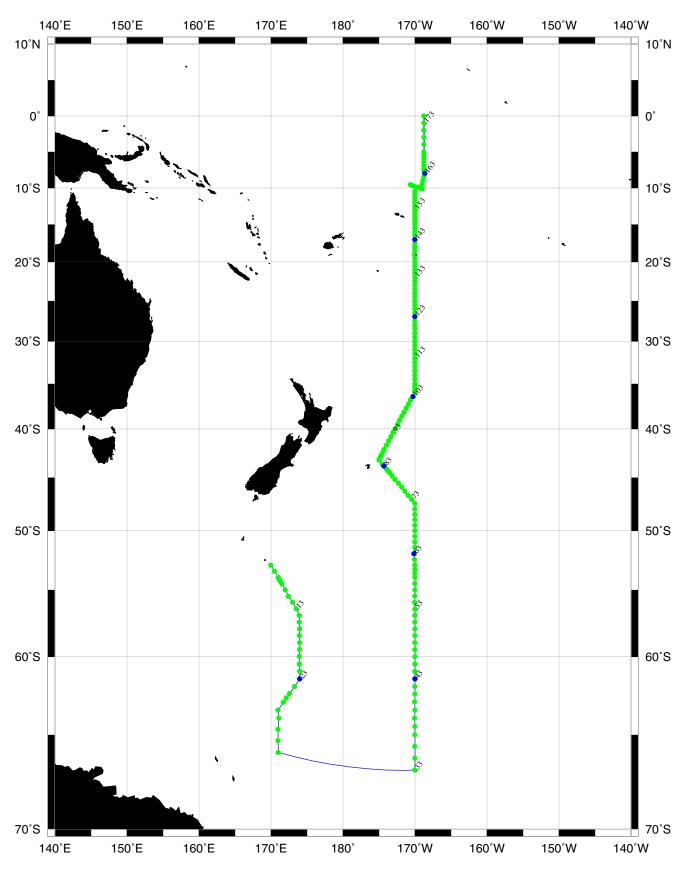
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All at:

National Oceanic and Atmospheric Administration
Pacific Marine Environmental Laboratory (NOAA-PMEL) 7600 Sand Point Way, NE Seattle, WA 98115 USA

Station locations for P14S



Produced from .sum file by WHPO-SIO

Cruise Track:

The station locations are shown in Fig. 1 and listed in Appendix 1 and in the P14SP15S.sum file.

182 Stations were completed:

- 3 test stations on the transit leg from Hobart to the start of the P14S section (2 thirty-six position rosette stations; 1 twenty-four position rosette station)
- 29 stations on the P14S section
 - (17 thirty-six position rosette stations; 12 twenty-four position rosette stations)
- 144 stations on the P15S section
 - (132 thirty-six position rosette stations; 10 twenty-four position rosette stations)
- 6 thirty-six position rosette stations in a short section across Samoa Passage
 One shallow primary productivity cast (with light meter) per day was made while on the P14S and P15S sections.

Approximately number of water samples analysed:

5700 salinity

5700 oxygen

5700 nutrients

3300 CFC-11 and CFC-12

1000 CFC-113 and carbon tetrachloride

3100 Total CO2

3000 pCO2

5700 pH

3100 Alkalinity

1350 DOC

Approximate number of water samples collected for shore-based analysis:

- 975 AMS carbon isotope samples (C-13 and C-14)
- 1025 DON

Floats:

14 ALACE floats were deployed (8 standard and 6 stretched profilers). The deployment locations are listed in Appendix 2.

ADCP:

Lowered ADCP profiles were obtained at about 70 stations on Leg 1 using a rosette mounted lowered ADCP instrument on 36 position rosette frame. Continous underway ADCP measurements were made along the cruise track.

Atmospheric chemistry data:

Air samples were collected at approximately 3 degrees intervals for analyses of atmospheric CFCs.

Participating Institutions:

| NOAA Pacific Marine Environmental Laboratory | (PMEL) |
|---|---------|
| NOAA Atlantic Oceanographic and Meteorological Laboratory | (AOML) |
| Bermuda Biological Station for Research | (BBSR) |
| Monterey Bay Aquarium Research Institute | (MBARI) |
| Scripps Institution of Oceanography | (SIO) |
| Oregon State University | (OSU) |
| Institute of Ocean Sciences | (IOS) |
| University of Tennessee | (UT) |
| University of Hawaii | (UH) |
| University of Miami | (UM) |
| University of South Florida | (USF) |
| University of Charleston, South Carolina | (UCSC) |
| University of Washington | (UW) |

Principal Investigators

| Measurements | Principal Investigators (PI) | Institution | Funding Agency |
|------------------------------|-------------------------------|-------------|-------------------|
| CTD/O2 and bottle salinity | Greg Johnson | PMEL | (NOAA) |
| Chlorofluorocarbons (CFCs) | John Bullister | PMEL | (NOAA) |
| Total CO2 (DIC), pCO2 | Dick Feely, Rik Wanninkhof | PMEL/AOML | (NOAA) |
| C-14 (AMS radiocarbon), C-13 | Paul Quay | UW | (NOAA) |
| Nutrients | Calvin Mordy, Zia-Zhong Zhang | PMEL/AOML | (NOAA) |
| Dissolved Oxygen (discrete) | John Bullister | PMEL | (NOAA) |
| Total Alkalinity | Frank Millero | UM | (NOAA) |
| рН | Robert Byrne | USF | (NOAA) |
| UW pH/DIC | Andrew Dickson | SIO | (NOAA) |
| DOC/DON | Dennis Hansell | BBSR | (NOAA) |
| ADCP | Peter Hacker/Eric Firing | U Hawaii | |
| ALACE Float deployment | Russ Davis | SIO | |
| Primary Productivity | Jack DiTullio, Walker Smith | UCSC/UT | (NOAA) |
| UW Chlorophyll | F. Chavez | MBARI | (NOAA) |
| Bathymetry | Ship personnel | | |
| Underway thermosalinograph | Ship personnel | | |

Cruise Summary:

WOCE Hydrographic Sections P14S and P15S were completed on the NOAA Ship Discoverer in early 1996, measuring a wide suite of physical, chemical, and biological processes. A total of 182 full-water column CTD/O2 stations were made along the sections (Fig. 1). A 36 position rosette was used as the primary system. On Leg 1, a lowered ADCP system was mounted on the 36 position rosette, reducing the number of available 10-liter sample bottles to 34.

Of the 182 stations, 159 stations were made with the 36-position, 10-liter bottle frame. The other 23 stations were made using a 24-position, 4-liter bottle frame, which was deployed primarily during bad weather.

A Sea-Bird Electronics 911plus CTD was mounted in each frame. In addition to the set of temperature and conductivity sensors resident on each CTD, a mobile set of temperature and conductivity sensors with a dissolved oxygen sensor was always mounted on the CTD in use. This arrangement allowed redundant temperature and conductivity measurements for quality control and continuity of temperature and conductivity measurements while keeping each CTD mounted in its own frame.

Water samples were collected at every station for analyses of salt, dissolved oxygen, and dissolved nutrients (silicate, nitrate, nitrite, and phosphate). Fig. 2a and 2b show locations where water samples were collected. Samples were drawn at selected locations for analysis of CFC-11, CFC-12, CFC-113, carbon tetrachloride, dissolved inorganic carbon (DIC), total alkalinity, pH, pCO2, dissolved organic carbon (DOC), carbon isotopes, oxygen isotopes, and other variables (see P14SP15s.sum file).

Daily shallow casts were made for assessment of various biological parameters, including productivity.

A total of 14 ALACE floats were deployed during the cruise, including 6 "Stretched T Profilers".

For both sections sampled on this cruise, stations were occupied at a nominal spacing of 30 nm, closer over steeply sloped bathymetry, and never more distant than 60 nm. Stations 1-3 were test stations occupied to evaluate the CTD/O2 and rosette systems on the transit from Hobart, Australia to the start of P14S. Stations 177 to 182 were taken after the completion of P15S but prior to the final port stop in Pago-Pago, American Samoa. These profiles constitute a short, nearly zonal, section across the Samoan Passage, taken to investigate deep water-mass and transport variability there. These data are reported here. The cruise was broken up into two legs of roughly one month duration each by a port stop in Wellington, New Zealand after station 93. Station 94 was a reoccupation of station 93 to evaluate temporal variations that occurred during the port stop.

WOCE section P14S began with station 4 at 53S, 170E in 200 m of water on the south edge of the Campbell Plateau and ended with station 32 at 66S, 171E, intersecting the zonal WHP section S4 occupied nominally along 67S in 1992. The section consisted of 29 stations. It sampled the entire Antarctic Circumpolar Current between the edge of the Campbell Plateau and the crest of the Pacific-Antarctic Ridge. At the ridge crest it explored a deep passage between the Ross Sea and the Southwest Pacific Basin. South of the ridge crest, it entered the north side of the Ross Sea Gyre.

WOCE section P15S began with station 33 at 67S, 170W, again intersecting the zonal WHP section S4 occupied nominally along 67S in 1992. It proceeded north to station 72 at 47.5S, 170W, whereupon it followed a diagonal in towards the Chatham Rise until station 85 at 43.25S, 175E. From there it moved back away from the rise towards 170W along a diagonal to station 104 at 36S, 170W. It then resumed north to station 154 at 10.5S, 170W, whereupon it shifted longitudes slightly to follow the axis of the Samoan Passage until station 164 at 7.5S, 168.75W. From there it continued north to station 174 at the equator, 168.75W. Station 175 and 176 were added to the section to improve meridional resolution in the vicinity of the Samoan Passage. From 15S to the equator the section overlapped WHP section P15N, occupied in 1994. The P15S section consisted of 143 stations, discounting the duplication after the Wellington port stop. It sampled the north end of the Ross Sea Gyre, the Antarctic Circumpolar Current, the Deep Western Boundary Current system on both flanks of the Chatham Rise, the Subtropical Gyre, and the Tropical Regime up to the equator.

Discussion:

Problems: In general, the ship, winches and analytical systems performed well on this expedition. All of the major goals of the program were met. At the completion of the P14S and P15S sections, enough time remained to extend the P15S section from 5S to the equator and to complete an additional 8 stations in Samoa Passage. Some time was lost at the beginning of Leg 1 due to problems with the level-wind mechanism on the primary winch. The wire was re-tensioned on the drum at sea by removing the CTD/rosette package, attaching a weight to the wire, and spooling the full length of the wire (except the last full wrap on the drum) behind the ship while underway. Level-wind problems were much reduced after this procedure.

Figs. 3-18 show preliminary sections of bottle salinity, dissolved oxygen, phosphate, silicate, nitrate, CFC-11, CFC-12. These preliminary sections only utilize values listed in the P14S and P15S.sea file which are flagged as "good" (flags 2 or 6) and where the btlnbr flag is also 2. Bathymetry shown in these figures is from depth recorded at each station.

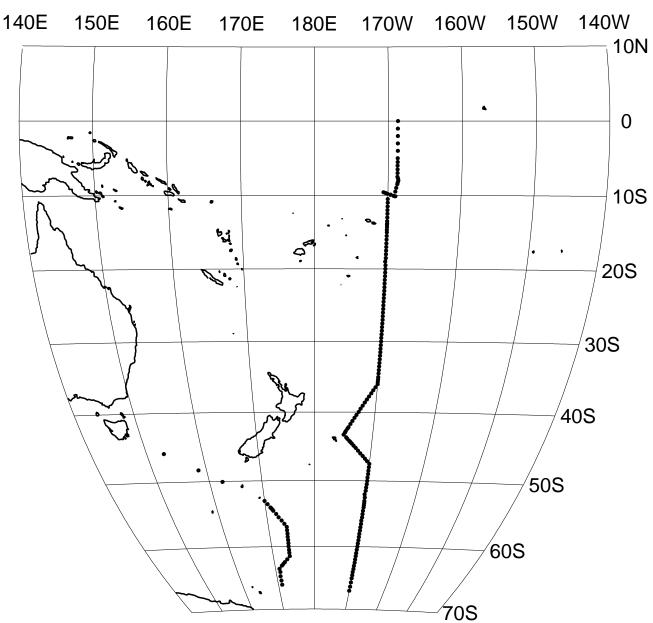
Participating Scientists: CGC96 Cruise

| Program | Inst. | Leg 1 | | Leg 2 | | Nationality (if non-US) |
|----------------|-------|------------------|---|------------------|---|-------------------------|
| Chief Sci. | PMEL | John Bullister | М | Richard Feely | M | |
| Co-Chief Sci. | PMEL | Greg Johnson | М | Marilyn Roberts | F | |
| CTD/O2 | PMEL | Kristy McTaggart | F | Kristy McTaggart | F | |
| | OSU | | | Jim Richman | М | |
| | IOS | John Love | М | | | (CANADA) |
| SeaBird | | Norge Larson | М | | | |
| Nutrients | PMEL | Calvin Mordy | М | Calvin Mordy | М | |
| | AOML | Zia-Zhong Zhang | М | Zia-Zhong Zhang | М | (PRC) |
| Oxygen | PMEL | Kirk Hargreaves | М | Kirk Hargreaves | М | |
| Salinity | AOML | Gregg Thomas | М | Gregg Thomas | М | |
| CFC | PMEL | Dave Wisegarver | М | Dave Wisegarver | М | |
| | PMEL | Craig Neill | М | Craig Neill | М | |
| | PMEL | Wenlin Huang | F | - | | (PRC) |
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| | RSMAS | Chris Edwards | М | Xiarong Zhu | М | |
| рН | USF | Sean McElligott | М | Sean McElliogott | М | |
| | USF | Wensheng Yao | М | Wensheng Yao | М | |
| | USF | Johan Schijf | М | Xeuwu Liu | М | |
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| DIC | PMEL | Marilyn Roberts | F | | | |
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| pCO2 | PMEL | Dana Greeley | М | Dana Greeley | М | |
| | AOML | Hua Chen | М | | | |
| | | | | Rhonda Kelly | F | |
| Primary Prod | UTK | Kendra Daly | F | Kendra Daly | F | |
| | USC | David Jones | М | David Jones | М | |
| | MBARI | Peter Walz | М | Tim Pennington | М | |
| DOC | BBSR | Susan Becker | F | Susan Becker | F | |
| | BBSR | Rachel Parsons | F | Rachel Parsons | F | |
| Carbon Isotop. | UW | Brian Kleinhaus | М | Tanya Westby | F | |
| Lowered ADCP | UH | Eric Firing | М | | | |

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Figure 1: P14S and P15S (CGC96) Station Locations



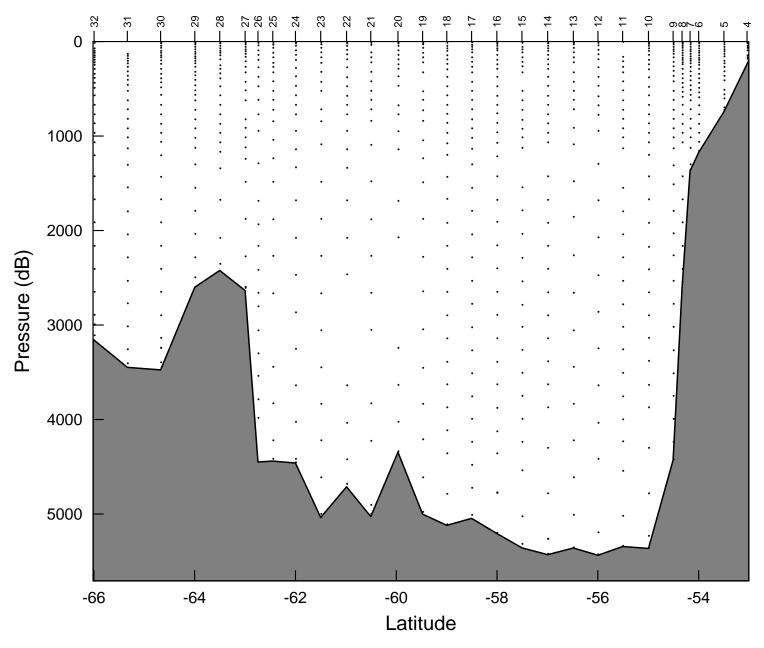


Figure 2a: Bottle Sample Locations on P14S

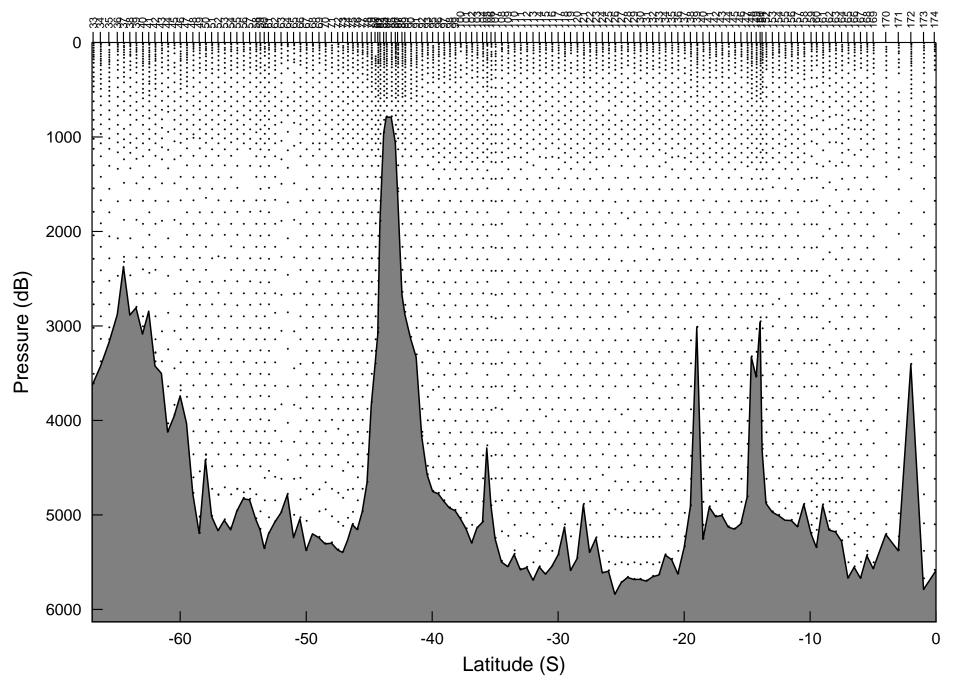


Figure 2b: Bottle Sample Locations on P15S

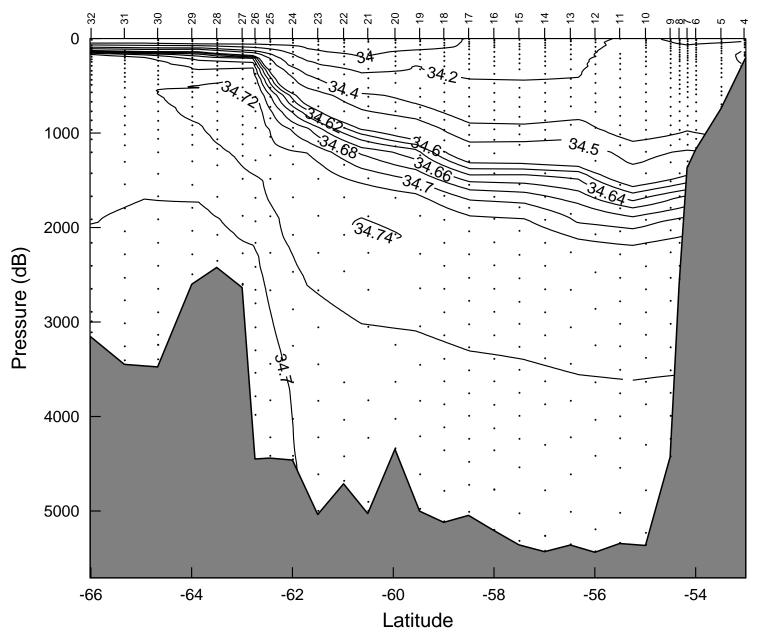


Figure 3a: Salinity Section along P14S (Preliminary)

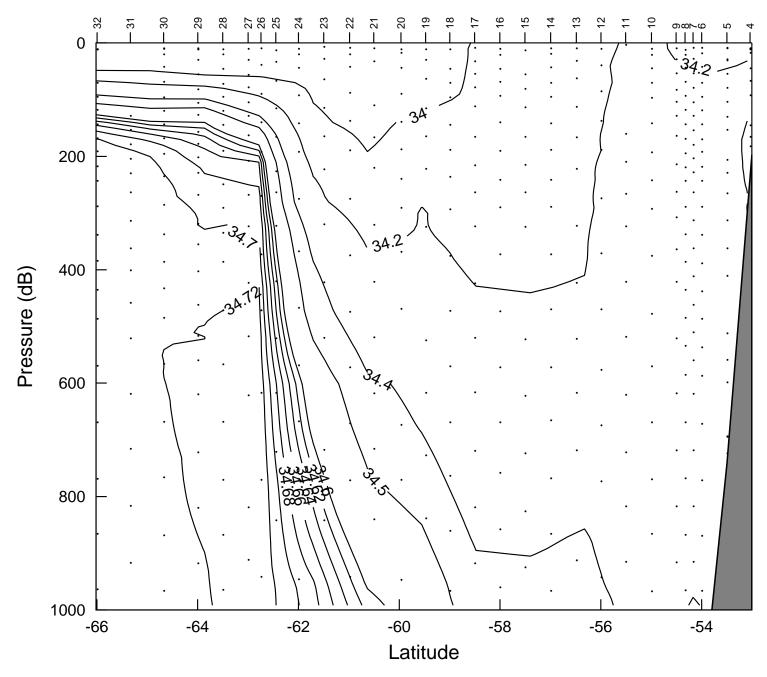


Figure 3b: Salinity Section along P14S (Preliminary)

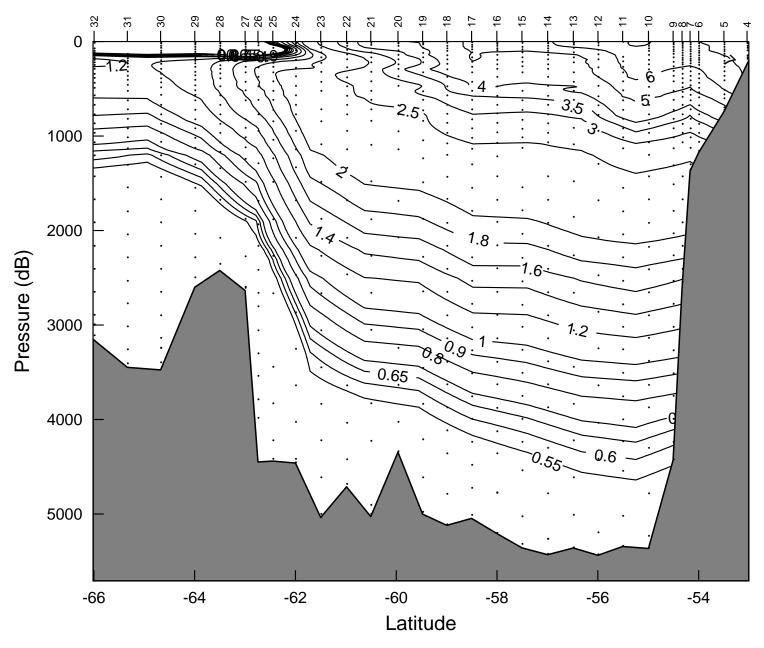


Figure 4a: Potential Temperature Section along P14S (Preliminary)

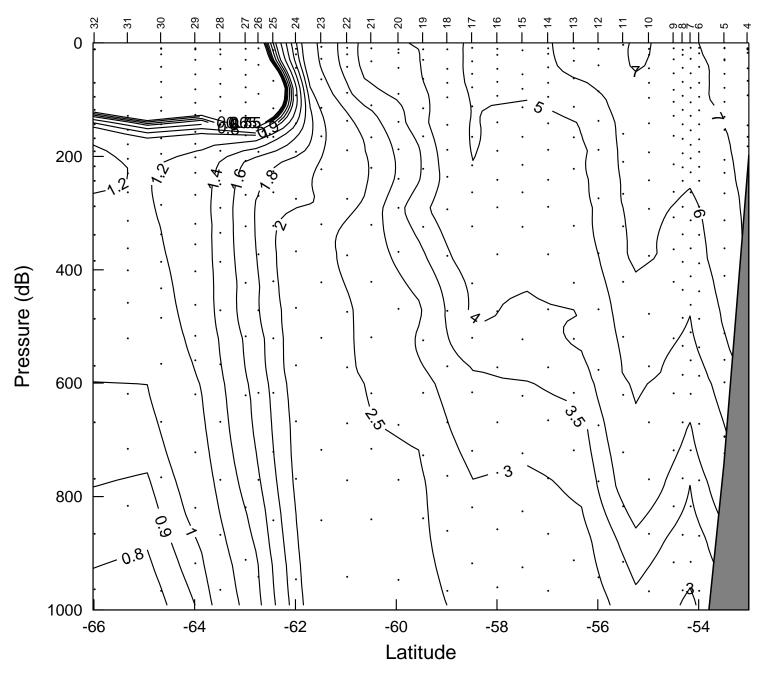


Figure 4b: Potential Temperature Section along P14S (Preliminary)

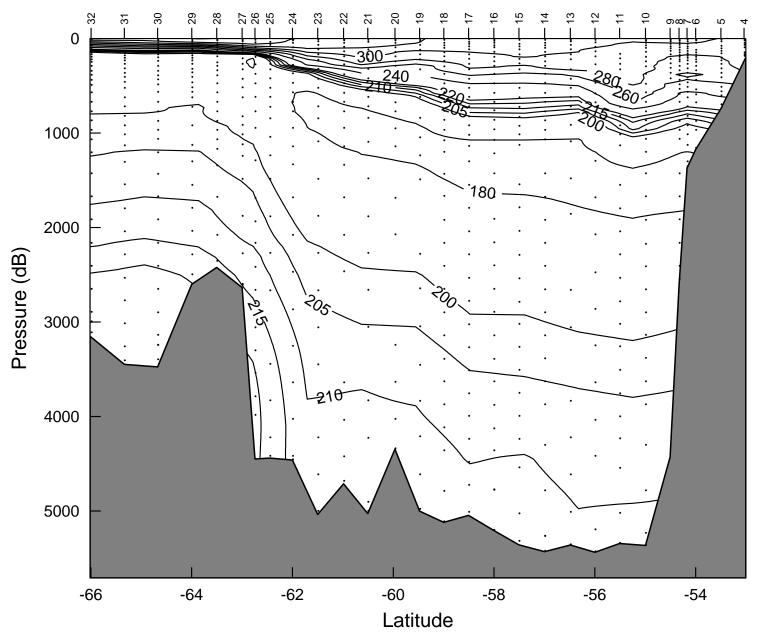


Figure 5a: Oxygen (umol/kg) Section along P14S (Preliminary)

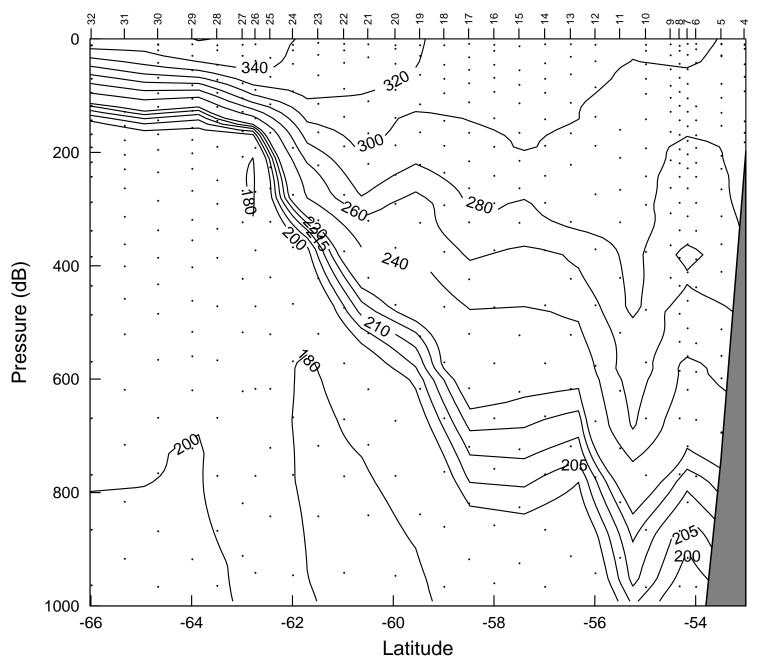


Figure 5b: Oxygen (umol/kg) Section along P14S (Preliminary)

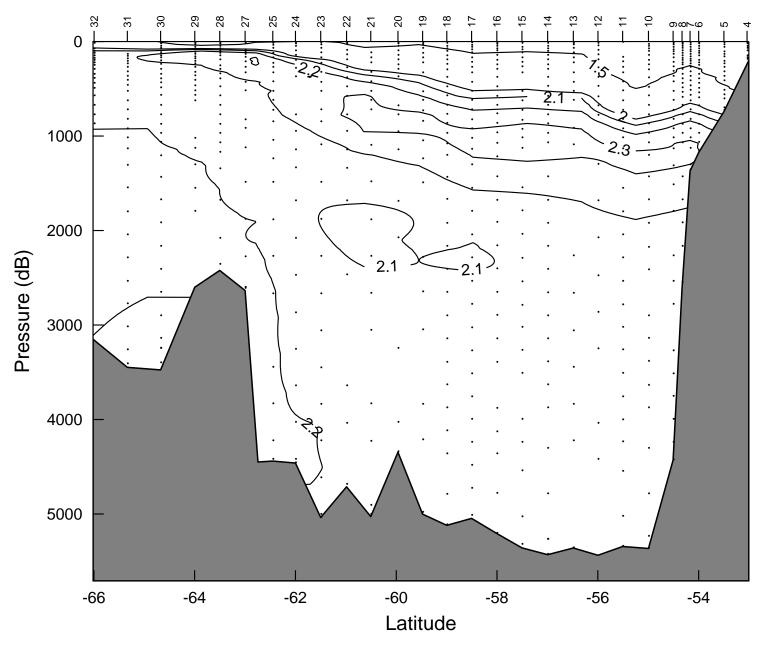


Figure 6a: Phosphate (umol/kg) Section along P14S (Preliminary)

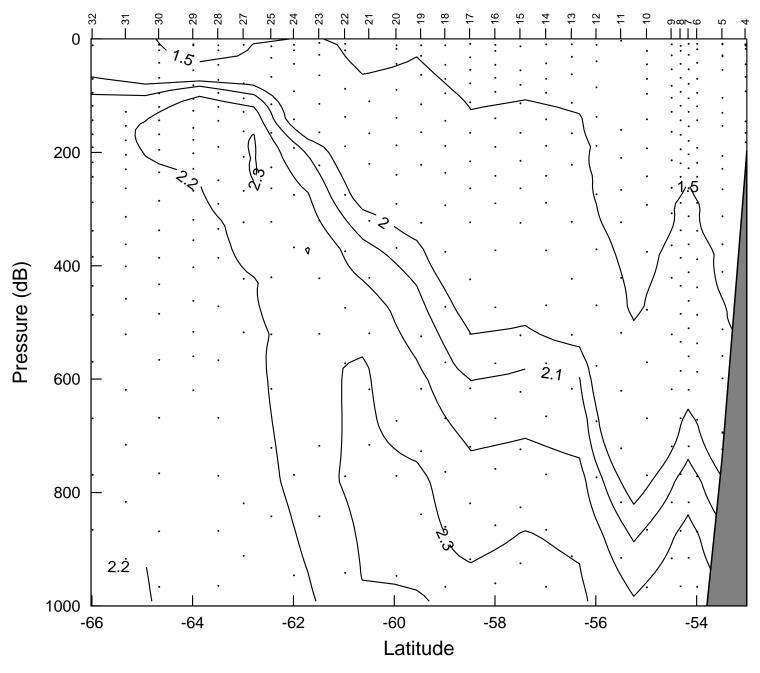


Figure 6b: Phosphate (umol/kg) Section along P14S (Preliminary)

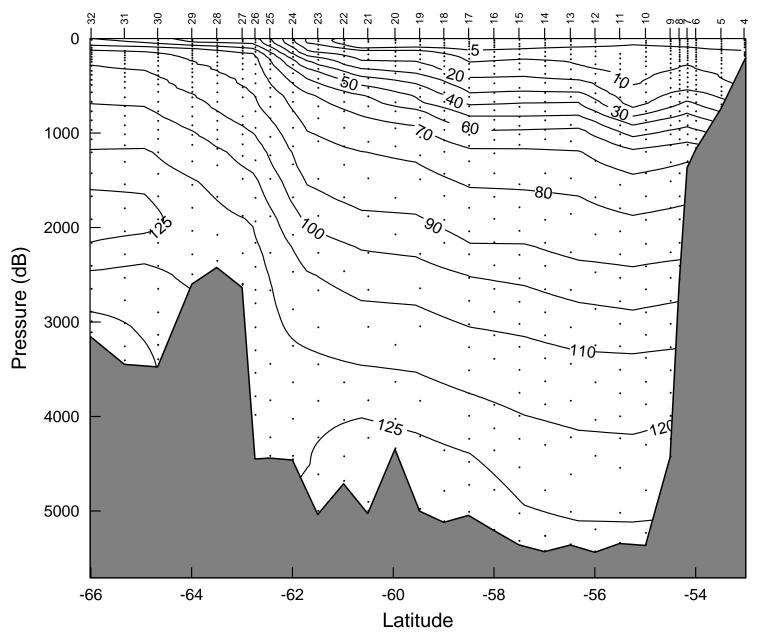


Figure 7a: Silicate (umol/kg) Section along P14S (Preliminary)

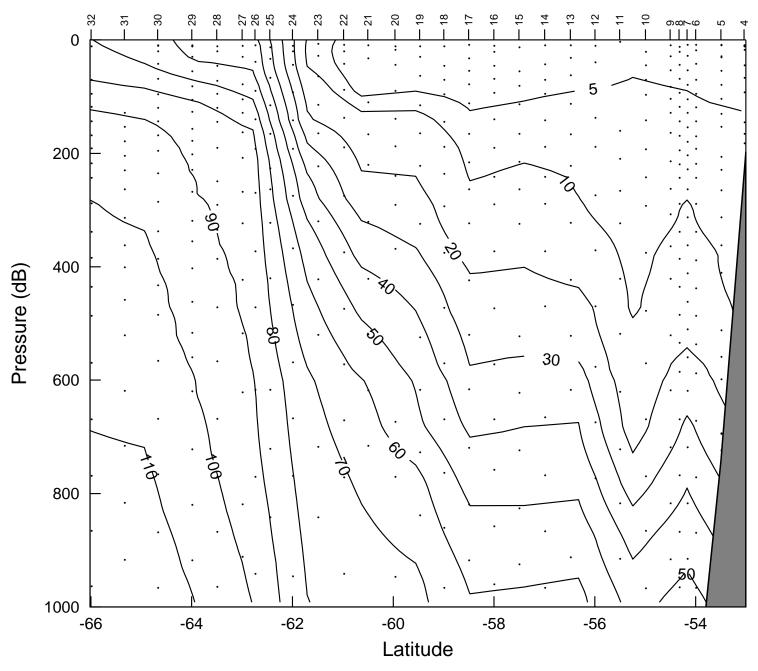


Figure 7b: Silicate (umol/kg) Section along P14S (Preliminary)

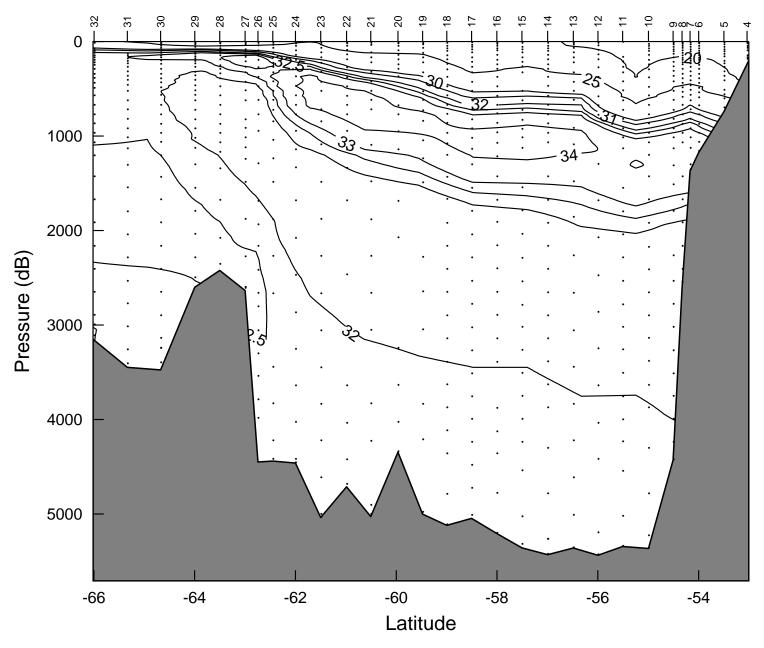


Figure 8a: Nitrate (umol/kg) Section along P14S (Preliminary)

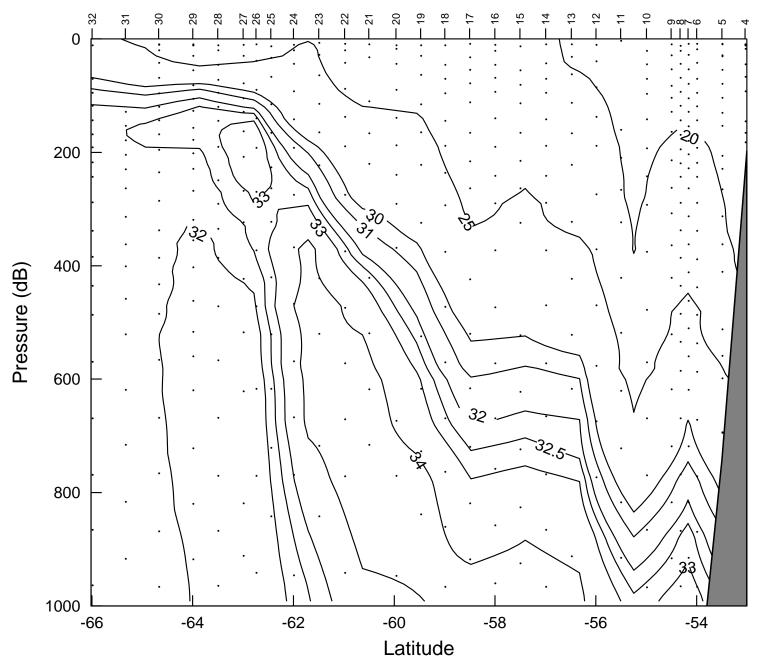


Figure 8b: Nitrate (umol/kg) Section along P14S (Preliminary)

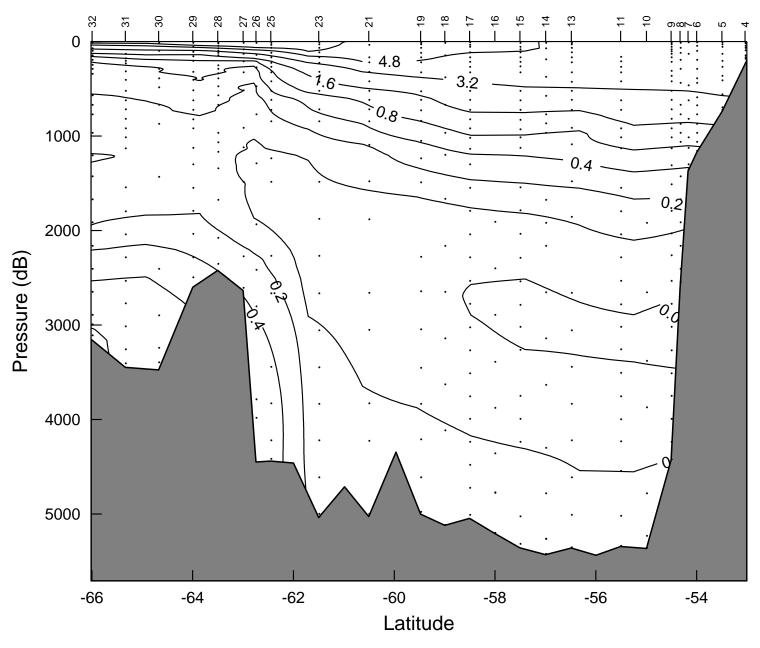


Figure 9a: CFC-11 (pmol/kg) Section along P14S (Preliminary)

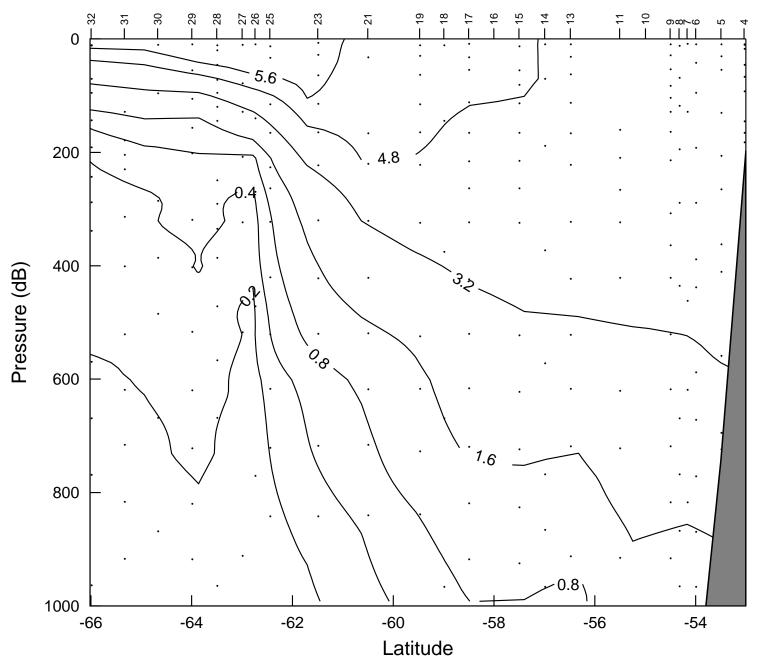


Figure 9b: CFC-11 (pmol/kg) Section along P14S (Preliminary)

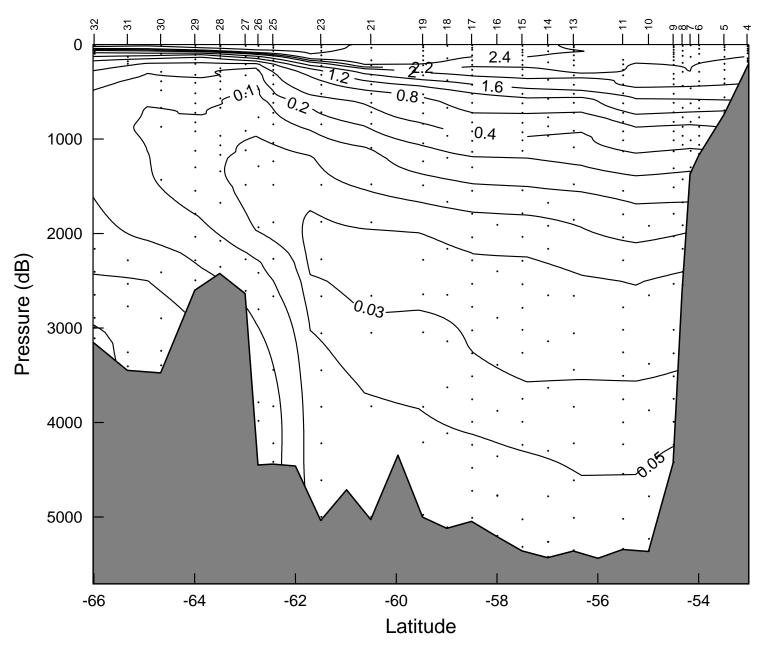


Figure 10a: CFC-12 (pmol/kg)Section along P14S (Preliminary)

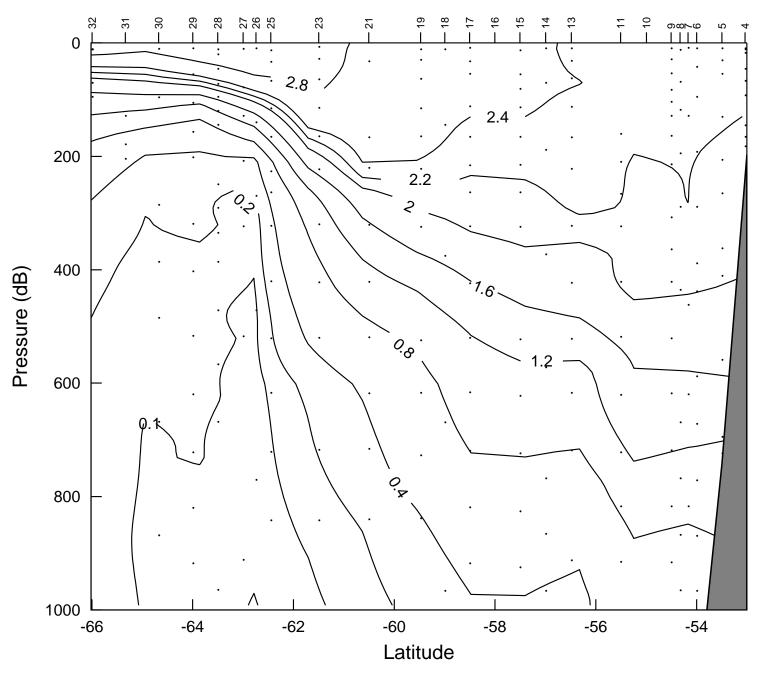


Figure 10b: CFC-12 (pmol/kg)Section along P14S (Preliminary)

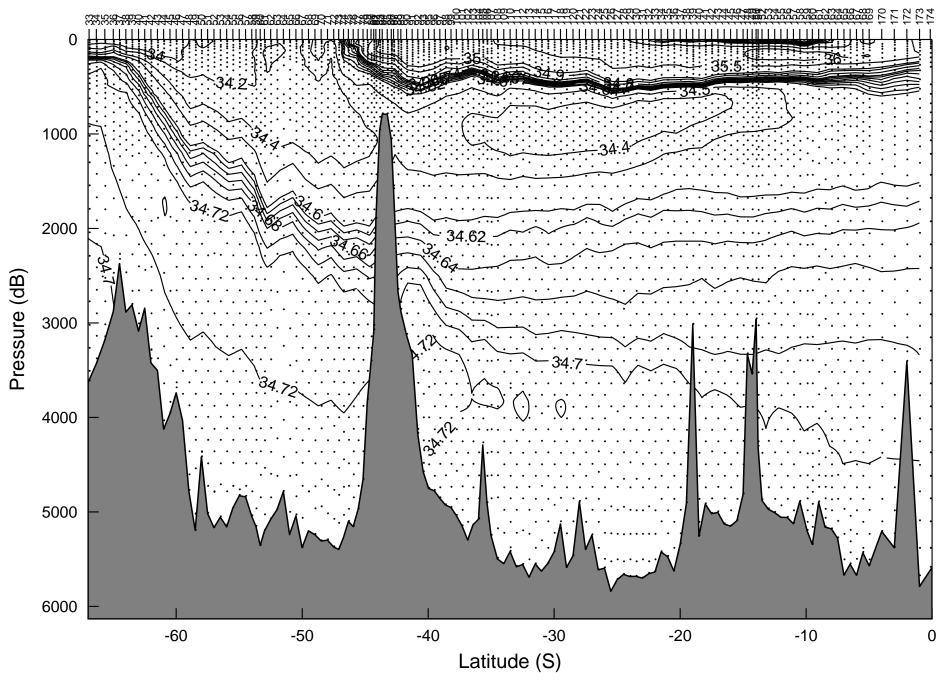


Figure 11a: Salinity Section along P15S (Preliminary)

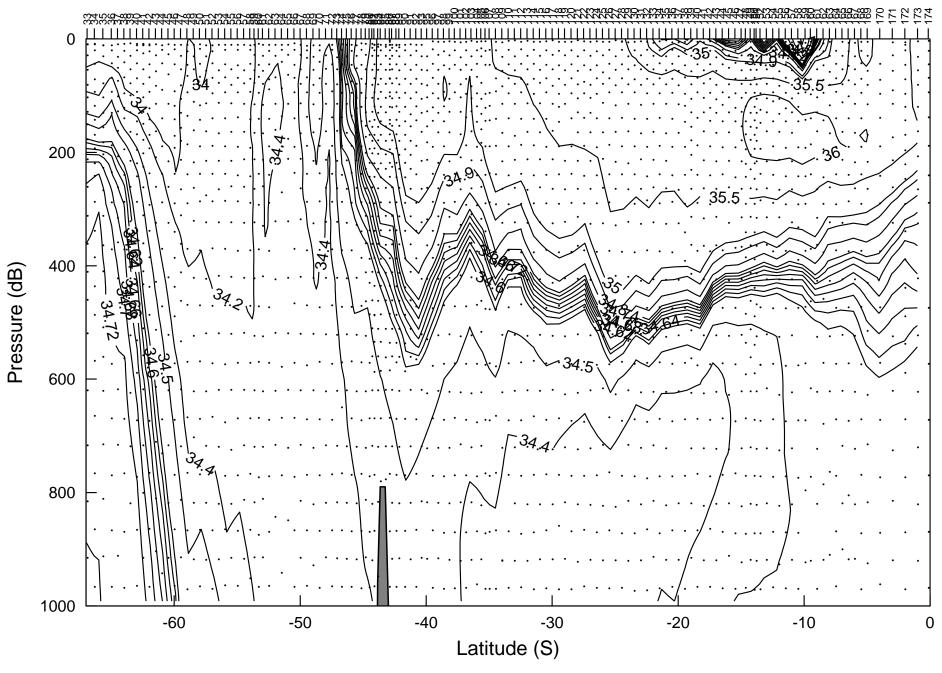


Figure 11b: Salinity Section along P15S (Preliminary)

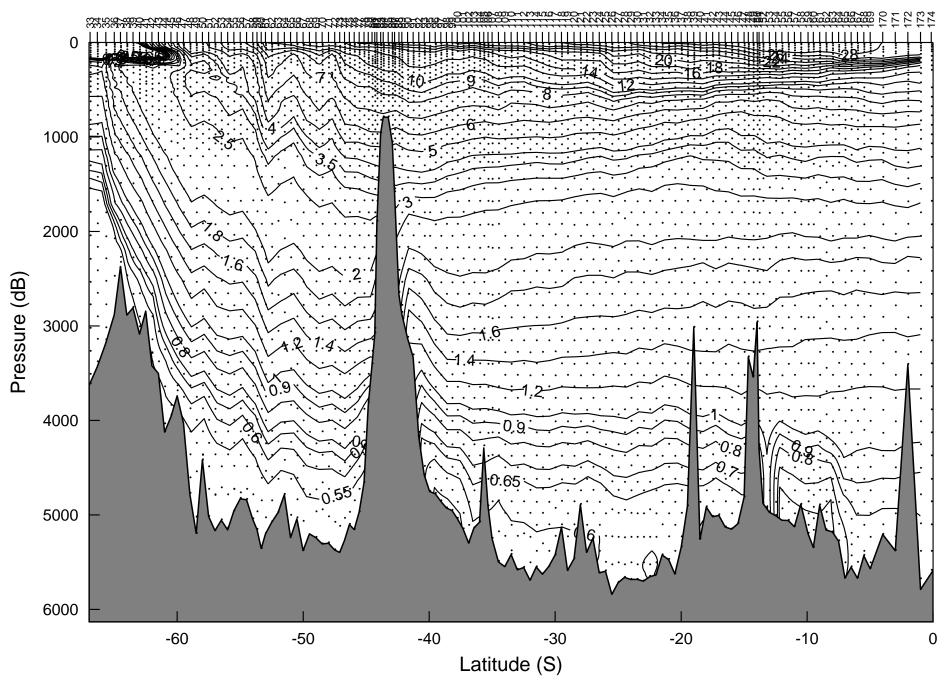


Figure 12a: Potential Temperature along P15S (Preliminary)

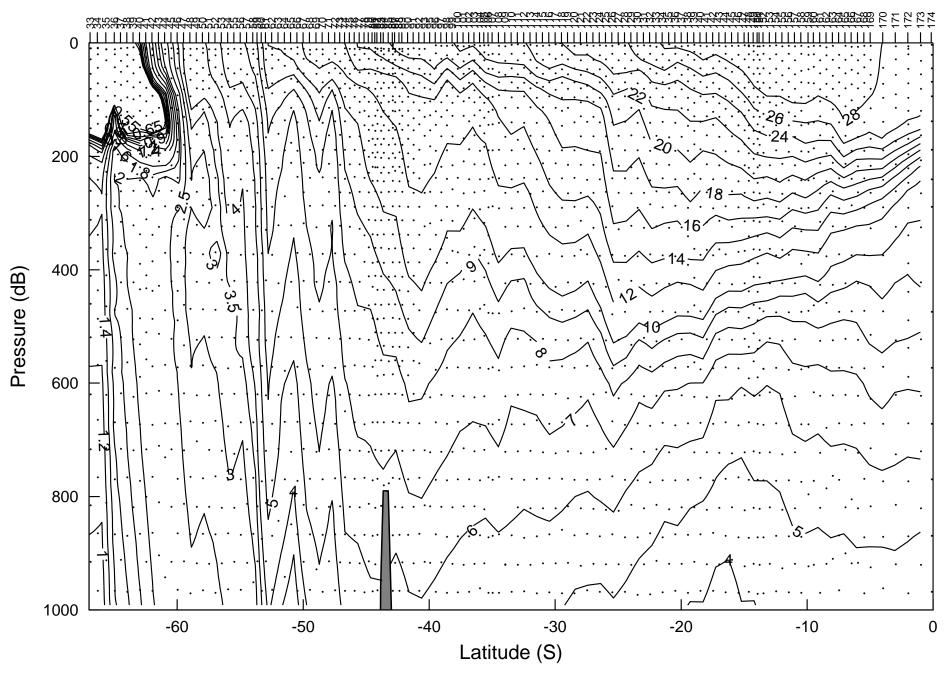


Figure 12b: Potential Temperature along P15S (Preliminary)

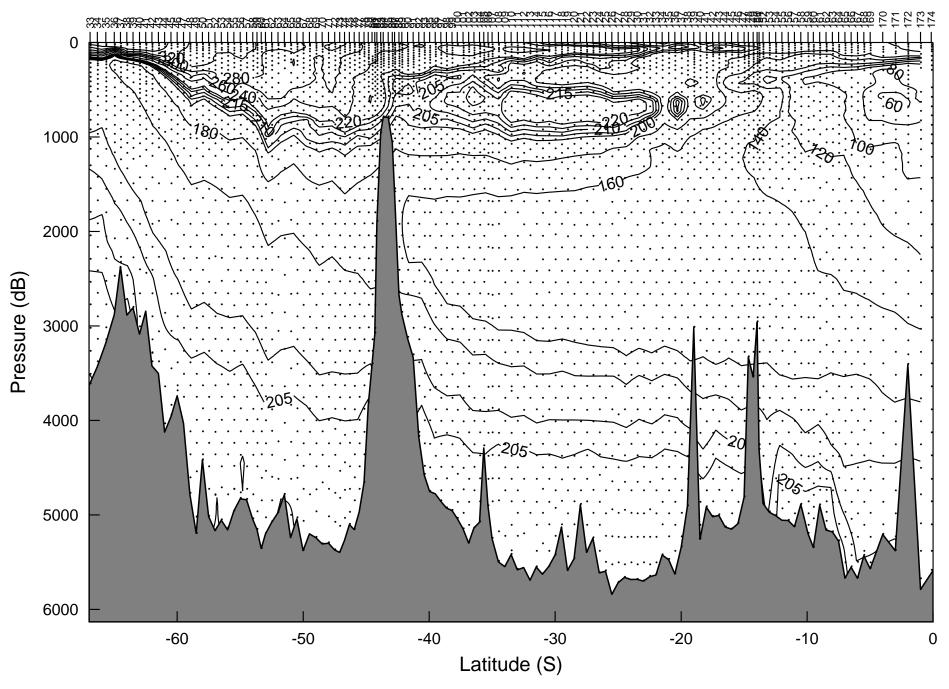


Figure 13a: Oxygen (umol/kg) Section along P15S (Preliminary)

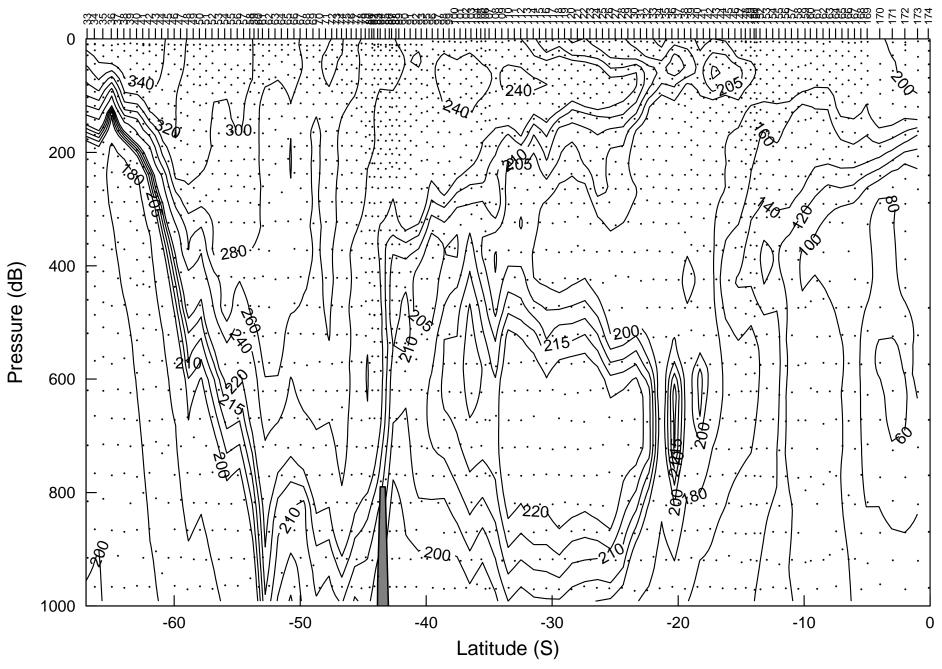


Figure 13b: Oxygen (umol/kg) Section along P15S (Preliminary)

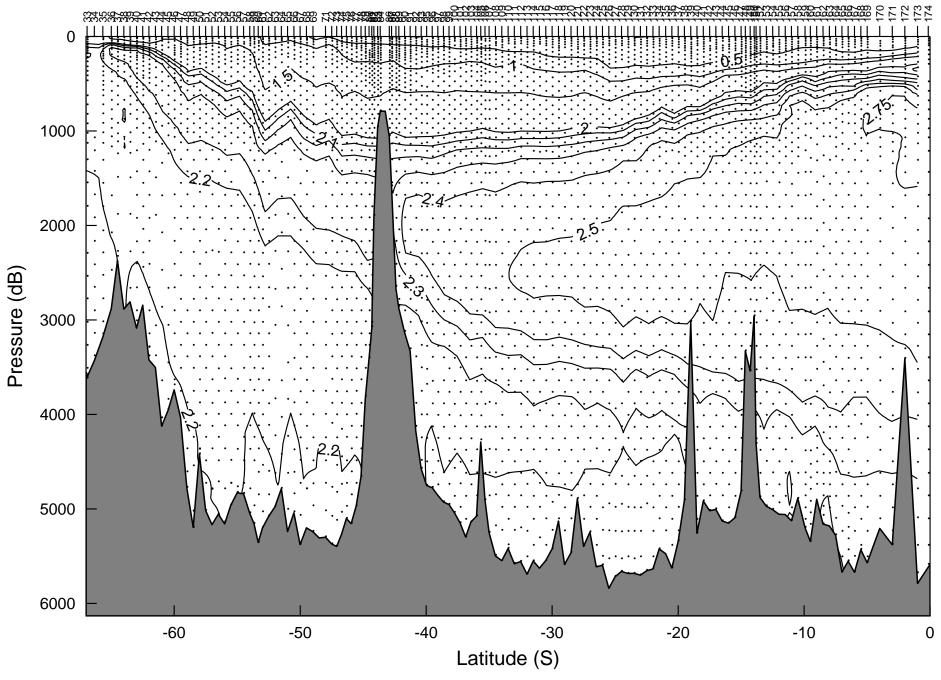


Figure 14a: Phosphate (umol/kg) Section along P15S (Preliminary)

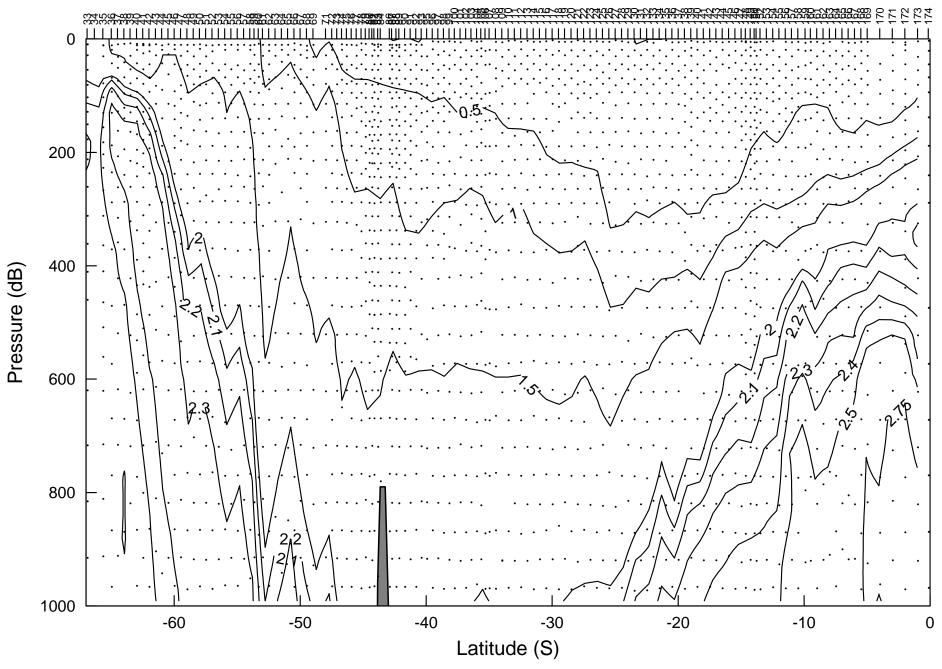


Figure 14b: Phosphate (umol/kg) Section along P15S (Preliminary)

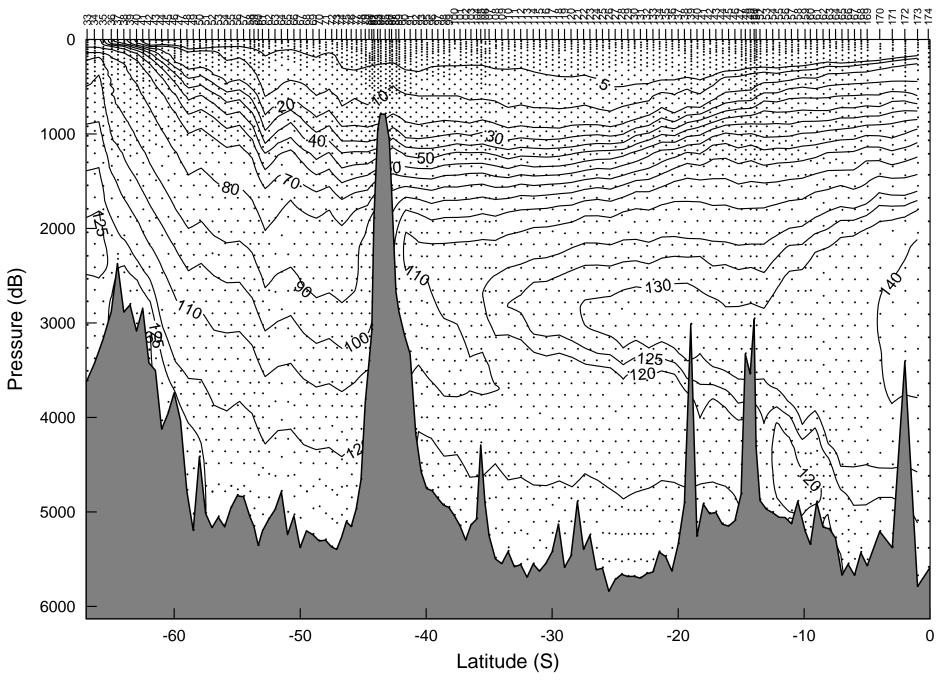


Figure 15a: Silicate (umol/kg) Section along P15S (Preliminary)

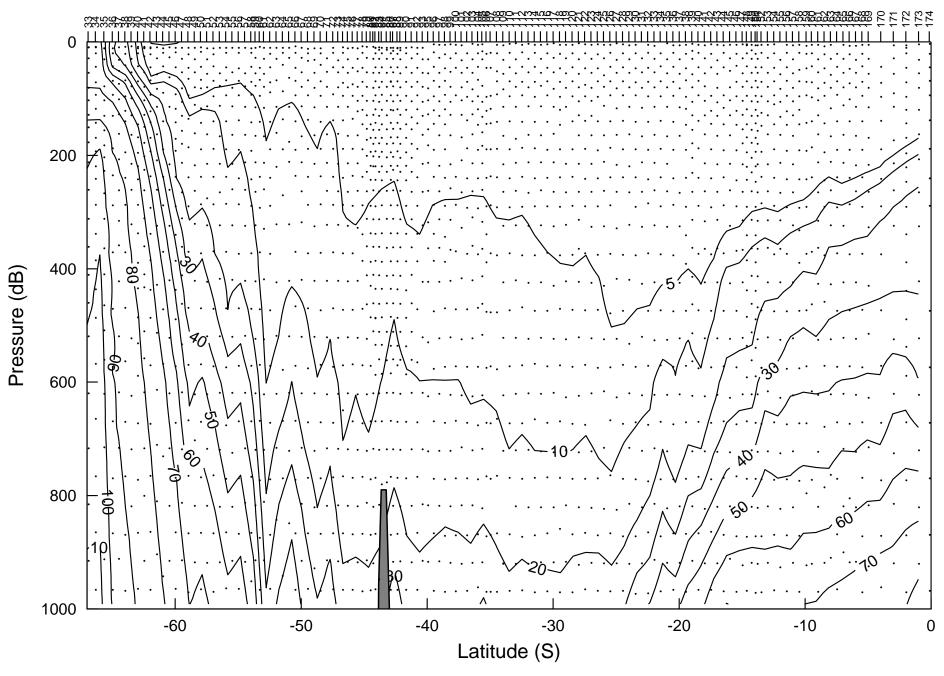


Figure 15b: Silicate (umol/kg) Section along P15S (Preliminary)

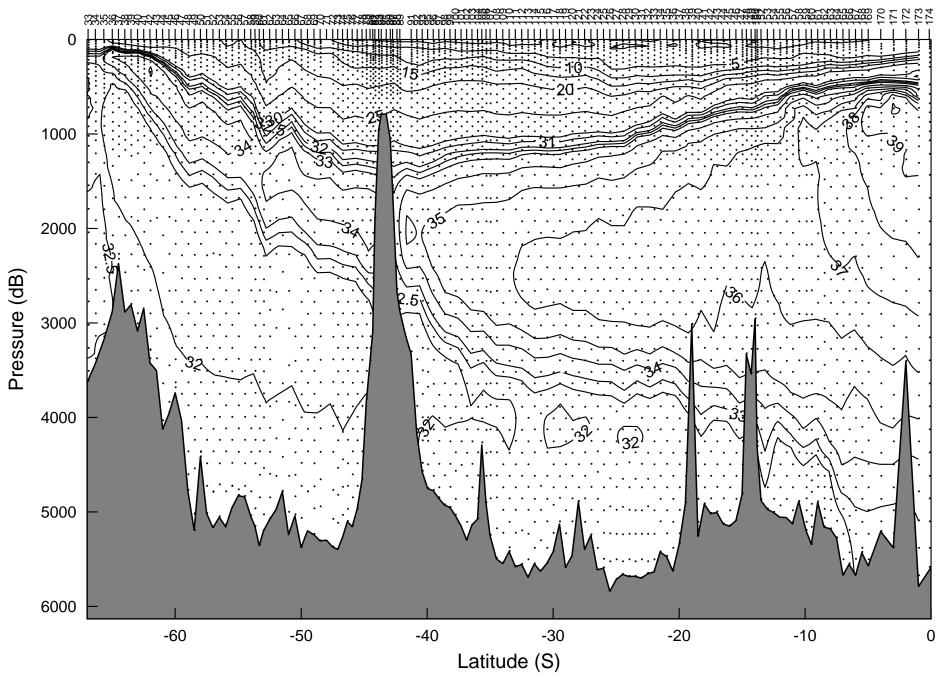


Figure 16a: Nitrate (umol/kg) Section along P15S (Preliminary)

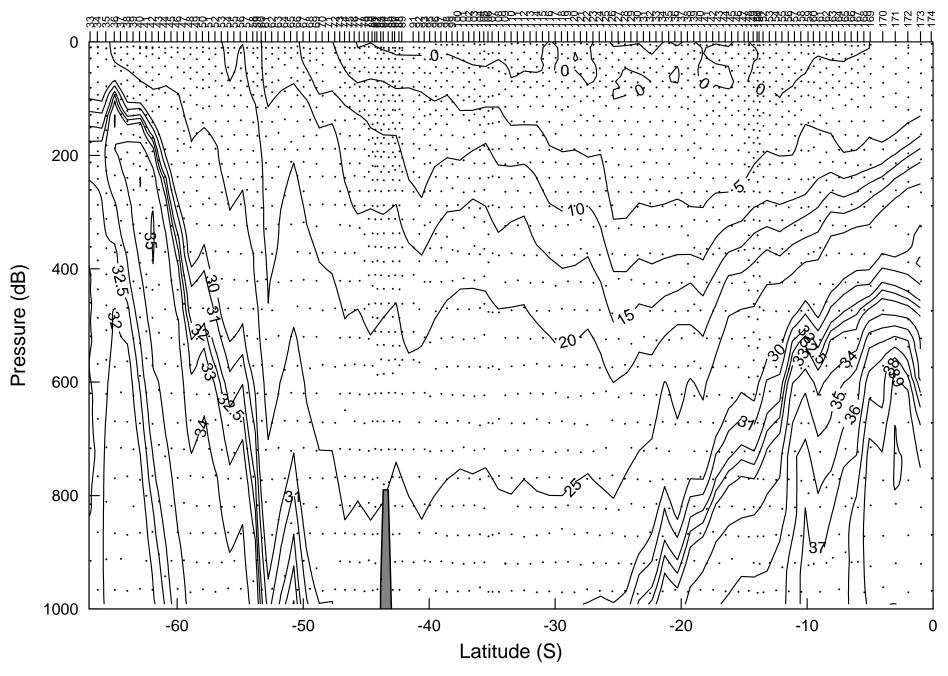


Figure 16b: Nitrate (umol/kg) Section along P15S (Preliminary)

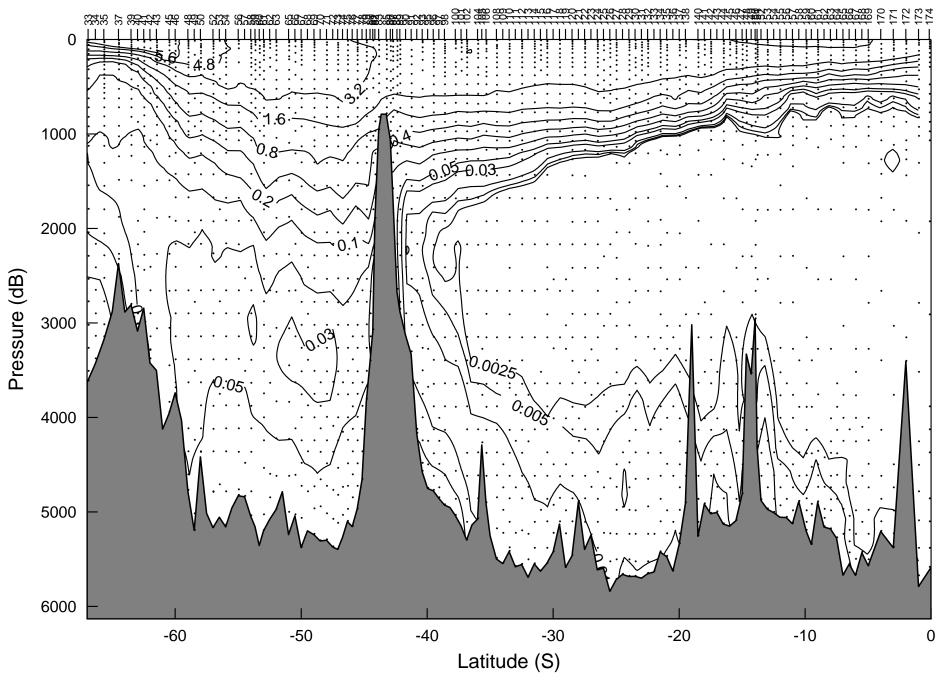


Figure 17a: CFC-11 (pmol/kg) Section along P15S (Preliminary)

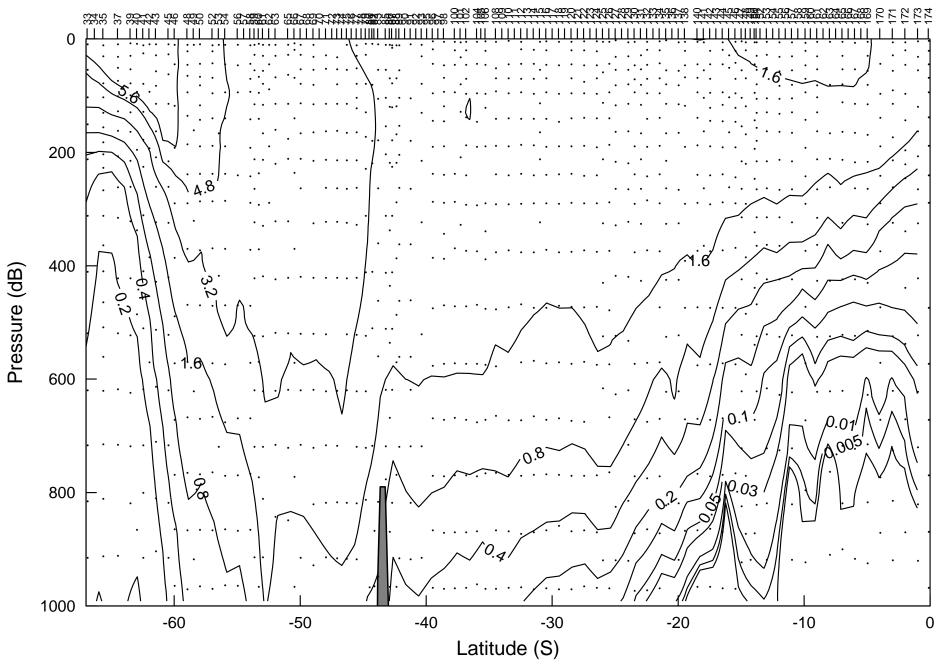


Figure 17b: CFC-11 (pmol/kg) Section along P15S (Preliminary)

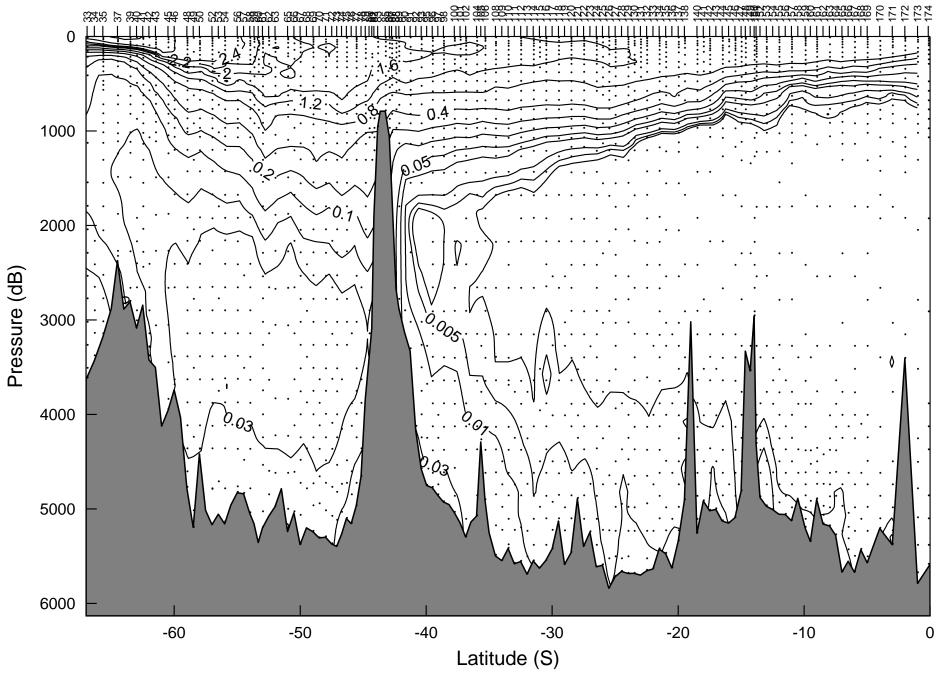


Figure 18a: CFC-12 (pmol/kg)Section along P15S (Preliminary)

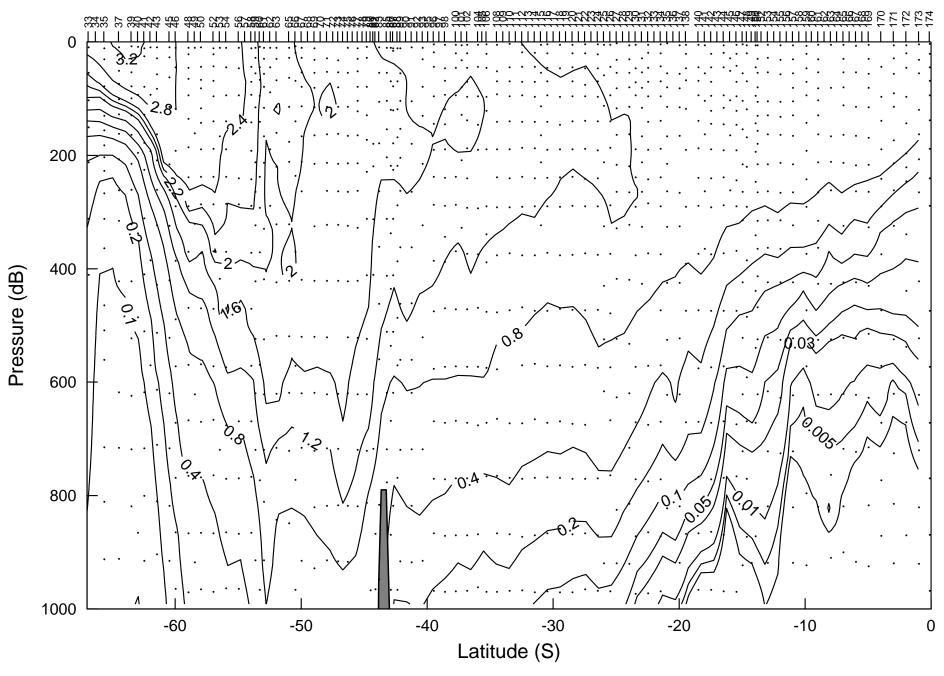


Figure 18b: CFC-12 (pmol/kg)Section along P15S (Preliminary)

APPENDIX 1: CGC96 Station Locations: Leg 1

| STATION | | | | BOTTOM |
|---------|-----------|------------|---------------------|-----------|
| NUMBER | Latitude | Longitude | Date | DEPTH (M) |
| 1 | 45 49.5 S | 153 05.1 E | 6 Jan 96 | 4468 |
| 2 | 48 19.1 S | 158 29.9 E | 7 Jan 96 | 4850 |
| 3 | 50 05.0 S | 162 29.3 E | 8 Jan 96 | 4456 |
| 4 | 53 00.1 S | 169 59.3 E | 9 Jan 96 | 198 |
| 5 | 53 29.9 S | 170 29.7 E | 9 Jan 96 | 743 |
| 6 | 53 59.9 S | 171 00.1 E | 9 Jan 96 | 1175 |
| 7 | 54 10.2 S | 171 10.8 E | 9 Jan 96 | 1370 |
| 8 | 54 19.8 S | 171 20.2 E | 9 Jan 96 | 2615 |
| 9 | 54 30.3 S | 171 29.8 E | 9 Jan 96 | 4390 |
| 10 | 54 59.7 S | 172 00.7 E | 10 Jan 96 | 5345 |
| 11 | 55 30.4 S | 172 27.0 E | 10 Jan 96 | 5332 |
| 12 | 55 59.8 S | 173 00.6 E | 10 Jan 96 | 5415 |
| 13 | 56 29.2 S | 173 30.2 E | 11 Jan 96 | 5345 |
| 14 | 56 59.7 S | 173 58.6 E | 11 Jan 96 | 5430 |
| 15 | 57 30.3 S | 173 58.5 E | 11 Jan 96 | 5358 |
| 16 | 58 00.2 S | 173 59.5 E | 12 Jan 96 | 5205 |
| 17 | 58 30.2 S | 173 58.2 E | 12 Jan 96 | 5046 |
| 18 | 58 59.8 S | 174 00.0 E | 12 Jan 96 | 5110 |
| 19 | 59 28.7 S | 173 59.7 E | 12 Jan 96 | 5002 |
| 20 | 59 57.9 S | 173 57.9 E | 13 Jan 96 | 4346 |
| 21 | 60 30.3 S | 173 57.8 E | 13 Jan 96 | 5028 |
| 22 | 60 59.1 S | 173 58.9 E | 14 Jan 96 | 4712 |
| 23 | 61 30.0 S | 174 00.2 E | 14 Jan 96 | 5037 |
| 24 | 62 00.0 S | 173 16.1 E | 14 Jan 96 | 4450 |
| 25 | 62 26.9 S | 172 35.2 E | 14 Jan 96 | 4440 |
| 26 | 62 44.7 S | 172 09.0 E | 15 Jan 96 | 4450 |
| 27 | 62 60.0 S | 171 44.9 E | 15 Jan 96 | 2636 |
| 28 | 63 30.1 S | 170 59.6 E | 15 Jan 96 | 2422 |
| 29 | 63 59.8 S | 171 06.6 E | 16 Jan 96 | 2600 |
| 30 | 64 40.6 S | 170 58.6 E | 16 Jan 96 | 3475 |
| 31 | 65 20.2 S | 170 60.0 E | 16 Jan 96 | 3449 |
| 32 | 66 00.9 S | 171 01.6 E | 17 Jan 96 | 3151 |
| 33 | 66 59.6 S | 170 00.0 W | 18 Jan 96 | 3630 |
| 34 | 66 20.3 S | 169 60.0 W | 18 Jan 96 | 3430 |
| 35 | 65 39.8 S | 170 00.3 W | 19 Jan 96 | 3180 |
| 36 | 64 59.6 S | 170 00.9 W | 19 Jan 96 | 2880 |
| 37 | 64 30.1 S | 169 59.9 W | 19 Jan 96 | 2370 |
| 38 | 63 59.7 S | 170 02.0 W | 19 Jan 96 | 2783 |
| 39 | 63 30.1 S | 170 00.3 W | 20 Jan 96 | 2805 |
| 40 | 62 59.7 S | 170 01.4 W | 20 Jan 96 | 3085 |
| 41 | 62 30.0 S | 169 59.8 W | 20 Jan 96 | 2843 |
| 42 | 62 00.2 S | 169 59.9 W | 20 Jan 96 | 3422 |

| STATION | | | | BOTTOM |
|---------|-----------|------------|-----------|-------------------------------|
| NUMBER | Latitude | Longitude | Date | $\overline{\text{DEPTH}}$ (M) |
| 43 | 61 29.5 S | 169 60.0 W | 21 Jan 96 | 3501 |
| 44 | 61 00.1 S | 170 00.3 W | 21 Jan 96 | 3630 |
| 45 | 60 29.7 S | 169 59.6 W | 22 Jan 96 | 3960 |
| 46 | 60 00.3 S | 170 00.3 W | 22 Jan 96 | 3738 |
| 47 | 59 30.2 S | 169 59.9 W | 22 Jan 96 | 4030 |
| 48 | 58 59.9 S | 170 00.2 W | 22 Jan 96 | 4780 |
| 49 | 58 29.6 S | 170 00.8 W | 23 Jan 96 | 5188 |
| 50 | 57 59.7 S | 170 00.8 W | 23 Jan 96 | 4140 |
| 51 | 57 30.1 S | 170 00.4 W | 23 Jan 96 | 5001 |
| 52 | 57 00.2 S | 170 00.2 W | 24 Jan 96 | 5165 |
| 53 | 56 29.9 S | 169 59.8 W | 24 Jan 96 | 5055 |
| 54 | 55 60.0 S | 170 01.8 W | 24 Jan 96 | 5157 |
| 55 | 55 29.9 S | 170 00.0 W | 24 Jan 96 | 4950 |
| 56 | 54 59.8 S | 169 60.0 W | 25 Jan 96 | 4820 |
| 57 | 54 29.4 S | 170 00.1 W | 25 Jan 96 | 4819 |
| 58 | 54 00.1 S | 169 59.3 W | 25 Jan 96 | 5013 |
| 59 | 53 39.9 S | 169 59.4 W | 25 Jan 96 | 5125 |
| 60 | 53 19.9 S | 169 59.6 W | 26 Jan 96 | 5276 |
| 61 | 52 60.0 S | 170 00.5 W | 26 Jan 96 | 5185 |
| 62 | 52 29.9 S | 170 01.8 W | 26 Jan 96 | 5065 |
| 63 | 52 00.1 S | 170 07.8 W | 26 Jan 96 | 4968 |
| 64 | 51 30.0 S | 170 00.2 W | 27 Jan 96 | 4757 |
| 65 | 51 00.2 S | 170 00.4 W | 27 Jan 96 | 5239 |
| 66 | 50 29.9 S | 169 59.6 W | 27 Jan 96 | 5041 |
| 67 | 50 00.4 S | 169 59.9 W | 28 Jan 96 | 5340 |
| 68 | 49 30.2 S | 170 00.9 W | 28 Jan 96 | 5200 |
| 69 | 48 59.6 S | 169 59.4 W | 28 Jan 96 | 5235 |
| 70 | 48 30.0 S | 170 00.2 W | 28 Jan 96 | 5280 |
| 71 | 47 59.8 S | 170 00.3 W | 29 Jan 96 | 5270 |
| 72 | 47 30.2 S | 169 59.8 W | 29 Jan 96 | 5285 |
| 73 | 47 06.5 S | 170 27.7 W | 29 Jan 96 | 5365 |
| | 46 43.4 S | 170 54.7 W | 30 Jan 96 | 5268 |
| 75 | 46 20.0 S | 171 22.2 W | 30 Jan 96 | 5083 |
| 76 | 45 57.0 S | 171 49.5 W | 30 Jan 96 | 5136 |
| 77 | 45 33.6 S | 172 16.7 W | 30 Jan 96 | 4953 |
| 78 | 45 10.6 S | 172 44.2 W | 31 Jan 96 | 4652 |
| 79 | 44 50.1 S | 173 08.2 W | 31 Jan 96 | 3838 |
| 80 | 44 31.8 S | 173 29.4 W | 31 Jan 96 | 3408 |
| 81 | 44 19.2 S | 173 44.7 W | | 3090 |
| 82 | 44 09.4 S | 173 56.3 W | | 1908 |
| 83 | 43 50.9 S | 174 17.7 W | 1 Feb 96 | 950 |
| | 43 38.8 S | 174 32.2 W | 1 Feb 96 | 790 |
| | 43 15.2 S | 174 59.9 W | 1 Feb 96 | 790 |
| 86 | 42 55.9 S | 174 47.2 W | 1 Feb 96 | 1059 |

| STATION | | | | BOTTOM |
|----------|------------------------|------------|----------------------|-----------|
| NUMBER | Latitude | Longitude | Date | DEPTH (M) |
| 87 | 42 44.8 S | 174 39.3 W | 1 Feb 96 | 1590 |
| 88 | 42 24.1 S | 174 24.4 W | 1 Feb 96 | 2668 |
| 89 | 42 10.0 S | 174 15.0 W | 2 Feb 96 | 2875 |
| 90 | 41 42.8 S | 174 15.0 W | 2 Feb 96 | 3130 |
| 91 | 41 16.0 S | 173 38.6 W | 2 Feb 96 | 3330 |
| 92 | 40 49.5 S | 173 19.5 W | 2 Feb 96 | 4170 |
| 93 | | | 2 Feb 96 2 Feb 96 | 4568 |
| 93 94 | 40 23.6 S 40 23.5 S | | | |
| | | | | 4568 |
| 95 06 | | 172 42.2 W | 14 Feb 96 | 4728 |
| 96 | 39 31.0 S | 172 25.2 W | 14 Feb 96 | 4751 |
| 97 | 39 04.3 S | 172 07.7 W | 14 Feb 96 | 4836 |
| 98 | 38 37.8 S | 171 48.6 W | 14 Feb 96 | 4901 |
| 99 | 38 11.4 S | 171 30.2 W | 15 Feb 96 | 4918 |
| 100 | 37 45.8 S | 171 12.0 W | 15 Feb 96 | 4980 |
| 101 | 37 18.6 S | 170 53.7 W | 15 Feb 96 | 5112 |
| 102 | 36 52.3 S | 170 37.0 W | 15 Feb 96 | 5254 |
| 103 | 36 27.0 S | 170 17.2 W | 16 Feb 96 | 5102 |
| 104 | 36 00.2 S | 170 00.3 W | 16 Feb 96 | 5050 |
| 105 | 35 40.3 S | 170 00.9 W | 16 Feb 96 | 4290 |
| 106 | 35 20.0 S | 170 00.1 W | 16 Feb 96 | 4880 |
| 107 | 35 00.5 S | 169 59.6 W | 17 Feb 96 | 5226 |
| 108 | 34 30.2 S | 170 00.2 W | 17 Feb 96 | 5457 |
| 109 | 33 59.8 S | 169 60.0 W | 17 Feb 96 | 5501 |
| 110 | 33 29.9 S | 170 00.1 W | 18 Feb 96 | 5387 |
| 111 | 33 00.1 S | 170 00.1 W | 18 Feb 96 | 5548 |
| 112 | 32 30.1 S | 170 00.1 W | 18 Feb 96 | 5501 |
| 113 | 31 59.8 S | 169 59.8 W | 18 Feb 96 | 5640 |
| 114 | 31 30.0 S | 169 59.3 W | 19 Feb 96 | 5496 |
| 115 | 31 00.4 S | 169 59.7 W | 19 Feb 96 | 5572 |
| 116 | 30 30.3 S | 169 59.8 W | 19 Feb 96 | 5505 |
| 117 | 30 00.2 S | 169 59.8 W | 19 Feb 96 | 5394 |
| 118 | 29 30.2 S | 169 59.8 W | 20 Feb 96 | 5127 |
| 119 | 29 00.8 S | 169 59.9 W | 20 Feb 96 | 5562 |
| 120 | 28 30.5 S | 169 59.8 W | 20 Feb 96 | 5425 |
| 121 | 28 00.3 S | 169 59.6 W | 21 Feb 96 | 4888 |
| 122 | 27 30.1 S | 170 00.1 W | 21 Feb 96 | 5318 |
| 123 | 27 00.3 S | 169 59.5 W | 21 Feb 96 | 5214 |
| 124 | 26 29.7 S | 169 59.4 W | 21 Feb 96 | 5575 |
| 125 | 26 00.3 S | 169 59.7 W | 22 Feb 96 | 5563 |
| 126 | 25 30.0 S | 169 60.0 W | 22 Feb 96 | 5787 |
| 127 | 25 00.1 S | 169 59.9 W | 22 Feb 96 | 5600 |
| 128 | 24 30.1 S | 170 00.1 W | 23 Feb 96 | 5610 |
| 129 | 23 59.8 S | 170 00.1 W | 23 Feb 96 | 5637 |
| 130 | 23 30.1 S | 170 00.1 W | 23 Feb 96 | 5626 |
| • | | · ·· | | = = |

| STATION | | | | BOTTOM |
|---------|-----------|------------|-----------|--------------|
| NUMBER | Latitude | Longitude | Date | DEPTH (M) |
| 131 | 22 59.8 S | 169 59.7 W | 23 Feb 96 | <u>565</u> 0 |
| 132 | 22 30.0 S | 169 59.9 W | 24 Feb 96 | 5609 |
| 133 | 22 00.0 S | 169 59.9 W | 24 Feb 96 | 5587 |
| 134 | 21 30.4 S | 170 00.1 W | 24 Feb 96 | 5388 |
| 135 | 20 59.7 S | 169 59.6 W | 25 Feb 96 | 5427 |
| 136 | 20 29.9 S | 170 00.1 W | 25 Feb 96 | 5560 |
| 137 | 20 00.0 S | 170 00.1 W | 25 Feb 96 | 5294 |
| 138 | 19 29.9 S | 170 00.1 W | 25 Feb 96 | 4885 |
| 139 | 19 00.1 S | 170 03.4 W | 26 Feb 96 | 3000 |
| 140 | 18 30.3 S | 170 00.1 W | 26 Feb 96 | 5232 |
| 141 | 17 60.0 S | 169 60.0 W | 26 Feb 96 | 4893 |
| 142 | 17 30.1 S | 169 60.0 W | 26 Feb 96 | 5002 |
| 143 | 17 00.1 S | 169 59.8 W | 27 Feb 96 | 4954 |
| 144 | 16 30.3 S | 169 59.9 W | 27 Feb 96 | 5109 |
| 145 | 16 00.2 S | 169 59.9 W | 27 Feb 96 | 5120 |
| 146 | 15 29.8 S | 170 00.1 W | 27 Feb 96 | 5064 |
| 147 | 15 00.2 S | 170 00.0 W | 28 Feb 96 | 4803 |
| 148 | 14 40.0 S | 169 59.9 W | 28 Feb 96 | 3322 |
| 149 | 14 16.9 S | 169 59.8 W | 28 Feb 96 | 3540 |
| 150 | 13 58.3 S | 169 60.0 W | 28 Feb 96 | 2947 |
| 151 | 13 49.1 S | 170 00.1 W | 28 Feb 96 | 4297 |
| 152 | 13 30.1 S | 169 60.0 W | 29 Feb 96 | 4860 |
| 153 | 12 59.9 S | 170 00.0 W | 29 Feb 96 | 4949 |
| 154 | 12 29.9 S | 169 59.9 W | 29 Feb 96 | 4979 |
| 155 | 12 00.1 S | 170 00.1 W | 29 Feb 96 | 5055 |
| 156 | 11 30.0 S | 169 59.9 W | 1 Mar 96 | 5035 |
| 157 | 11 00.1 S | 169 59.9 W | 1 Mar 96 | 5100 |
| 158 | 10 30.1 S | 169 59.8 W | 1 Mar 96 | 4858 |
| 159 | 09 55.6 S | 169 37.7 W | 1 Mar 96 | 5179 |
| 160 | 09 30.1 S | 168 59.9 W | 2 Mar 96 | 5310 |
| 161 | 08 59.9 S | 168 52.6 W | 2 Mar 96 | 4848 |
| 162 | 08 29.9 S | 168 44.9 W | 2 Mar 96 | 5129 |
| 163 | 08 00.0 S | 168 37.0 W | 2 Mar 96 | 5138 |
| 164 | 07 30.1 S | 168 44.9 W | 3 Mar 96 | 5244 |
| 165 | 06 60.0 S | 168 44.9 W | 3 Mar 96 | 5628 |
| 166 | 06 30.1 S | 168 44.9 W | 3 Mar 96 | 5498 |
| 167 | 06 00.0 S | 168 45.0 W | 4 Mar 96 | 5629 |
| 168 | 05 30.1 S | 168 45.0 W | 4 Mar 96 | 5347 |
| 169 | 05 00.0 S | 168 44.9 W | 4 Mar 96 | 5534 |
| 170 | 03 60.0 S | 168 45.1 W | 4 Mar 96 | 5191 |
| 171 | 03 00.0 S | 168 45.0 W | 5 Mar 96 | 5347 |
| 172 | 02 00.1 S | 168 45.0 W | 5 Mar 96 | 3293 |
| 173 | 01 00.1 S | 168 45.2 W | 6 Mar 96 | 5748 |
| 174 | 00 00.1 S | 168 45.0 W | 6 Mar 96 | 5542 |
| -· · | | | | |

| STATION | | | | BOTTOM |
|---------|-----------|------------|-------------|-----------|
| NUMBER | Latitude | Longitude | <u>Date</u> | DEPTH (M) |
| 175 | 07 44.8 S | 168 40.2 W | 8 Mar 96 | 5289 |
| 176 | 08 15.1 S | 168 41.3 W | 8 Mar 96 | 4944 |
| 177 | 10 08.7 S | 168 58.8 W | 8 Mar 96 | 4628 |
| 178 | 10 04.1 S | 169 12.7 W | 8 Mar 96 | 5226 |
| 179 | 09 55.2 S | 169 37.7 W | 9 Mar 96 | 5188 |
| 180 | 09 47.0 S | 170 03.5 W | 9 Mar 96 | 4993 |
| 181 | 09 41.6 S | 170 19.5 W | 9 Mar 96 | 4297 |
| 182 | 09 35.7 S | 170 36.1 W | 9 Mar 96 | 4038 |

APPENDIX 2: ALACE Float Deployment Locations on P14s and P15S: CGC96 Station Locations: Leg 1

| STATION | | | | |
|---------|-----------------|------------|-------------------------------|---------------|
| NUMBER | <u>Latitude</u> | Longitude | Date | <u>Time</u> |
| 1 | 56 29.7 S | 173 32.4 E | $11 \overline{\text{Jan}} 96$ | 0323 |
| 2 | 59 27.5 S | 173 57.9 E | 12 Jan 96 | 0035 |
| 3 | 60 29.7 S | 170 01.3 W | 22 Jan 96 | 0606 Profiler |
| 4 | 57 30.1 S | 170 00.7 W | 23 Jan 96 | 2120 Profiler |
| 5 | 55 29.5 S | 170 01.9 W | 24 Jan 96 | 2321 Profiler |
| 6 | 53 59.5 S | 169 59.3 W | 25 Jan 96 | 1545 Profiler |
| 7 | 52 00.0 S | 170 05.7 W | 26 Jan 96 | 0155 Profiler |
| 8 | 50 00.4 S | 170 00.4 W | 28 Jan 96 | 0502 Profiler |
| 9 | 47 29.5 S | 169 58.6 W | 29 Jan 96 | 1505 |
| 10 | 45 10.6 S | 172 43.8 W | 31 Jan 96 | 0701 |
| 11 | 42 23.7 S | 174 24.6 W | 1 Feb 96 | 2143 |
| 12 | 39 04.4 S | 172 06.8 W | 14 Feb 96 | 1820 |
| 13 | 29 59.2 S | 169 59.5 W | 20 Feb 96 | 0125 |
| 14 | 24 29.9 S | 170 00.1 W | 22 Feb 96 | 0252 |

APPENDIX 3. CTD/O2 techniques on WOCE P14S and P15S (CGC96)

1. Introduction:

A detailed discussion of the CTD data and calibration techniques is given in the CGC96 CTD data report and .ctd files submitted to the WHP Office, and in the publication:

McTaggart, K.E. and and G.C. Johnson (1997). CTD/O2 Measurements Collected on a Climate & Global Change Cruise (WOCE Sections P14S and P15S) During January -March, 1996. NOAA Data Report ERL PMEL-63, Pacific Marine Environmental Laboratory, Seattle. Washington, September 1997.

2. STANDARDS AND PRE-CRUISE CALIBRATIONS

The CTD/O2 system is a real time data system with the data from a Sea-Bird Electronics, Inc. (SBE) 9plus underwater unit transmitted via a conducting cable to the SBE 11plus deck unit. The serial data from the underwater unit is sent to the deck unit in RS-232 NRZ format using a 34560 Hz carrier-modulated differential-phase-shift-keying (DPSK) telemetry link. The deck unit decodes the serial data and sends it to a personal computer for display and storage in a disk file using Sea-Bird SEASOFT software.

The SBE 911plus system transmits data from primary and auxiliary sensors in the form of binary number equivalents of the frequency or voltage outputs from those sensors. The calculations required to convert from raw data to engineering units of the parameters being measured are performed by software, either in real-time, or after the data has been stored in a disk file.

The SBE 911plus system is electrically and mechanically compatible with standard unmodified rosette water samplers made by General Oceanics (GO), including the 1016 36-position sampler, which was used for most stations on this cruise. An optional modem and rosette interface allows the 911plus system to control the operation of the rosette directly without interrupting the data from the CTD, eliminating the need for a rosette deck unit.

The SBE 9plus underwater unit uses Sea-Bird's standard modular temperature (SBE 3) and conductivity (SBE 4) sensors which are mounted with a single clamp and "L" bracket to the lower end cap. The conductivity cell entrance is co-planar with the tip of the temperature sensor's protective steel sheath. The pressure sensor is mounted inside the underwater unit main housing and is ported to outside pressure through the oil-filled plastic capillary tube seen protruding from the main housing bottom end cap. A compact, modular unit consisting of a centrifugal pump head and a brushless DC ball bearing motor contained in an aluminum underwater housing pump flushes water through sensor tubing at a constant rate independent of the CTD's motion. This improves dynamic performance.

Motor speed and pumping rate (3000 rpm) remain nearly constant over the entire input voltage range of 12-18 volts DC.

The SBE 11plus deck unit is a rack-mountable interface which supplies DC power to the underwater unit, decodes the serial data stream, formats the data under microprocessor control, and passes the data to a companion computer. It provides access to the modem channel and control of the rosette interface. Output data is in RS-232 (serial) format.

2.1 Conductivity

The flow-through conductivity-sensing element is a glass tube (cell) with three platinum electrodes. The resistance measured between the center electrode and end electrode pair is determined by the cell geometry and the specific conductance of the fluid within the cell, and controls the output frequency of a Wien Bridge circuit. The sensor has a frequency output of approximately 3 to 12 kHz corresponding to conductivity from 0 to 7 S/m (0 to 70 mmho/cm). The SBE 4 has a typical accuracy/stability of +/- 0.0003 S/m/month; resolution of 0.00004 S/m at 24 samples per second; and 6800 meter anodized aluminum housing depth rating.

Pre-cruise sensor calibrations were performed at Sea-Bird Electronics, Inc. in Bellevue, Washington. The following coefficients were entered into SEASOFT using software module SEACON:

| S/N 748 S/N 1561 | S/N 1562 | |
|---------------------|---------------------|---------------------|
| December 14, 1995 | December 14, 1995 | December 14, 1995 |
| g = -4.13299236 | g = -4.09205330 | g = -4.16899749 |
| h = 4.36576287e-01 | h = 5.28538155e-01 | h = 5.53740992e-01 |
| i = -1.39236118e-04 | i = -1.56949585e-04 | i = -5.94323544e-05 |
| j = 2.59599092e-05 | j = 3.46776288e-05 | j = 3.11836344e-05 |
| ctcor = 3.2500e-06 | ctcor = 3.2500e-06 | ctcor = 3.2500e-06 |
| cpcor = -9.5700e-08 | cpcor = -9.5700e-08 | cpcor = -9.5700e-08 |
| | | |

Conductivity calibration certificates show an equation containing the appropriate pressuredependent correction term to account for the effect of hydrostatic loading (pressure) on the conductivity cell:

$$C (S/m) = (af^m + bf^2 + c + dt) / [10 (1 - 9.57e-08 p)]$$

where a, b, c, d, and m are the calibration coefficients above, f is the instrument frequency (kHz), t is the water temperature (C), and p is the water pressure (dbar). SEASOFT automatically implements this equation.

2.2 Temperature

The temperature-sensing element is a glass-coated thermistor bead, pressure-protected by a stainless steel tube. The sensor output frequency ranges from approximately 5 to 13

kHz corresponding to temperature from -5 to 35 C. The output frequency is inversly proportional to the square root of the thermistor resistance which controls the output of a patented Wien Bridge circuit. The thermistor resistance is exponentially related to temperature. The SBE 3 thermometer has a typical accuracy/stability of +/- 0.004 C per year; and resolution of 0.0003 C at 24 samples per second. The SBE 3 thermometer has a fast response time of 70 ms. It's anodized aluminum housing provides a depth rating of 6800 m.

Pre-cruise sensor calibrations were performed at Sea-Bird Electronics, Inc. in Bellevue, Washington. The following coefficients were entered into SEASOFT using software module SEACON:

| S/N 1370 | S/N 2038 | S/N 2037 |
|--------------------|--------------------|--------------------|
| November 22, 1995 | December 14, 1995 | December 14, 1995 |
| g = 4.84042876e-03 | g = 4.11396861e-03 | g = 4.13135090e-03 |
| h = 6.74974915e-04 | h = 6.20923913e-04 | h = 6.33482482e-04 |
| i = 2.38622986e-05 | i = 1.98024796e-05 | i = 2.11340704e-05 |
| j = 1.66698127e-06 | j = 1.99224715e-06 | j = 2.16252937e-06 |
| f0 = 1000.0 | f0 = 1000.0 | f0 = 1000.0 |

Temperature (IPTS-68) is computed according to

$$T(C) = 1/{a+b[ln(f0/f)]+c[ln^2(f0/f)]+d[ln^3(f0/f)]}-273.15$$

where a, b, c, d, and f0 are the calibration coefficients above and f is the instrument frequency (kHz). SEASOFT automatically implements this equation.

2.3 Pressure

The Paroscientific series 4000 Digiquartz high pressure transducer uses a quartz crystal resonator whose frequency of oscillation varies with pressure induced stress measuring changes in pressure as small as 0.01 parts per million with an absolute range of 0 to 10,000 psia (0 to 6885 dbar). Also, a quartz crystal temperature signal is used to compensate for a wide range of temperature changes. Repeatability, hysteresis, and pressure conformance are 0.005% FS. The nominal pressure frequency (0 to full scale) is 34 to 38 kHz. The nominal temperature frequency is 172 kHz + 50 ppm/degree Celsius.

Pre-cruise sensor calibrations were performed at Sea-Bird Electronics, Inc. in Bellevue, Washington. The following coefficients were entered into SEASOFT using software module SEACON:

| S/N 53960 | S/N 53586 |
|------------------------------|----------------------|
| April 11, 1995 | October 29, 1993 |
| c1 = -4.315048e + 04 | c1 = -3.920451e + 04 |
| c2 = 4.542800e-01 c2 = 6 | 5.234560e-01 |
| c3 = 1.344380e-02 c3 = 1 | .350570e-02 |
| d1 = 3.795200e-02 d1 = 3 | 3.894300e-02 |
| d2 = 0.0 d2 = 0.0 | |
| t1 = 3.034230e + 01 | t1 = 3.046303e+01 |
| t2 = -1.809380e-04 | t2 = -9.018862e-05 |
| $t3 = 4.616150e-06 \ t3 = 4$ | l.528890e-06 |
| $t4 = 2.084220e-09 \ t4 = 3$ | 3.309590e-09 |

Pressure coefficients are first formulated into

$$c = c1 + c2*U + c3*U^2$$
 $d = d1 + d2*U$ $t0 = t1 + t2*U + t3*U^2 + t4*U^3$

where U is temperature in degrees Celsius. Then pressure is computed according to

$$P (psia) = c * [1 - (t0^2/t^2)] * {1 - d[1 - (t0^2/t^2)]}$$

where t is pressure period (us). SEASOFT automatically implements this equation.

2.4 Oxygen

The SBE 13 dissolved oxygen sensor uses a Beckman polarographic element to provide in-situ measurements at depths up to 6800 meters. This auxiliary sensor is also included in the path of pumped sea water. Oxygen sensors determine the dissolved oxygen concentration by counting the number of oxygen molecules per second (flux) that diffuse through a membrane. By knowing the flux of oxygen and the geometry of the diffusion path the concentration of oxygen can be computed. The permeability of the membrane to oxygen is a function of temperature and ambient pressure. The interface electronics outputs voltages proportional to membrane current (oxygen current) and membrane temperature (oxygen temperature). Oxygen temperature is used for internal temperature compensation. Computation of dissolved oxygen in engineering units is done in the software. The range for dissolved oxygen is 0 to 650 µmol/kg; accuracy is 4umol/kg; resolution is 0.4 umol/kg. Response times are 2 s at 25°C and 5 s at 0°C.

The following oxygen calibrations were entered into SEASOFT using SEACON:

```
S/N 130309

September 28, 1995

m = 2.4544 e-07

b = -4.6633 e-10

soc = 2.6721

boc = -0.0178

tcor = -3.3e-02

pcor = 1.5e-04

tau = 2.0

wt = 0.67

k = 8.9224

c = -6.9788
```

The use of these constants in linear equations of the form I = mV + b and T = kV + c will yield sensor membrane current and temperature (with a maximum error of about 0.5 degrees C) as a function of sensor output voltage. These scaled values of oxygen current and oxygen temperature were carried through the SEASOFT processing stream unaltered.

3. DATA ACQUISITION

CTD/O2 measurements were made using one of two Seabird 9plus CTDs each equipped with a fixed pumped temperature-conductivity (TC) sensor pair. A mobile pumped TC pair with dissolved oxygen sensor was mounted on whichever CTD was in use so that dual TC measurements and dissolved oxygen measurements were always collected. The TC pairs were monitored for calibration drift and shifts by examining the differences between the two pairs on each CTD and comparing CTD salinities with bottle salinity measurements.

PMEL's Sea-Bird 9plus CTD/O2 S/N 09P8431-0315 (sampling rate 24 Hz) was mounted in a 36-position frame and employed as the primary package. Auxiliary sensors included a lowered ADCP, Metrox load cell, and Benthos altimeter. Water samples were collected using a General Oceanics 36-bottle rosette and 10-liter Nisken bottles. The primary package was used for the majority of 182 casts.

PMEL's Sea-Bird 9plus CTD/O2 S/N 329053-0209 (sampling rate 24 Hz) was mounted in a 24-position frame and employed as the backup package. Auxiliary sensors included a Metrox load cell and Benthos altimeter. Water samples were collected using a Sea-Bird 24-bottle rosette, and 4-liter Niskin bottles. One test cast and 22 bad-weather stations were made using the smaller backup package.

The package entered the water from the stern of the ship and was held 5-15 m beneath the surface for one minute in order to activate the pump and attach tag lines for package recovery. Under ideal conditions the package was lowered at a rate of 30 m/min to 50 m, 45 m/min to 200 m, and 60 m/min to depth. Ship heave often caused substantial variation about these mean lowering rates, especially at southern ocean stations. Load cell values were monitored in real-time during each cast. The position of the package relative to the bottom was monitored on the ship's Precision Depth Recorder (PDR) and an altimeter. A bottom depth was estimated from bathymetric charts and the PDR ran during the bottom 1000 m of the cast. Stations were generally made to within 10 m of the bottom, sometimes farther away in heavy weather. Fig. 2 shows the depths of bottle closures during the upcast.

Upon completion of the cast, sensors were flushed with deionized water and stored with a dilute Triton-X solution in the plumbing. Niskin bottles were then sampled for various water properties detailed in the introduction. Sample protocols conformed to those specified by the WOCE Hydrographic Programme.

A Sea-Bird 11plus deck unit received the data signal from the CTD. The analog data stream was recorded onto video cassette tape as a backup. Digitized data were forwarded to a 286-AT personal computer equipped with SEASOFT acquisition and processing software version 4.216. Temperature, salinity, and oxygen profiles were displayed in real-time. Raw data files were transferred to a 486 personal computer using Laplink version 3 and backed up to optical disk.

3.1 Data Acquisition Problems

Some time was lost at the beginning of leg 1 owing to level-wind problems on the primary winch. The sea cable was retensioned on the drum at sea by removing the CTD/rosette package, attaching a weight to the cable, and spooling the full length of cable behind the ship while underway to within the last full wrap on the drum . Level-wind problems were much reduced after this procedure.

No useful data from the secondary TC pair and dissolved oxygen sensor was collected during station 12 owing to biological fouling of the mobile sensors. Data from the primary TC pair were processed for station 12, as well as for stations 69, 78, 79, 128, 130, 131, and 159 owing to noise. No oxygen data are available for stations 132, 133, 134, and 144 during which problems with the dissolved oxygen sensor were being diagnosed and repaired.

3.2 Salinity Analyses

Bottle salinity analyses were performed in the ship's salinity laboratory using two Guildline Model 8400A inductive autosalinometers standardized with IAPSO Standard Seawater batch P114. The autosalinometer in use was standardized before each run and either at the end of each run or after no more than 48 samples. The drift between standardizations was monitored and the individual samples were corrected for that drift by linear interpolation. Duplicate samples taken from the deepest bottle on each cast were analyzed on a subsequent day. Bottle salinities were compared with preliminary CTD

salinities to aid in identification of leaking bottles as well as to monitor the CTD conductivity cells' performance and drift.

The expected precision of the autosalinometer with an accomplished operator is 0.001 PSS, with an accuracy of 0.003. To assess the precision of discrete salinity measurements on this cruise, a comparison was made for data from the instances in which two bottles were tripped within 10 dbar of each other at the same station below a depth of 2000 dbar. For the 124 instances in which both bottles of the pair have acceptable salinity measurements, the standard deviation of the differences is 0.0008 PSS. This value is below the expected precision.

4. AT SEA PROCESSING

SEASOFT consists of modular menu driven routines for acquisition, display, processing, and archiving of oceanographic data acquired with Sea-Bird equipment and is designed to work with an IBM or compatible personal computer. Raw data is acquired from the instruments and is stored as unmodified data. The conversion module DATCNV uses the instrument configuration and calibration coefficients to create a converted engineering unit data file that is operated on by all SEASOFT post processing modules. Each SEASOFT module that modifies the converted data file adds information to the header of the converted file permitting tracking of how the various oceanographic parameters were obtained. The converted data is stored in either rows and columns of ascii numbers or as a binary data stream with each value stored as a 4 byte binary floating point number. The last data column is a flag field used to mark scans as good or bad.

The following are the SEASOFT processing module sequence and specifications used in the reduction of P14S/P15S CTD/O2 data:

DATCNV

converted the raw data to pressure, temperature, conductivity, oxygen current, and oxygen temperature; and computed salinity and the time rate of change of oxygen current. DATCNV also extracted bottle information where scans were marked with the bottle confirm bit during acquisition.

ROSSUM

created a summary of the bottle data. Bottle position, date, and time were output as the first two columns. Pressure, temperature, conductivity, salinity, oxygen current, oxygen temperature, and time rate of change of oxygen current were averaged over a 2-s interval (48 scans). For the primary package, the time interval was from 5 to 3 s prior to the confirm bit in order to avoid spikes in conductivity and oxygen current owing to minor incompatibilities between the Sea-Bird 911plus CTD/O2 system and General Oceanics 1016 rosette. Bottle data from the backup package were averaged from 1 s prior to the confirm bit to 1 s after the confirm bit in the data stream. ROSSUM computed CTD oxygen, potential temperature, and sigma-theta.

WILDEDIT marked extreme outliers in the data files. The first pass of WILDEDIT obtained an accurate estimate of the true standard deviation of the data. The data were read in blocks of 200 scans. Data greater than two standard deviations were flagged. The second pass computed a standard deviation over the same 200 scans excluding the flagged values. Values greater than 16 standard deviations were marked bad.

SPLIT removed decreasing pressure records from the data files leaving only the downcast.

FILTER performed a low pass filter on pressure with a time constant of 0.15 s. In order to produce zero phase (no time shift) the filter first runs forward through the file and then runs backwards through the file.

ALIGNCTD aligned conductivity in time relative to pressure to ensure that all calculations were made using measurements from the same parcel of water.

- Conductivity for the primary sensor on the 36-bottle package was advanced by -0.020 s.
- Conductivity for the primary sensor on the 24-bottle package was advanced by -0.010 s.
- Conductivity for the secondary, mobile sensor on either package was advanced 0.055 s.

CELLTM used a recursive filter to remove conductivity cell thermal mass effects from the measured conductivity. For C748 with an epoxy coating, the thermal anomaly amplitude (alpha=0.03) and the time constant (1/beta=9.0) were higher than for C1561 and C1562 with no coating (alpha=0.02, 1/beta=7.0).

DERIVE was used to compute fall rate (m/s) with a time window size for fall rate and acceleration of 2.0 seonds.

LOOPEDIT marked scans where the CTD was moving less than the minimum velocity of 0.25 m/s or travelling backwards due to ship roll.

BINAVG averaged the data into 1-dbar pressure bins starting at 1 dbar with no surface bin. The center value of the first bin was set equal to the bin size. The bin minimum and maximum values are the center value +/- half the bin size. Scans with pressures greater than the minimum and less than or equal to the maximum were averaged. Scans were interpolated so that a data record exists every decibar.

STRIP removed scan number and fall rate from the data files. TRANS converted the data file format from binary to ascii.

5. POST-CRUISE CALIBRATIONS

Post-cruise sensor calibrations were done at Sea-Bird Electronics, Inc. during May 1996. Mobile, secondary sensor pair T1370 and C748 were selected for final data reduction for all stations except 12, 69, 128, 130, 131, and 159. Post-cruise calibrations showed T1370 to have drifted by 0.43e-03 C over the 3.2 months between calibrations. Station 12 data are from sensors T2037 and C1562. Post-cruise calibrations showed T2037 to have drifted by -0.28e-03 C over the 3.2 months between calibrations. The remaining station data are from sensors T2038 and C1561. Post-cruise calibrations showed T2038 to have drifted by 0.11e-03 C over the 3.3 months between calibrations.

5.1 Conductivity

SEASOFT module ALIGNCTD was used to align conductivity measurements in time relative to pressure. Measurements can be misaligned due to the inherent time delay of the sensor response, the water transit time delay in the pumped plumbing line, and the sensors being physically misaligned in depth. Because SBE 3 temperature response is fast (0.06 s), it is not necessary to advance temperature relative to pressure. When measurements are properly aligned, salinity spiking and density errors are minimized.

For a SBE 9 CTD with ducted TC sensors and a 3000 rpm pump the typical net advance of conductivity relative to temperature is 0.073 s. The SBE 11 deck units advanced primary conductivity 0.073 s but do not advance secondary conductivity. Therefore the alignment of C748 conductivity data, which was from the secondary sensor channel (except for stations 78 and 79), was much larger, typically 0.06 s versus coming from a primary sensor channel, typically 0.02 s.

Conductivity slope and bias, along with a linear pressure term (modified beta), were computed by a least-squares minimization of CTD and bottle conductivity differences. The function minimized was

where BC is bottle conductivity (S/m), CC is pre-cruise calibrated CTD conductivity (S/m), CP is the CTD pressure (dbar), m is the conductivity slope, b is the bias (S/m), and beta is a linear pressure term (S/m/dbar). The final CTD conductivity (S/m) is

The slope term m is a fourth-order polynomial function of station number to allow the entire cruise to be fit at once with a smoothly-varying station- dependent slope correction. For sensors C748 and C1561 a series of fits were made, each fit throwing out bottle values for locations having a residual between CTD and bottle conductivities greater than three standard deviations. This procedure was repeated with the remaining bottle values until no more bottle values were thrown out.

For C748, the slope correction ranged from 1.0000501 to 1.0001274, the bias applied was -7.5e-04, and the beta term was -9.01e-09. Of 5680 bottles, the percentage of bottles retained in the fit was 85.2 with a standard devia- tion of CTD versus bottle conductivity differences of 9.88e-05 S/m. For C1561, the slope correction ranged from 1.0001481 to 1.0002849, the bias applied was -3.8e-04, and the beta term was -3.16e-09. Of 5118 bottles, the percentage of bottles retained in the fit was 88.1 with a standard deviation of 9.93e-05 S/m.

For station 12, station 13 calibrated secondary salinity data was used as a reference. A slope, bias, and pressure correction was determined that matched station 13 uncalibrated primary salinity (C1562,T2037) to station 13 calibrated secondary salinity (C748,T1370). These coefficients (slope=1.004, bias=-0.0011, beta=-2.49e-08) were used to calibrate station 12 primary salinity (C1562,T2037).

CTD-bottle conductivity are plotted against cast number to show the stability of the calibrated CTD conductivities relative to the bottle conductivities (McTaggart and Johnson, 1997; Fig. 3, upper panel). CTD-bottle conductivity differences are plotted against pressure to show the tight fit below 800 m and the increasing scatter above 800 m (McTaggart and Johnson, 1997; Fig. 3, lower panel).

5.2 Temperature

Adjustments were made to the bias of the thermistors as deviations from the pre-cruise calibrations on a station by station basis. These deviations were obtained from a linear fit of the pre-cruise and post-cruise temperature residuals from the pre-cruise calibration versus time.

A pressure correction was then applied to each sensor such that

where CT is CTD temperature (C) with the bias adjustment, pcor is the pressure correction (dbar) for each sensor, and CP is CTD pressure (dbar).

```
pcor1370 = -2.6e-03/9000 = -2.8889e-007

pcor2037 = -2.3e-03/9000 = -2.5556e-007

pcor2038 = -1.7e-03/9000 = -1.8889e-007
```

Also, a uniform correction is applied for heating of the thermistor owing to viscous effects. All the thermistors are biased high by this effect and were adjusted down accordingly. An adjustment of 0.6e-03 C results in errors of no more than +-0.15 C from this effect for the full range of oceanographic temperature and salinity.

Post-cruise temperature and conductivity calibrations were applied to all sensor pairs using PMEL program CALCTD (STA12CAL for station 12). Surface values were filled using PMEL program FILLSFC. FILLSFC copied the first good value of salinity and

potential temperature back to the surface and then back- calculated temperature and conductivity. Primary and secondary sensor differences were examined. Data from the secondary sensor pair (T1370/C748) was chosen for all stations except 12, 69, 78, 79, 128, 130, 131, and 159. Primary sensor data chosen for these 8 stations were within .001 psu of the secondary sensor data of the surrounding stations. All profiles were despiked and data linearly interpolated using PMEL program DESPIKE.

Package slowdowns and reversals owing to ships heave can move mixed water in tow to in front of the CTD sensors and obscure measurements. In addition to SEASOFT module LOOPEDIT (see below), PMEL program DELOOP computed values of density locally referenced between every 1 dbar of pressure to compute $N^2 = (-g/rho)(drho/dz)$ and linearly interpolated over those records where $N^2 <= -1.0e-05 \text{ s}^{-1}$.

Post-cruise calibrations were applied to CTD data associated with bottle data using PMEL program CALMSTR. CALMSTR also ammended WOCE quality flags associated with CTD and bottle salinities. Eighteen CTD salinities were flagged as bad during station 78 likely owing to clogged plumbing of the primary sensors during the up-cast. Of the 5640 bottle salinities, 0.33% were flagged as bad and 2.68% were flagged as questionable.

5.3 Oxygen

In situ oxygen samples collected during CTD profiles are used for post-measurement calibration. Calibrated CTD data associated with bottle data were merged with bottle oxygen data flagged as 'good'. Because the dissolved oxygen sensor has an obvious hysteresis, program OXDWNP replaced up-profile water sample data with corresponding down-profile CTD/O2 data at common pressure levels. The time rate of change of oxygen current was computed using 2 second intervals in SEASOFT and smoothed using a median filter of width 5 dbar prior to OXDWNP. Oxygen saturation values were computed according to Benson and Krause (1984) in units of umol/kg.

The algorithm used for converting oxygen sensor current and probe temperature measurements to oxygen as described by Owens and Millard (1985) requires a non-linear least squares regression technique in order to determine the best fit coefficients of the model for oxygen sensor behavior to the water sample observations. WHOI program OXFITMR uses Numerical Recipes (Press et al., 1986) Fortran routines MRQMIN, MRQCOF, GAUSSJ, and COVSRT to perform non-linear least squares regression using Levenberg-Marquardt method. A Fortran subroutine FOXY describes the oxygen model with the derivatives of the model with respect to six coefficients in the following order: oxygen current slope, temperature correction, pressure correction, weight, oxygen current bias, and oxygen current lag.

Program OXFITMR reads the data for a group of stations. The data are editted to remove spurious points where values are less than zero or greater than 1.2 times the saturation value. The routine varies the six (or fewer) parameters of the model in such a way as to produce the minimum sum of squares in the difference between the calibration oxygens and the computed values. Individual differences between the calibration oxygens and the

computed oxygen values (residuals) are then compared with the standard deviation of the residuals. Any residual exceeding an edit factor of 2.8 standard deviations is rejected. A factor of 2.8 will have a 0.5% chance of rejecting a valid oxygen value for a normally distributed set of residuals. The iterative fitting process is continued until none of the data fail the edit criteria. The best fit to the oxygen probe model coefficients is then determined. Coefficents were applied by PMEL program CALOX2W and CTD oxygen was computed using subroutine OXY6W.

By plotting the oxygen residuals versus station, appropriate station groupings for further refinements of fitting were obtained by looking for abrupt station to station changes in the residuals. For each grouping, two sets of coefficients were determined, one fitting all the bottles and a second fitting only bottles deeper than just above the median bottle oxygen minimum. Sometimes it was necessary to fix values of some oxygen algorithm parameters to keep those parameters within a reasonable range (noted by asterisks in Table 2). Final coefficients were applied to downcast data using PMEL program OXYCALC; and to bottle data using OXYCALB. The two sets of coefficients were blended at the oxygen minimum using a set of hyperbolic tangent functions with 250-dbar decay scales.

CTD oxygen values were despiked using PMEL program CLEANOX. Bad CTD oxygen data were flagged for all of station 12 owing to clogged plumbing, parts of stations 127-131 where the dissolved oxygen module failed in the deep water (the dissolved oxygen module was replaced prior to station 135), and stations 177-182 above 2850 dbar where no shallow bottle data were available to calibrate the sensor.

CTD-bottle oxygen differences are plotted against station number to show the stability of the calibrated CTD oxygens relative to the bottle oxygens (McTaggart and Johnson, 1997; Fig. 4, upper panel). CTD-bottle oxygen differences are plotted against pressure to show the tight fit below 1200 m and the increasing scatter above 1200 m (McTagart and Jihnson, 1997; Fig. 4, lower panel).

PMEL program P15_EPIC converted finalized CTD data files into EPIC format (Soreide, 1995); and computed ITS-90 temperature, ITS-90 potential temperature, and dynamic height. EPIC datafiles contain a WOCE quality flag parameter associated with pressure, temperature, salinity, and CTD oxygen. Quality flag definitions can be found in the WOCE Operations Manual (1994).

 Table 1. CTD cast summary.

| STN | LATITUDE | LONGITUDE | | DATE | | TIME | W/D T | W/S (kts) | DEPTH (m) | HAB* (m) | CAST (db) |
|----------|----------------------|------------------------|----------|------------|----------|-----------------|------------|--------------|--------------|-------------|--------------|
| 4 | 53 0.1S | 169 59.3E | 9 | JAN | 96 | 13 | 270 | 5 | 195 | 12 | 185 |
| 5 | 53 29.9S | 170 29.6E | 9 | JAN | 96 | 342 | 275 | 8 | 732 | 10 | 733 |
| 6 | 53 59.9S | 171 0.1E | 9 | JAN | 96 | 736 | 275 | 10 | 1159 | 10 | 1172 |
| 7 | 54 10.2S | 171 10.9E | 9 | JAN | 96 | 1022 | 320 | 9 | 1346 | 10 | 1368 |
| 8 | 54 19.8S | 171 20.2E | 9 | JAN | 96 | 1338 | 315 | 15 | 2583 | 11 | 2582 |
| 9 | 54 30.3S | 171 29.8E | 9 | JAN | 96 | 1852 | 355 | 16 | 4373 | 9 | 4503 |
| 10 | 54 59.7S | 172 0.7E | 10 | JAN | 96 | 203 | 260 | 19 | 5350 | 5 | 5469 |
| 11 | 55 30.4S | 172 27.0E | 10 | JAN | 96 | 904 | 250 | 38 | | 10 | 5453 |
| 12 | 55 59.8S | 173 0.6E | 10 | JAN | 96 | 1750 | 240 | 27 | 5448 | 10 | 5544 |
| 13 | 56 29.2S | 173 30.2E | 11 | JAN | 96 | 42 | 220 | 20 | 5350 | 0 | 5466 |
| 14 | 56 59.7S | 173 58.6E | 11 | JAN | 96 | 908 | 230 | 17 | 5437 | 10 | 5549 |
| 15 | 57 30.3S | 173 58.5E | 11 | JAN | 96 | 1731 | 275 | 23 | 5368 | 11 | 5425 |
| 16 17 | 58 0.2S 58 30.3S | 173 59.5E 173 58.2E | 12 12 | JAN JAN | 96 96 | <u>1</u> 641 | 300 315 | 18 21 | 5206 5043 | 16 5 | 5308 5108 |
| 18 | 58 59.8S | 173 50.2E | 13 | JAN | 96 | 1344 | 265 | 25 | 5109 | 8 | 5216 |
| 19 | 59 28.7S | 173 59.7E | 13 | JAN | 96 | 2208 | 280 | 30 | 4998 | 18 | 5077 |
| 20 | 59 57.9S | 173 59.7E | 13 | JAN | 96 | 530 | 270 | 34 | 4330 | 40 | 4419 |
| 21 | 60 30.3S | 173 57.8E | 13 | JAN | 96 | 1958 | 285 | 25 | 5016 | 22 | 5107 |
| 22 | 60 59.1S | 173 58.8E | 14 | JAN | 96 | 257 | 315 | 19 | 4692 | 9 | 4774 |
| 23 | 61 30.0S | 174 0.2E | 14 | JAN | 96 | 856 | 340 | 27 | 5025 | 10 | 5134 |
| 24 | 62 0.0S | 173 16.1E | 14 | JAN | 96 | 1631 | 330 | 23 | 4450 | 10 | 4538 |
| 25 | 62 26.9S | 172 35.2E | 14 | JAN | 96 | 2249 | 305 | 26 | 4414 | 12 | 4499 |
| 26 | 62 44.7S | 172 9.0E | 15 | JAN | 96 | 424 | 270 | 30 | 4425 | 39 | 4052 |
| 27 | 63 0.0S | 171 44.9E | 15 | JAN | 96 | 1135 | 295 | 23 | | 10 | 2644 |
| 28 | 63 30.1S | 170 59.6E | 15 | JAN | 96 | 1744 | 5 | 16 | 2374 | 12 | 2391 |
| 29 | 63 59.8S | 171 6.6E | 16 | JAN | 96 | 29 | 10 | 26 | 2551 | 25 | 2534 |
| 30 | 64 40.6S | 170 58.6E | 16 | JAN | 96 | 737 | 330 | 24 | 3430 | 10 | 3457 |
| 31 | 65 20.2S | 171 0.0E | 16 | JAN | 96 | 1459 | 35 | 14 | 3403 | 6 | 3461 |
| 32 | 66 0.9S | 171 1.6E | 17 | JAN | 96 | 11 | 355 | 12 | 3103 | 7 | 3159 |
| 33 | 66 59.6S | 170 0.0W | 18 | JAN | 96 | 1150 | 340 | 18 | 3587 | 10 | 3668 |
| 34 | 66 20.3S | 170 0.0W | 18 | JAN | 96 | 1930 | 325 | 12 | 3384 | 10 | 3431 |
| 35 | 65 39.8S | 170 0.3W 170 0.9W | 19 | JAN | 96 | 114 | 305 | 17 | 3142 | 7 | 3190 |
| 36 37 | 64 59.6S 64 30.1S | 170 0.9W 169 59.9W | 19 19 | JAN JAN | 96 96 | 815 1333 | 265 230 | 23 32 | 2332 | 6 11 | 2905 2357 |
| 38 | 63 59.7S | 170 2.0W | 19 | JAN | 96 | 1858 | 240 | 28 | 2744 | 19 | 2922 |
| 39 | 63 30.1S | 170 2.0V 170 0.3W | | JAN | 96 | 57 | 280 | 23 | 2766 | 12 | 2842 |
| 40 | 62 59.7S | 170 0.5W | 20 | JAN | 96 | 630 | 255 | 17 | 3046 | 12 | 3064 |
| 41 | 62 30.0S | 169 59.8W | 20 | JAN | 96 | 1206 | 310 | 15 | 0010 | 17 | 2473 |
| 42 | 62 0.2S | 169 59.9W | 20 | JAN | 96 | 1806 | 330 | 28 | 3384 | 11 | 3431 |
| 43 | 61 29.5S | 170 0.0W | 21 | JAN | 96 | 37 | 315 | 33 | 3463 | 12 | 3434 |
| 44 | 61 0.1S | 170 0.3W | 21 | JAN | 96 | 2105 | 300 | 15 | 4169 | 30 | 4190 |
| 45 | 60 29.7S | 169 59.6W | 22 | JAN | 96 | 410 | 280 | 34 | 3926 | 10 | 4013 |
| 46 | 60 0.3S | 170 0.3W | 22 | JAN | 96 | 1030 | 310 | 17 | 3702 | 12 | 3747 |
| 47 | 59 30.2S | 169 59.9W | 22 | JAN | 96 | 1702 | 315 | 20 | 4007 | 10 | 4104 |
| 48 | 58 59.9S | 170 0.2W | 22 | JAN | 96 | 2311 | 310 | 18 | 4771 | 10 | 4860 |

| 49 58 29.6S 170 0.8W 23 JAN 96 547 315 17 5188 10 5295 50 57 59.7S 170 0.8W 23 JAN 96 1212 290 13 4119 8 4492 51 57 30.1S 170 0.4W 23 JAN 96 1858 240 9 4998 7 5110 52 57 0.2S 170 0.2W 24 JAN 96 1858 240 9 4998 7 5110 53 56 29S 169 59.8W 24 JAN 96 1352 220 20 5157 7 5236 54 56 0.0S 170 0.0W 24 JAN 96 1352 220 20 5157 7 5236 55 55 29.9S 170 0.0W 24 JAN 96 2050 240 5 4945 9 5049 56 54 59.8S 170 0.1W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 169 59.3W 25 JAN 96 1545 220 16 5009 8 5138 59 53 39S 169 59.6W 25 JAN 96 122 270 | STN | LATITUDE | LONGITUDE | DAT | E | TIME | W/D T | W/S (kts) | DEPTH (m) | HAB* (m) | CAST (db) |
|---|-----|----------|-----------|--------|----|------|----------|--------------|--------------|-------------|-----------|
| 50 57 59,7S 170 0.8W 23 JAN 96 1212 290 13 4119 8 4492 51 57 30.1S 170 0.4W 23 JAN 96 122 240 9 4998 7 5110 52 57 0.2S 170 0.2W 24 JAN 96 122 250 14 5165 8 5261 53 56 29S 169 59.8W 24 JAN 96 751 250 21 5052 9 5159 54 56 0.0S 170 1.8W 24 JAN 96 250 240 5 4945 9 5049 55 55 29.9S 170 0.0W 25 JAN 96 307 285 11 4812 7 4916 57 54 29S 170 0.1W 25 JAN 96 307 285 13 4811 4812 7 4916 <td>49</td> <td>58 29.6S</td> <td>170 0.8W</td> <td>23 JAN</td> <td>96</td> <td>547</td> <td></td> <td></td> <td></td> <td></td> <td></td> | 49 | 58 29.6S | 170 0.8W | 23 JAN | 96 | 547 | | | | | |
| 51 57 30.1S 170 0.4W 23 JAN 96 1858 240 9 4998 7 5110 52 57 0.2S 170 0.2W 24 JAN 96 122 250 14 5165 8 5261 53 56 29S 169 59.8W 24 JAN 96 1352 220 20 5157 7 5236 54 56 0.0S 170 1.8W 24 JAN 96 1352 220 20 5157 7 5236 55 55 29.9S 170 0.0W 24 JAN 96 1352 220 20 5157 7 5236 56 54 59.8S 170 0.0W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 169 59.8W 25 JAN 96 190 285 13 4811 3 4929 58 53 39S 169 59.6W 26 JAN 96 320 280 22 5286 8 5459 61 53 0.0S 170 0.5W | | | | | | | | | | | |
| 53 56 29S 169 59.8W 24 JAN 96 751 250 21 5052 9 5159 54 56 0.0S 170 1.8W 24 JAN 96 1352 220 20 5157 5236 55 55 29.9S 170 0.0W 24 JAN 96 2050 240 5 4945 9 5049 56 54 59.8S 170 0.0W 25 JAN 96 307 285 11 4812 7 4916 57 54 29S 170 0.1W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 189 59.W 25 JAN 96 1545 290 16 500 8 5138 59 53 39S 169 59.6W 25 JAN 96 320 280 22 5286 8 5459 60 53 19.9S 169 59.6W 26 JAN 96 320 280 22 5286 8 5459 61 53 0.0S 170 0.8W 26 JAN 96 2325 275 | | | | | | | | | 4998 | 7 | |
| 54 56 0.0S 170 1.8W 24 JAN 96 1352 220 20 5157 7 5236 55 55 55 9.9S 170 0.0W 24 JAN 96 2050 240 5 4945 9 5049 56 54 9.9S 170 0.0W 25 JAN 96 307 285 11 4812 7 4916 57 54 29S 170 0.1W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 169 59.3W 25 JAN 96 2122 20 10 5523 60 53 19.9S 169 59.4W 26 JAN 96 225 275 22 5193 9 5298 61 53 0.0S 170 0.5W 26 JAN 96 2325 | 52 | 57 0.2S | 170 0.2W | 24 JAN | 96 | 122 | 250 | 14 | 5165 | 8 | 5261 |
| 55 55 29.9S 170 0.0W 24 JAN 96 2050 240 5 4945 9 5049 56 54 59.8S 170 0.0W 25 JAN 96 307 285 11 4812 7 4916 57 54 29S 170 0.0W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 169 59.3W 25 JAN 96 1545 290 16 5009 8 5138 59 53 39S 169 59.6W 25 JAN 96 2122 270 17 5131 5 5253 60 53 199 59.6W 20 JAN 96 225 275 26 4070 7 5173 62 53 199 59.6W 27 JAN 96 606 270 | 53 | 56 29S | 169 59.8W | 24 JAN | 96 | 751 | 250 | 21 | 5052 | 9 | 5159 |
| 56 54 59.8S 170 0.0W 25 JAN 96 307 285 11 4812 7 4916 57 54 29S 170 0.1W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 169 59.3W 25 JAN 96 1545 290 16 5009 8 5138 59 53 39S 169 59.6W 25 JAN 96 2122 270 17 5131 5 5253 60 53 19.9S 169 59.6W 26 JAN 96 320 280 22 5286 8 5459 61 53 0.0S 170 0.5W 26 JAN 96 325 275 22 5193 9 5298 62 52 29.9S 170 1.8W 26 JAN 96 2325 275 26 4970 10 5067 64 51 30.0S 170 0.2W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1921 250 20 5249 12 5321 66 50 29S 169 59.6W 27 JAN 96 1921 250 <t< td=""><td>54</td><td>56 0.0S</td><td>170 1.8W</td><td>24 JAN</td><td>96</td><td>1352</td><td>220</td><td>20</td><td>5157</td><td>7</td><td>5236</td></t<> | 54 | 56 0.0S | 170 1.8W | 24 JAN | 96 | 1352 | 220 | 20 | 5157 | 7 | 5236 |
| 57 54 29S 170 0.1W 25 JAN 96 900 285 13 4811 3 4929 58 54 0.1S 169 59.3W 25 JAN 96 1545 290 16 5009 8 5138 59 53 39S 169 59.4W 25 JAN 96 2122 270 17 5131 5 5253 60 53 19.9S 169 59.6W 26 JAN 96 320 280 22 5286 8 5459 61 53 0.0S 170 0.5W 26 JAN 96 925 275 22 5193 9 5298 62 52 29.9S 170 1.8W 26 JAN 96 1643 270 27 5070 7 5173 63 52 0.1S 170 7.8W 26 JAN 96 1643 270 27 5070 7 5173 63 52 0.1S 170 0.2W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1937 220 10 5062 15 5129 67 50 0S 169 59.6W 27 JAN 96 1937 220 1 | 55 | 55 29.9S | 170 0.0W | 24 JAN | 96 | 2050 | 240 | 5 | 4945 | 9 | 5049 |
| 58 54 0.1S 169 59.3W 25 JAN 96 1545 290 16 5009 8 5138 59 53 39S 169 59.4W 25 JAN 96 2122 270 17 5131 5 5253 60 53 19.9S 169 59.6W 26 JAN 96 320 228 226 8286 8 5459 61 53 0.0S 170 0.5W 26 JAN 96 925 275 22 5193 9 5298 62 20 15 170 7.8W 26 JAN 96 1643 270 27 5070 7 5173 63 52 0.1S 170 0.2W 27 JAN 96 606 270 26 4754 20 4876 20 5249 12 5321 16 565 51 30.2S 170 | 56 | 54 59.8S | 170 0.0W | 25 JAN | 96 | 307 | 285 | 11 | 4812 | 7 | 4916 |
| 59 53 39S 169 59.4W 25 JAN 96 2122 270 17 5131 5 5253 60 53 19.9S 169 59.6W 26 JAN 96 320 280 22 5286 8 5459 61 53 0.0S 170 0.5W 26 JAN 96 925 275 22 5193 9 5298 62 52 29.9S 170 1.8W 26 JAN 96 1643 270 27 5070 7 5173 63 52 0.1S 170 7.8W 26 JAN 96 606 270 26 4974 10 5067 64 51 30.0S 170 0.2W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1921 250 20 5249 12 5321 66 50 29S 169 59.4W 28 JAN 96 1937 220 10 5052 15 5129 67 50 0S 169 59.4W 28 JA | 57 | 54 29S | | | | | 285 | 13 | 4811 | | |
| 60 53 19.9S 169 59.6W 26 JAN 96 320 280 22 5286 8 5459 61 53 0.0S 170 0.5W 26 JAN 96 925 275 22 5193 9 5298 62 52 29.9S 170 1.8W 26 JAN 96 1643 270 27 5070 7 5173 63 52 0.1S 170 7.8W 26 JAN 96 12325 275 26 4970 10 5067 64 51 30.0S 170 0.4W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1937 220 10 5052 15 5129 67 50 0S 169 59.4W 28 JAN 96 9137 220 10 5052 15 5129 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 169 59.4W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 170 0.3W 29 JAN 96 1633 270 | | | | | | | | | | | |
| 61 53 0.0S 170 0.5W 26 JAN 96 925 275 22 5193 9 5298 62 52 29.9S 170 1.8W 26 JAN 96 12325 275 26 4970 10 5067 64 51 30.0S 170 0.2W 27 JAN 96 202 24 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 169 59.6W 27 JAN 96 1937 220 10 5052 15 5129 66 50 29S 169 59.4W 28 JAN 96 225 210 11 5361 8 5479 67 50 8 19 59.4W 28 JAN 96 1633 | | | | | | | | | | | |
| 62 52 29.9S 170 1.8W 26 JAN 96 1643 270 27 5070 7 5173 63 52 0.1S 170 7.8W 26 JAN 96 2325 275 26 4970 10 5067 64 51 30.0S 170 0.4W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1221 250 20 5249 12 5321 66 50 29S 169 59.6W 27 JAN 96 1221 250 20 5249 12 5321 67 50 0S 169 59.4W 28 JAN 96 225 210 11 5361 8 5479 68 49 30.3S 170 0.9W 28 JAN 96 1633 270 18 5253 10 5409 70 48 59.6S 169 59.4W 28 JAN 96 | | | | | | | | | | | |
| 63 52 0.1S 170 7.8W 26 JAN 96 2325 275 26 4970 10 5067 64 51 30.0S 170 0.2W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1221 250 20 5249 12 5321 66 50 29S 169 59.6W 27 JAN 96 1937 220 10 5052 15 5129 67 50 0S 169 59.4W 28 JAN 96 217 265 15 5217 15 5337 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 68 49 30.3S 169 59.4W 28 JAN 96 <td></td> | | | | | | | | | | | |
| 64 51 30.0S 170 0.2W 27 JAN 96 606 270 26 4754 20 4876 65 51 0.2S 170 0.4W 27 JAN 96 1221 250 20 5249 12 5321 5321 66 50 29S 169 59.6W 27 JAN 96 1937 220 10 5052 15 5129 15 5129 67 50 0S 169 59.4W 28 JAN 96 225 210 11 5361 8 5479 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 169 59.4W 28 JAN 96 1633 270 18 5253 10 5340 70 48 30.0S 170 0.2W 28 JAN 96 1633 270 18 5253 10 5340 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5303 5 5409 72 47 30.3S 169 59.8W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 124 45 6 5292 9 5387 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 173 147 | | | | | | | | | | | |
| 65 51 0.2S 170 0.4W 27 JAN 96 1221 250 20 5249 12 5321 66 50 29S 169 59.6W 27 JAN 96 1937 220 10 5052 15 5129 67 50 0S 169 59.4W 28 JAN 96 225 210 11 5361 8 5479 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 169 59.4W 28 JAN 96 133 270 18 5253 10 5340 70 48 30.0S 170 0.2W 28 JAN 96 2248 310 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 <td></td> | | | | | | | | | | | |
| 66 50 29S 169 59.6W 27 JAN 96 1937 220 10 5052 15 5129 67 50 0S 169 59.4W 28 JAN 96 225 210 11 5361 8 5479 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 169 59.4W 28 JAN 96 1633 270 18 5253 10 5340 70 48 30.0S 170 0.2W 28 JAN 96 2248 310 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1148 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 | | | | | | | | | | | |
| 67 50 0S 169 59.4W 28 JAN 96 225 210 11 5361 8 5479 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 169 59.4W 28 JAN 96 1633 270 18 5253 10 5340 70 48 30.0S 170 0.2W 28 JAN 96 2248 310 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1418 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 <td></td> | | | | | | | | | | | |
| 68 49 30.3S 170 0.9W 28 JAN 96 917 265 15 5217 15 5337 69 48 59.6S 169 59.4W 28 JAN 96 1633 270 18 5253 10 5340 70 48 30.0S 170 0.2W 28 JAN 96 2248 310 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1148 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 1446 100 15 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S | | | | | | | | | | | |
| 69 48 59.6S 169 59.4W 28 JAN 96 1633 270 18 5253 10 5340 70 48 30.0S 170 0.2W 28 JAN 96 2248 310 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1148 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 144 45 6 5292 9 5387 75 45 33.6S 172 16.7W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S | | | | | | | | | | | |
| 70 48 30.0S 170 0.2W 28 JAN 96 2248 310 10 5303 5 5409 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1148 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 49.5W 30 JAN 96 743 50 10 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 | | | | | | | | | | | |
| 71 47 59.8S 170 0.3W 29 JAN 96 531 340 10 5293 10 5400 72 47 30.3S 169 59.8W 29 JAN 96 1148 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 743 50 10 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 | | | | | | | | | | | |
| 72 47 30.3S 169 59.8W 29 JAN 96 1148 45 13 5309 5 5474 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 743 50 10 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 | | | | | | | | | | | |
| 73 47 6.5S 170 27.7W 29 JAN 96 1902 70 6 5391 8 5500 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 743 50 10 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W 1 FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FE | | | | | | | | | | | |
| 74 46 43S 170 54.7W 30 JAN 96 124 45 6 5292 9 5387 75 46 20.0S 171 22.2W 30 JAN 96 743 50 10 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W | | | | | | | | | | | |
| 75 46 20.0S 171 22.2W 30 JAN 96 743 50 10 5101 8 5196 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W 1 FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1627 300 4 1581 9 1595 87 42 44.8S 174 39.3W 1 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 <tr< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<> | | | | | | | | | | | |
| 76 45 57.0S 171 49.5W 30 JAN 96 1446 100 15 5156 9 5250 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W 1 FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W | | | | | | | | | | | |
| 77 45 33.6S 172 16.7W 30 JAN 96 2127 110 9 4968 7 5057 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W I FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 | | | | | | | | | | | |
| 78 45 10.6S 172 44.2W 31 JAN 96 443 180 10 4660 10 4738 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W I FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 </td <td></td> | | | | | | | | | | | |
| 79 44 50.1S 173 8.2W 31 JAN 96 1035 230 15 3832 10 3869 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W I FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 520 330 12 3118 6 3162 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 80 44 31.8S 173 29.4W 31 JAN 96 1707 230 16 3397 10 3452 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W I FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 | | | | | | | | | | | |
| 81 44 19.2S 173 44.7W 31 JAN 96 2119 225 10 3077 9 3115 82 44 9S 173 56.3W I FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 4 | | | | | | | | | | | |
| 82 44 9S 173 56.3W I FEB 96 106 280 5 1897 10 1911 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 | | | | | | | | | | | |
| 83 43 50S 174 17.7W 1 FEB 96 434 250 11 946 10 959 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 84 43 38.8S 174 32.2W 1 FEB 96 710 0 0 790 10 789 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 85 43 15.2S 174 59.9W 1 FEB 96 1023 280 9 788 12 785 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 86 42 55S 174 47.2W 1 FEB 96 1328 270 5 1054 10 1055 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 87 42 44.8S 174 39.3W 1 FEB 96 1627 300 4 1581 9 1595 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 88 42 24.1S 174 24.4W 1 FEB 96 2014 315 7 2654 10 2677 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 89 42 10.1S 174 15.0W 2 FEB 96 6 350 10 2862 7 2889 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 90 41 42.8S 173 56.5W 2 FEB 96 520 330 12 3118 6 3162 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| 91 41 16.0S 173 38.7W 2 FEB 96 1014 325 12 3319 6 3353 | | | | | | | | | | | |
| | | | | | | | | | | | |
| 32 4043.00 1/3 13.0VV 2 FED 30 1040 330 14 4109 0 4239 | 92 | 40 49.5S | 173 19.5W | 2 FEB | | 1545 | 330 | 14 | 4169 | 6 | 4239 |
| 93 40 23.6S 173 2.0W 2 FEB 96 2056 345 18 4574 9 4652 | | | | | | | | | | | |
| 94 40 23.5S 173 1.7W 13 FEB 96 2049 130 15 4574 4 4658 | | | | | | | | | | 4 | |
| 95 39 57.7S 172 42.2W 14 FEB 96 326 150 22 4738 8 4823 | 95 | 39 57.7S | 172 42.2W | 14 FEB | 96 | 326 | 150 | 22 | 4738 | 8 | 4823 |

| STN | LATITUDE | LONGITUDE | DATE | TIME | W/D T | W/S (kts) | DEPTH (m) | HAB* (m) | CAST (db) |
|-------------|----------------------|-----------------------|------------------------|------------|-----------|--------------|--------------|-------------|--------------|
| 96 | 39 31-0S | 172 25.2W | 14 FEB 96 | 937 | 190 | 23 | 4761 | 8 | 4848 |
| 97 | 39 4.3S | 172 7.7W | 14 FEB 96 | 1612 | 160 | 18 | 4835 | 10 | 4929 |
| 98 | 38 37.8S | 171 48.6W | 14 FEB 96 | 2202 | 140 | 12 | 4914 | 10 | 5003 |
| 99 | 38 11S | 171 30.2W | 15 FEB 96 | 423 | 140 | 8 | 4932 | 10 | 5031 |
| 100 | 37 45.8S | 171 12.0W | 15 FEB 96 | 1033 | 130 | 14 | 4997 | 7 | 5119 |
| 101 | 37 18.6S | 170 53.7W | 15 FEB 96 | 1727 | 145 | 14 | 5130 | 5 | 5230 |
| 102 | 36 52.3S | 170 37.0W | 15 FEB 96 | 2306 | 210 | 12 | 5278 | 6 | 5384 |
| 103 | 36 27.0S | 170 17.2W | 16 FEB 96 | 513 | 220 | 15 | 5122 | 8 | 5219 |
| 104 | 36 0.2S | 170 0.3W | 16 FEB 96 | 1135 | 200 | 19 | 5069 | 8 | 5156 |
| 105 | 35 40.3S | 170 0.9W | 16 FEB 96 | 1727 | 205 | 24 | 4292 | 5 | 4329 |
| 106 | 35 20.0S | 170 0.1W | 16 FEB 96 | 2233 | 170 | 21 | 4895 | 7 | 4981 |
| 107 | 35 0.5S | 169 59.6W | 17 FEB 96 | 415 | 140 | 19 | 5250 | 5 | 5348 |
| 108 | 34 30.3S | 170 0.2W | 17 FEB 96 | 1137 | 160 | 20 | 5487 | 6 | 5591 |
| 109 | 33 59.8S | 170 0.0W | 17 FEB 96 | 1849 | 150 | 16 | 5533 | 6 | 5640 |
| 110 | 33 29.9S | 170 0.1W | 18 FEB 96 | 119 | 150 | 10 | 5416 | 6 | 5509 |
| 111 | 33 0.1S | 170 0.1W | 18 FEB 96 | 736 | 115 | 10 | 5582 | 10 | 5677 |
| 112 | 32 30.1S | 170 0.1W | 18 FEB 96 | 1404 | 115 | 8 | 5533 | 7 | 5651 |
| 113 | 31 59.8S | 169 59.8W | 18 FEB 96 | 2055 | 140 | 6 | 5677 | 7 | 5790 |
| 114 | 31 30.0S | 169 59.3W | 19 FEB 96 | 330 | 90 | 7 | 5526 | 8 | 5645 |
| 115 | 31 OS | 169 59.7W | 19 FEB 96 | 951 | 80 | 15 | 5606 | 7 | 5725 |
| 116 | 30 30.3S | 169 59.8W | 19 FEB 96 | 1640 | 90 | 14 | 5537 | 9 | 5640 |
| 117 | 30 0.2S | 169 59.8W | 19 FEB 96 | 2259 | 80 | 12 | 5413 | 7 | 5514 |
| 118 | 29 30.2S | 169 59.8W | 20 FEB 96 | 503 | 90 | 15 | 5148 | 12 | 5190 |
| 119 | 29 0.8S | 169 59.9W | 20 FEB 96 | 1113 | 70 | 18 | 5596 | 15 | 5684 |
| 120 | 28 30.5S | 169 59.8W | 20 FEB 96 | 1809 | 90 | 10 | 5459 | 9 | 5555 |
| 121 | 28 0.3S | 169 59.6W | 21 FEB 96 | 10 | 90 | 13 | 4907 | 10 | 4966 |
| 122 | 27 30.1S | 170 0.1W | 21 FEB 96 | 600 | 100 | 20 | 5349 | 7 | 5485 |
| 123 | 27 0.3S | 169 59.5W | 21 FEB 96 | 1202 | 95 | 13 | 5241 | 7 | 5331 |
| 124 | 26 29.7S | 169 59.4W | 21 FEB 96 | 1906 | 110 | 24 | 5613 | 8 | 5710 |
| 125 | 26 0.3S | 169 59.7W | 22 FEB 96 22 FEB 96 | 321 | 100 | 20 | 5601 | 9 | 5695 |
| 126 | 25 30.0S | 170 0.0W | | 1005 | 105 | 17 | 5833 | 9 | 5944 |
| 127 128 | 25 0.1S 24 30.0S | 169 59.9W 170 0.1W | | 1734 16 | 100 90 | 20 | 5640 5650 | | 5818 5757 |
| 129 | 24 50.0S 23 59.8S | 170 0.1W 170 0.1W | 23 FEB 96 23 FEB 96 | 720 | 80 | 16 16 | 5678 | 10 10 | 5780 |
| 130 | 23 39.6S 23 30.1S | 170 0.1W | 23 FEB 96 | 1404 | 100 | 18 | 5666 | 7 | 5781 |
| 131 | 22 59.8S | 169 59.7W | 23 FEB 96 | 2139 | 120 | 9 | 5691 | 9 | 5799 |
| 132 | 22 39.0S 22 30.0S | 169 59.9W | 24 FEB 96 | 448 | 120 | 13 | 5649 | 7 | 5752 |
| 133 | 22 0.0S | 169 59.9W | 24 FEB 96 | 1127 | 160 | 12 | 5626 | 8 | 5731 |
| 134 | 21 30S | 170 0.1W | 24 FEB 96 | 1837 | 150 | 7 | 5421 | 6 | 5514 |
| 135 | 20 59.7S | 169 59.6W | 25 FEB 96 | 107 | 160 | 5 | 5461 | 4 | 5566 |
| 136 | 20 29\$ | 170 0.1W | 25 FEB 96 | 739 | 175 | 5 | 5598 | 40 | 5722 |
| 137 | 20 0.0S | 170 0.1W | 25 FEB 96 | 1354 | 170 | 6 | 5315 | 7 | 5429 |
| 138 | 19 29.9S | 170 0.1W | 25 FEB 96 | 2023 | 80 | 4 | 4904 | 8 | 4982 |
| 139 | 19 0.1S | 170 3.4W | 26 FEB 96 | 159 | 350 | 5 | 2991 | 10 | 3047 |
| 140 | 18 30.3S | 170 0.4W | 26 FEB 96 | 730 | 330 | 9 | 5260 | 3 | 5343 |
| 141 | 18 0.0S | 170 0.0W | 26 FEB 96 | 1324 | 350 | 3 | 4912 | 9 | 4991 |
| 142 | 17 30.1S | 170 0.0W | 26 FEB 96 | 1948 | 65 | 5 | 5024 | 8 | 5097 |
| | | | 00 | | | | | | |

| STN | LATITUDE | LONGITUDE | DATE | TIME | W/D T | W/S (kts) | DEPTH (m) | HAB* (m) | CAST (db) |
|-----|----------|-----------|-----------|--------|----------|--------------|--------------|-------------|--------------|
| 143 | 17 0.1S | 169 59.8W | 27 FEB 96 | 156 | 80 | (Kts) | 4974 | 7 | 5081 |
| 144 | 16 30.3S | 169 59.9W | 27 FEB 96 | | 80 | 17 | 5134 | 6 | 5208 |
| 145 | 16 0.2S | 169 59.9W | 27 FEB 96 | | 90 | 13 | 5145 | 5 | 5233 |
| 146 | 15 29.8S | 170 0.1W | 27 FEB 96 | | 70 | 10 | 5087 | 8 | 5172 |
| 147 | 15 0.2S | 170 0.0W | 28 FEB 96 | | 0 | 10 | 4820 | 8 | 4884 |
| 148 | 14 40.0S | 169 59.9W | 28 FEB 96 | | 80 | 14 | 3315 | 8 | 3365 |
| 149 | 14 16.9S | 169 59.8W | 28 FEB 96 | | 20 | 10 | 3535 | 8 | 3578 |
| 150 | 13 58.3S | 170 0.0W | 28 FEB 96 | | 355 | 11 | 2938 | 9 | 2986 |
| 151 | 13 49.1S | 170 0.1W | 28 FEB 96 | | 40 | 7 | 4303 | 7 | 4367 |
| 152 | 13 30.1S | 170 0.0W | 29 FEB 96 | | 280 | 6 | 4878 | 8 | 4952 |
| 153 | 12 59S | 170 0.0W | 29 FEB 96 | | 95 | 11 | 4969 | 10 | 5047 |
| 154 | 12 29.9S | 169 59.9W | 29 FEB 96 | 1403 | 20 | 7 | 5000 | 5 | 5084 |
| 155 | 12 0.1S | 170 0.1W | 29 FEB 96 | | 310 | 11 | 5078 | 9 | 5016 |
| 156 | 11 30.0S | 170 0.0W | 1 MAR 96 | 3 217 | 330 | 13 | 5057 | 9 | 5138 |
| 157 | 11 0.1S | 170 0.0W | 1 MAR 96 | 807 | 20 | 9 | 5124 | 10 | 5205 |
| 158 | 10 30.1S | 169 59.8W | 1 MAR 96 | 345 | 350 | 7 | 4876 | 5 | 4964 |
| 159 | 9 55.5S | 169 37.7W | 1 MAR 96 | 3 2112 | 20 | 20 | 5205 | 10 | 5285 |
| 160 | 9 30.1S | 168 59.4W | 2 MAR 96 | 3 429 | 60 | 18 | 5340 | 5 | 5432 |
| 161 | 9 0.0S | 168 52.6W | 2 MAR 96 | 1036 | 70 | 19 | 4866 | 9 | 4973 |
| 162 | 8 29S | 168 44.9W | 2 MAR 96 | 1726 | 40 | 10 | 5154 | 6 | 5243 |
| 163 | 8 0.0S | 168 37.0W | 2 MAR 96 | 2343 | 40 | 5 | 5164 | 8 | 5260 |
| 164 | 7 30.0S | 168 45.0W | 3 MAR 96 | 542 | 70 | 10 | 5273 | 7 | 5364 |
| 165 | 7 0.0S | 168 44.9W | 3 MAR 96 | 1141 | 100 | 10 | 5670 | 8 | 5767 |
| 166 | 6 30.1S | 168 44.9W | 3 MAR 96 | | 70 | 10 | 5535 | 10 | 5646 |
| 167 | 6 0.0S | 168 45.0W | 4 MAR 96 | | 30 | 10 | 5671 | 8 | 5769 |
| 168 | 5 30.1S | 168 45.0W | 4 MAR 96 | | 50 | 10 | 5379 | 8 | 5522 |
| 169 | 5 0.0S | 168 45.0W | 4 MAR 96 | | 50 | 9 | 5572 | 10 | 5666 |
| 170 | 4 0.0S | 168 45.1W | 4 MAR 96 | | 40 | 14 | 5208 | 8 | 5290 |
| 171 | 3 0S | 168 45.0W | 5 MAR 96 | | 30 | 20 | 5379 | 4 | 5467 |
| 172 | 2 0S | 168 45.0W | 5 MAR 96 | | 40 | 17 | 3285 | 10 | 3447 |
| 173 | 1 0S | 168 45.2W | 6 MAR 96 | | 80 | 17 | 5786 | 8 | 5891 |
| 174 | 0 0.1S | 168 45.0W | 6 MAR 96 | | 70 | 16 | 5581 | 10 | 5683 |
| 175 | 7 44.8S | 168 40.2W | 8 MAR 96 | | 80 | 14 | 5319 | 3 | 5414 |
| 176 | 8 15.1S | 168 41.3W | 8 MAR 96 | | 75 | 10 | 4964 | 6 | 5051 |
| 177 | 10 8.7S | 168 58.8W | 8 MAR 96 | | 100 | 12 | 4640 | 8 | 4709 |
| 178 | 10 4.1S | 169 12.7W | 8 MAR 96 | | 100 | 10 | 5254 | 10 | 5336 |
| 179 | 9 55.2S | 169 37.7W | 9 MAR 96 | | 70 | 11 | 5215 | 4 | 5306 |
| 180 | 9 47.0S | 170 3.5W | 9 MAR 96 | | 95 | 7 | 5014 | 8 | 5097 |
| 181 | 9 41.6S | 170 19.5W | 9 MAR 96 | | 30 | 6 | 4293 | 8 | 4372 |
| 182 | 9 35.7S | 170 36.1W | 9 MAR 96 | 1900 | 90 | 9 | 4038 | 7 | 4090 |

^{*} height above bottom depth corrected water depth

 Table 2a:
 Full water column station groupings for CTD oxygen algorithm parameters.

| Station | StdDev | #Obs | 2.8*sd | 1:Bias | 2:Slope | 3:Pcor | 4:Tcor | 5: Wt | 6: Lag |
|---------|------------|------|--------|--------|------------|-------------|-------------|-------------|-------------|
| 4-9 | 0.1351E+01 | 96 | 3.782 | 0.014 | 0.3616E-02 | 0.1350E-03* | -0.3149E-01 | 0.8702E+00* | 0.3275E+01* |
| 10-13 | 0.1732E+01 | 73 | 4.849 | 0.026 | 0.3561E-02 | 0.1350E-03* | -0.3003E-01 | 0.8702E+00* | 0.3275E+01* |
| 14-18 | 0.9219E+00 | 145 | 2.581 | 0.007 | 0.3815E-02 | 0.1350E-03* | -0.3797E-01 | 0.8702E+00* | 0.3275E+01* |
| 19-24 | 0.1207E+01 | 108 | 3.380 | 0.020 | 0.3702E-02 | 0.1350E-03* | -0.3494E-01 | 0.8702E+00* | 0.3275E+01* |
| 25-31 | 0.8802E+00 | 149 | 2.465 | 0.019 | 0.3738E-02 | 0.1350E-03* | -0.3822E-01 | 0.8702E+00* | 0.3275E+01* |
| 32-45 | 0.1088E+01 | 322 | 3.045 | 0.017 | 0.3772E-02 | 0.1338E-03 | -0.3540E-01 | 0.6807E+00 | 0.7588E+01 |
| 46-53 | 0.9705E+00 | 237 | 2.718 | 0.023 | 0.3676E-02 | 0.1345E-03 | -0.3174E-01 | 0.6084E+00 | 0.6309E+01 |
| 54-62 | 0.1516E+01 | 273 | 4.244 | 0.021 | 0.3675E-02 | 0.1361E-03 | -0.3032E-01 | 0.8185E+00 | 0.1341E+01 |
| 63-77 | 0.2001E+01 | 430 | 5.603 | 0.045 | 0.3481E-02 | 0.1310E-03 | -0.2757E-01 | 0.8358E+00 | 0.2439E+01 |
| 78-87 | 0.2184E+01 | 231 | 6.114 | 0.044 | 0.3320E-02 | 0.1449E-03 | -0.2536E-01 | 0.7788E+00 | 0.2021E+01 |
| 88-95 | 0.1724E+01 | 255 | 4.827 | 0.050 | 0.3271E-02 | 0.1409E-03 | -0.2511E-01 | 0.7474E+00 | 0.2745E+01 |
| 96-113 | 0.1770E+01 | 574 | 4.956 | 0.034 | 0.3472E-02 | 0.1389E-03 | -0.2739E-01 | 0.8249E+00 | 0.2537E+01 |
| 114-131 | 0.1687E+01 | 587 | 4.724 | 0.034 | 0.3479E-02 | 0.1390E-03 | -0.2703E-01 | 0.8737E+00 | 0.3543E+01 |
| 135-154 | 0.1714E+01 | 624 | 4.800 | 0.045 | 0.2938E-02 | 0.1476E-03 | -0.2465E-01 | 0.8803E+00 | 0.5267E-01 |
| 155-171 | 0.1929E+01 | 558 | 5.402 | 0.009 | 0.3289E-02 | 0.1508E-03 | -0.2794E-01 | 0.8965E+00 | 0.1374E-01 |
| 172-176 | 0.1494E+01 | 124 | 4.182 | -0.006 | 0.3554E-02 | 0.1474E-03 | -0.3070E-01 | 0.7925E+00 | 0.0000E+00* |
| 177 | 0.4873E+00 | 13 | 1.364 | 0.021 | 0.3213E-02 | 0.1474E-03* | -0.4386E-01 | 0.7925E+00* | 0.0000E+00* |
| 178 | 0.8195E+00 | 16 | 2.295 | -0.009 | 0.3443E-02 | 0.1474E-03* | -0.8431E-01 | 0.7925E+00* | 0.0000E+00* |
| 179 | 0.5936E+00 | 15 | 1.662 | -0.019 | 0.3316E-02 | 0.1474E-03* | -0.9472E-01 | 0.7925E+00* | 0.0000E+00* |
| 180 | 0.5059E+00 | 13 | 1.416 | -0.040 | 0.3283E-02 | 0.1474E-03* | -0.1163E+00 | 0.7925E+00* | 0.0000E+00* |
| 181 | 0.3037E+00 | 10 | 0.850 | -0.041 | 0.3268E-02 | 0.1474E-03* | -0.1508E+00 | 0.7925E+00* | 0.0000E+00* |
| 182 | 0.1928E+01 | 7 | 5.398 | -0.098 | 0.3711E-02 | 0.1474E-03* | -0.1875E+00 | 0.7925E+00* | 0.0000E+00* |

fixed parameter

Table 2b: Deep water column station groupings for CTD oxygen algorithm parameters.

| Station | StdDev | #Obs | 2.8*,sd | 1:Bias | 2:Slope | 3:Pcor | 4:Tcor | 5: Wt | 6: Lag |
|---------|------------|------|---------|--------|------------|-------------|-------------|-------------|-------------|
| 10-18 | 0.8233E+00 | 119 | 2.305 | 0.000 | 0.3918E-02 | 0.1350E-03* | -0.4539E-01 | 0.8702E+00* | 0.3275E+01* |
| 19-31 | 0.8240E+00 | 187 | 2.307 | 0.016 | 0.3754E-02 | 0.1350E-03* | -0.3740E-01 | 0.8702E+00* | 0.3275E+01* |
| 32-45 | 0.8000E+00 | 237 | 2.240 | 0.021 | 0.3735E-02 | 0.1338E-03* | -0.3460E-01 | 0.6807E+00* | 0.7588E+01* |
| 46-53 | 0.5762E+00 | 131 | 1.613 | 0.010 | 0.3846E-02 | 0.1345E-03* | -0.3893E-01 | 0.6084E+00* | 0.6309E+01* |
| 54-62 | 0.4671E+00 | 139 | 1.308 | -0.001 | 0.3939E-02 | 0.1361E-03* | -0.3908E-01 | 0.8185E+00* | 0.1341E+01* |
| 63-77 | 0.5677E+00 | 190 | 1.590 | 0.008 | 0.3972E-02 | 0.1310E-03* | -0.4515E-01 | 0.8358E+00* | 0.2439E+01* |
| 78-95 | 0.8477E+00 | 90 | 2.374 | -0.011 | 0.3991E-02 | 0.1409E-03* | -0.3776E-01 | 0.7474E+00* | 0.2745E+01* |
| 96-113 | 0.7719E+00 | 196 | 2.161 | -0.001 | 0.3901E-02 | 0.1389E-03* | -0.3079E-01 | 0.8249E+00* | 0.2537E+01* |
| 114-131 | 0.7562E+00 | 213 | 2.117 | -0.008 | 0.4008E-02 | 0.1390E-03* | -0.3101E-01 | 0.8737E+00* | 0.3543E+01* |
| 135-154 | 0.8193E+00 | 180 | 2.294 | -0.003 | 0.3476E-02 | 0.1476E-03* | -0.2547E-01 | 0.8803E+00* | 0.5267E-01* |
| 155-171 | 0.8459E+00 | 225 | 2.368 | -0.013 | 0.3480E-02 | 0.1508E-03* | -0.6254E-02 | 0.8965E+00* | 0.1374E-01* |
| 172-176 | 0.1120E+01 | 64 | 3.135 | -0.009 | 0.3524E-02 | 0.1474E-03* | -0.1246E-01 | 0.7500E+00* | 0.0000E+00* |

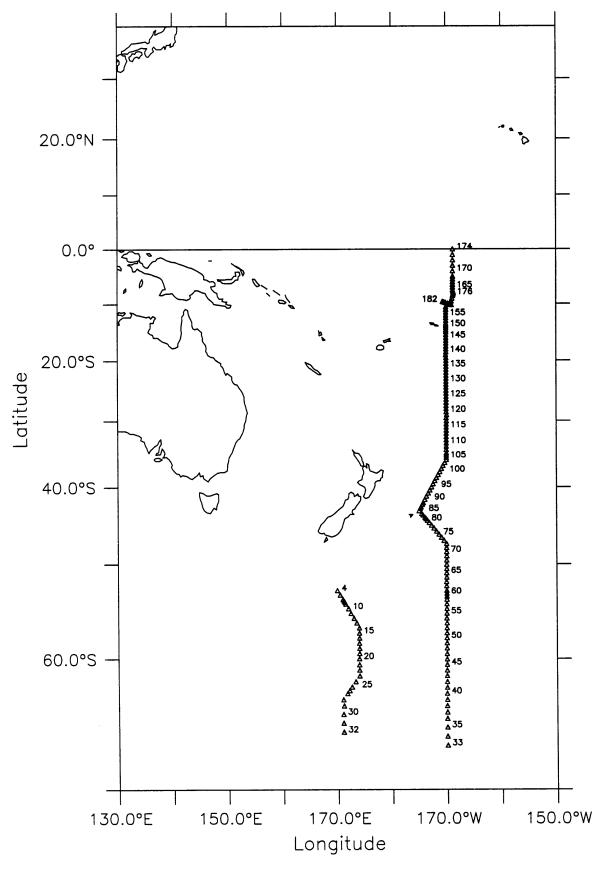


Figure 1: CTD station locations made on the RN Discoverer from January 9 to March 9, 1996.

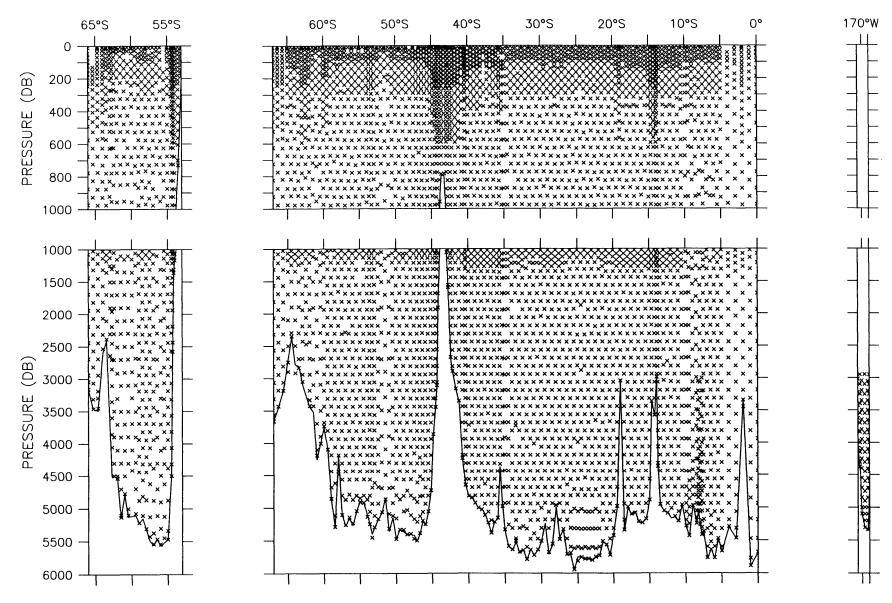
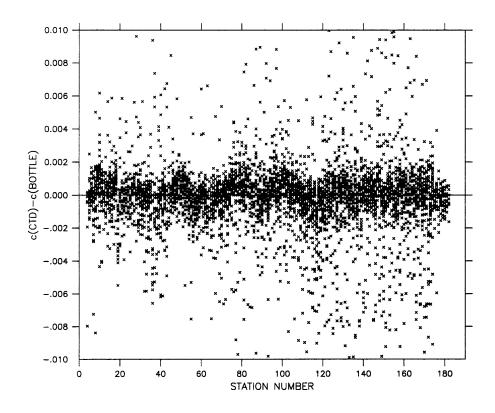


Figure 2: Pressures of bottle closures at each station.



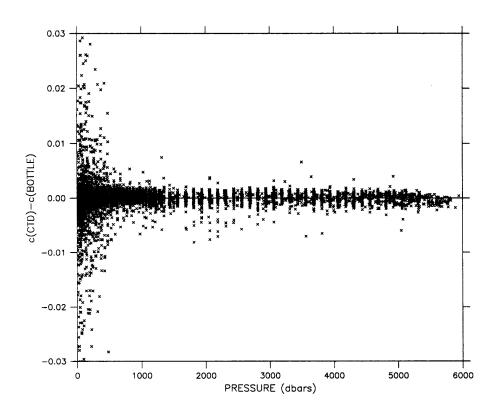


Figure 3: Calibrated CTD-bottle conductivity differences (mS/cm) plotted against station number (upper panel). Calibrated CTD-bottle conductivity differences (mS/cm) plotted against pressure (lower panel).

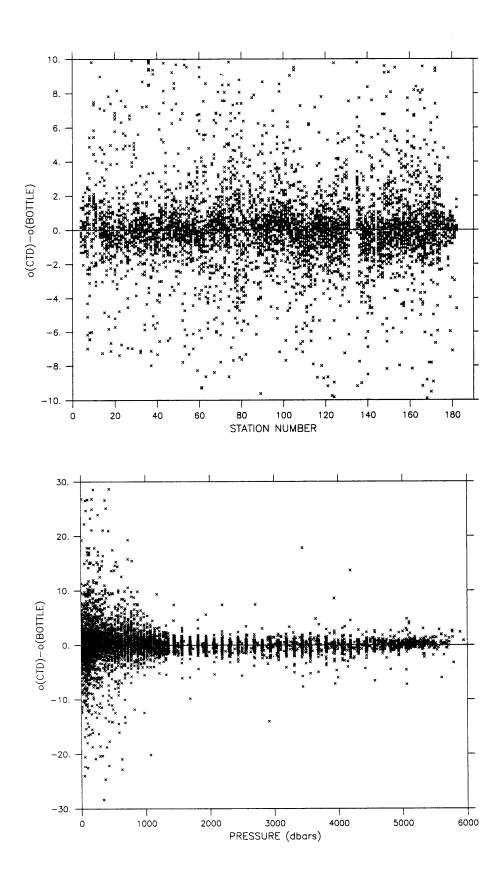


Figure 4: Calibrated CTD-bottle oxygen differences (µmol/kg) plotted against station number (upper panel). Calibrated CTD-bottle oxygen differences (µmol/kg) plotted against pressure (lower panel).

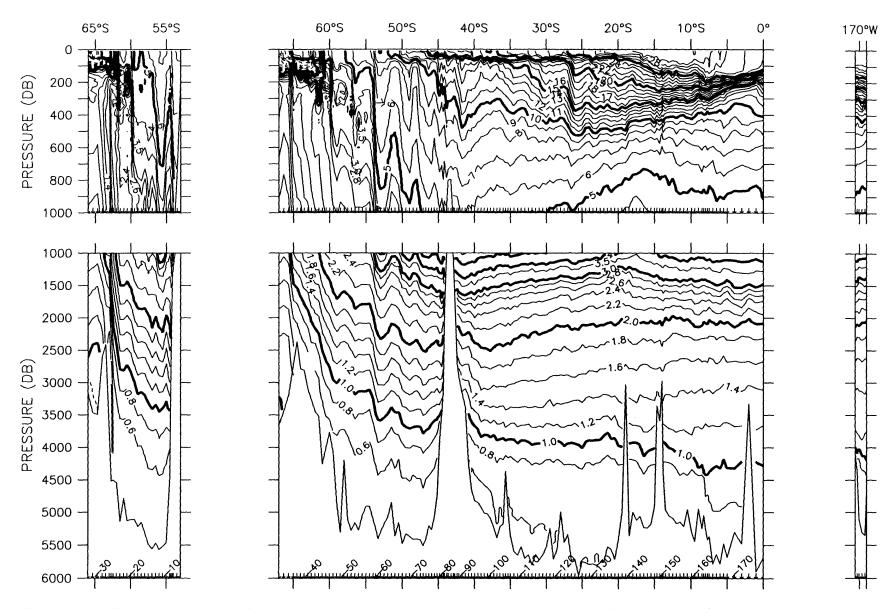


Figure 5: Potential temperature (IC) sections along P14S, P15S, and across the Samoan Passage. Contour intervals are 0.2 from $-2-3^{\circ}$ C, 0.5 from $3-4^{\circ}$ C, and 1 from $4-35^{\circ}$ C.

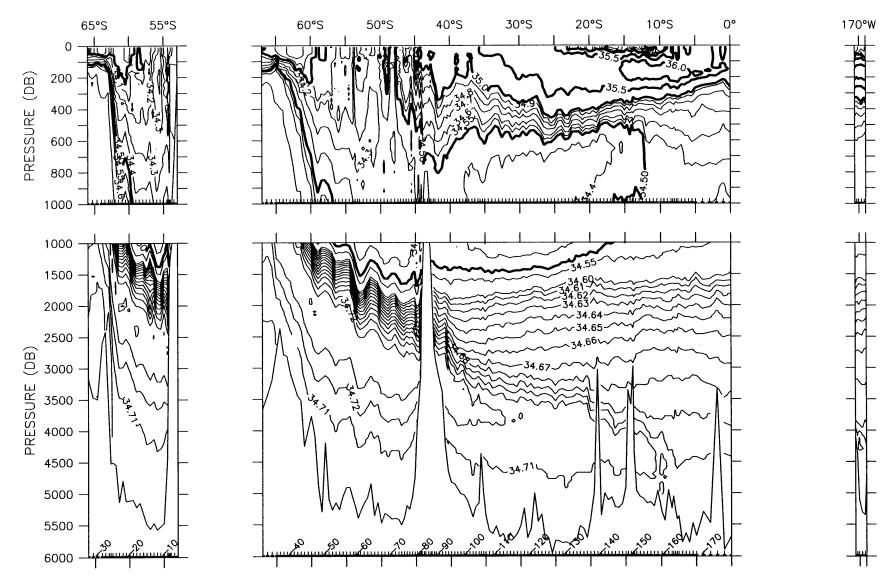


Figure 6: Salinity (PSS) sections along P14S, P15S, and across the Samoan Passage. Contour intervals are 0. 1 from 32-34.5 PSS, 0.05 from 34.5-34.6 PSS, 0. 1 from 34.6-35 PSS, 0.5 from 35-37 PSS in the upper panel. Contour intervals are 0. 1 from 32-34.5 PSS, 0.05 from 34.5-34.6 PSS, and 0.0 1 from 34.6-34.8 PSS, 0.1 from 34.8-35, and 1.0 from 35-37 PSS in the lower panel.

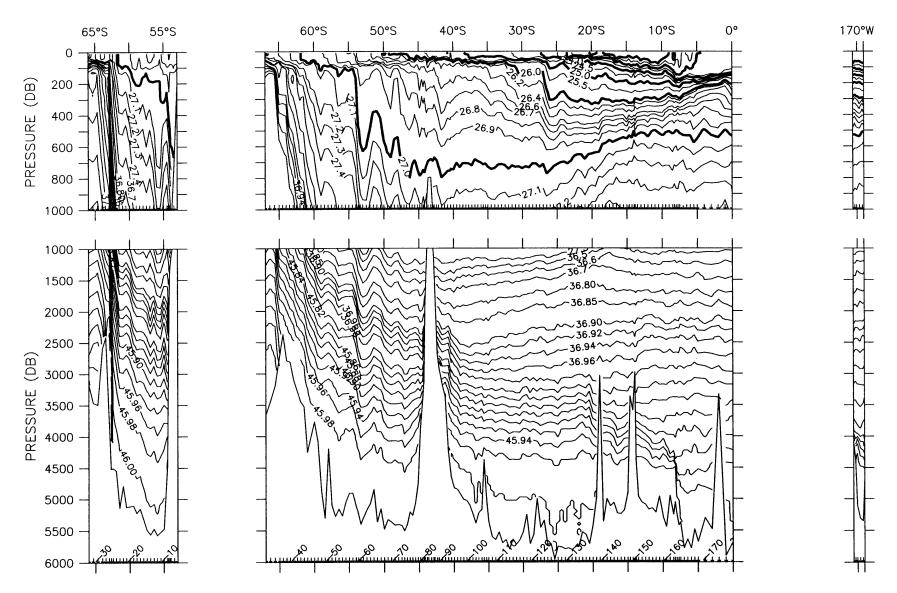
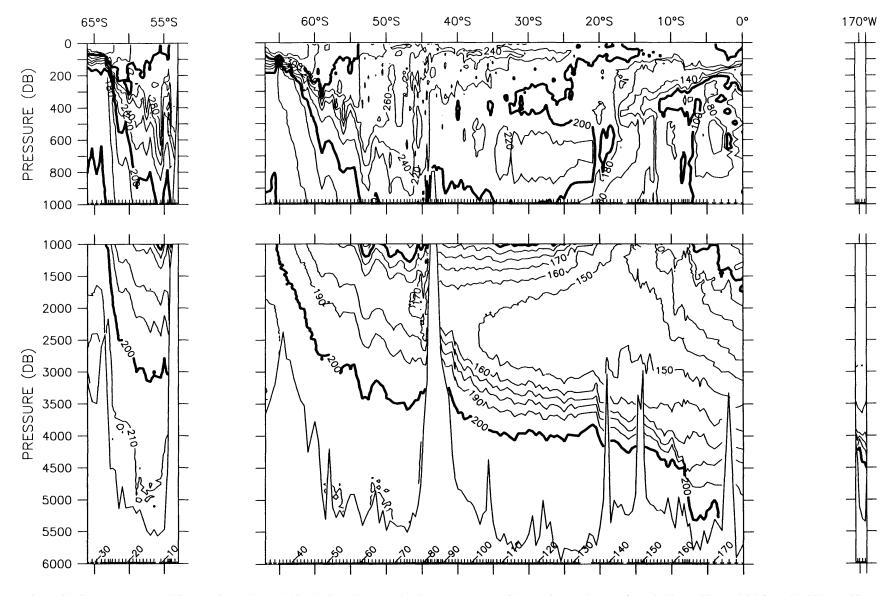


Figure 7: Potential density (kg/m3) sections along P14S, P15S, and across the Samoan Passage. Sigma-theta contour intervals are 0.5 from 22-26, 0.2 from 26-26.6, and 0.1 from 26.6-27.4. Sigma-2 contour intervals are 0.1 from 36.7-36.8, 0.05 from 36.8-36.9, and 0.02 from 36.9-37. Sigma-4 contour intervals are 0.02 from 45.82-48.



 $Figure~8:~CTD~oxygen~(\mu mol/kg)~sections~along~P14S,~P15S,~and~across~the~Samoan~Passage.~Contour~intervals~are~5~from~0-20~\mu mol/kg~and~20~from~20-400~\mu mol/kg.$

9. REFERENCES

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APPENDIX 4a. Oxygen Measurement techniques on WOCE P14S and P15S (CGC96)

Summary of Oxygen Data for CGC96

(Kirk Hargreaves) 15 May 1996

1.1 Oxygen

1.1.1 Overview

Oxygen samples were drawn from every bottle for every station (except for some test casts and severely leaking bottles). A total of 5683 samples plus 516 duplicates were analyzed. Four people drew oxygen samples and three people ran analyses. The estimated accuracy, relative to the standards, is 0.1% (potentially 0.05%) plus an estimated precision of 0.2 umol/kg. Note that precision is sampler dependent and was as good as 0.15 umol/kg for some samplers. Also, discounting the 12 duplicates (2.5% of total) with more than three sigma error, the total precision is 0.15 umol/kg. Individual sampler variation is from 0.14 to 0.19 umol/kg.

Water temperature was not measured at the time of sampling. Previous measurements have shown that even in the tropics, bottom water warms only a few degrees C before being sampled. For a rise in temperature from 0 C to 4 C, the change in the density of the water is 0.03%. Conversion to umol/kg is calculated with potential density.

Samples were titrated using Culberson's (Culberson, 1992) modifications to Carpenter's whole bottle technique (Carpenter, 1969). An auto-titrator based on a design by Gernot Friederich (Friederich, 1991) and using a modified version of Friederich's software was used to titrate the samples. The titrator consists of a Kloehn 50100 Syringe Drive with a 5 ml syringe, a custom- built photometer with two color channels, LM35 temperature sensors, an eight channel A/D board, and a computer. Post- processing software was used to add in temperature corrections and to analyze data.

1.1.2 Sampling and pickling

Oxygen sampled immediately after CFC's. Samples were drawn in calibrated 125 ml nominal volume iodine determination flasks (Corning 5400-125). The sampling tube was inserted into the flask, allowed to flow freely and squeezed and tapped to remove bubbles, and then inverted. The tube was pinched to reduce flow and allow water in the flask to drain. A water sheet was formed on the inside of the flask, the sampling tube pinched to reduce flow, the flask drained, and then put right-side up. The sampling tube was slowly released to prevent turbulent flow and the flask allowed to fill. For best results, the sampling tube was kept pinched to keep the flow smooth throughout sampling. By counting, the fill time was measured and used to ensure at least two volumes overflow.

Reagents were introduced shortly after sampling using Brinkmann 1.0 ml Fixed Volume Dispensette repipets. The tips of the repipets were lengthened using clear polyolefin

shrink tubing. The MnCl2 was added at the midpoint of the flask, and NaOH/NaI just below the neck. Repipets were filled before inserting into the water. If necessary, a little was dispensed to ensure the tubes were full.

Flasks were capped at this point and shaken while pushing on the stopper until the reagents were well mixed. The flask was inverted and checked for bubbles. Deionized water was added to the collar of the flask and the flask stowed. At least 20 minutes after sampling was finished, flasks were reshaken and deionized water added to the collars again.

1.1.3 Analysis

Samples were analyzed no earlier than 20 minutes and no later than 8 hours after remixing. Liquid from the flask collar was aspirated with a transfer pipette and the stopper removed. ~1ml of 10N sulfuric acid and a rinsed, pivotless stir bar were added (pivotless stir bars spin most easily). The flask was inserted into a water bath in the photometer and titrated with 0.05 N sodium thiosulfate. (The water path minimizes refractive effects). After titration, the sample was poured out and the flask rinsed with hot tap water. The typical sample-to-sample time was 1.5 to 2 minutes.

1.1.4 Standardization

Titrant was standardized daily with ~0.01N (actually 0.01 eq/kg) potassium iodate solution. The standard deviation of standardization is 0.05%, though one batch of thiosulfate solution showed a variation of 0.2%. Standards were mixed before the cruise and stored in upside down air tight Boston round bottles. All standards intercompared before the cruise to better than 0.02%.

Standards were prepared by weight from two ~0.1 eq/kg stock solutions. The stock solutions were made from oven dried and vacuum desiccated KIO3 from two different manufacturers (Mallinckrodt Lot #1094-KHSR and Fisher Lot #951151). In addition, all standards were compared to a volumetrically prepared standard from Baker (pre-weighed KIO3 obtained from Oregon State University. Lot number unknown). Mixing standards by weight is both faster and more accurate than mixing standards volumetrically.

Standard was dispensed using a spare Kloehn 50100 with a calibrated 25 ml buret or an Eppendorf Maxipettor with calibrated tip. Unfortunately, the Eppendorf Maxipettor has a large (0.02%/C) temperature dependence that needs to be taken into account. The measured precision of the dispensed standards is 0.6 uL and 2 uL for the Kloehn and Eppendorf, respectively.

The temperature of the standard was measured directly with a calibrated thin film Pt-RTD (Sensycon GW2107-01) and thermometer (Cole-Parmer H-08497-00). Standard concentration was converted to normality by dividing by then density of pure water at temperature plus 0.03% (mass fraction of the potassium iodate).

1.1.5 Post-processing

Post-processing software written in Perl (Wall, 1991) and using algorithms from "Numerical Recipes in C" (Press, 1988) was used to add in temperature corrections and update standardization. Perl code was also used to generate the correct WOCE flags, average duplicate data, and generate the final output. Lotus 1-2-3 was used to plot curves, compare bottle data to oxygen sensor data, and analyze duplicates.

1.1.6 Reagents

Reagents were gravimetrically prepared before the cruise. 600 g MnCl2 were added to 692.92 g water, and 320 g NaOH and 600 g NaI were added to 753.68 g water. At room temperature, these give molar concentrations equal to the WOCE specifications, but are much faster to mix. Reagents were stored in glass or HDPE bottles.

1.2 Oxygen References

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APPENDIX 4b Replicate Oxygen Measurements on WOCE P14S and P15S (CGC96)

These are the standard deviations of the oxygen data duplicates. The averaged data are in the oxygen data file and flagged with a '6'.

| <u>Sta</u> | Smp | StdDev | Sta | Smp | StdDev | Sta | Smp | StdDev | Sta | Smp | StdDev |
|-----------------|------------|--------------|----------|------------|--------------|----------|------------|--------------|----------|------------|--------------|
| 5 | 104 | 0.00 | 33 | 123 | 0.04 | 54 | 103 | 0.09 | 69 | 221 | 0.03 |
| 6 | 104 | 0.15 | 34 | 107 | 0.10 | 54 | 109 | 0.13 | 69 | 229 | 0.01 |
| 6 | 107 | 0.16 | 34 | 113 | 0.14 | 54 | 115 | 0.13 | 70 | 106 | 0.35 |
| 10 | 204 | 0.01 | 34 | 119 | 0.02 | 54 | 121 | 0.05 | 70 | 109 | 0.01 |
| 10 | 208 | 0.17 | 34 | 125 | 0.02 | 55 | 107 | 0.11 | 70 | 111 | 0.08 |
| 11 | 105 | 0.11 | 35 | 104 | 0.31 | 55 55 | 110 | 0.16 | 71 | 105 | 0.22 |
| 11 | 110 | 0.00 0.06 | 35 | 107 | 0.19 | 55 56 | 113 | 0.06 | 71 71 | 113 | 0.06 |
| 11 11 | 115 120 | 0.06 | 35 40 | 110 108 | 0.36 0.21 | 56 56 | 106 108 | 0.09 0.16 | 71 71 | 119 123 | 0.03 0.08 |
| $\frac{11}{14}$ | 112 | 0.47 | 40 | 119 | 0.21 | 56 | 110 | 0.16 | 72 | 103 | 0.08 |
| $\frac{14}{14}$ | 120 | 0.10 | 41 | 109 | 0.18 | 57 | 107 | 0.10 | 72 | 113 | 0.16 |
| $\frac{14}{14}$ | 128 | 0.27 | 41 | 115 | 0.04 | 57 | 113 | 0.11 | 72 | 119 | 0.00 |
| 15 | 207 | 0.14 | 41 | 121 | 0.13 | 57 | 119 | 0.02 | 72 | 127 | 0.02 |
| 15 | 214 | 0.08 | 41 | 127 | 0.79 | 57 | 125 | 0.13 | 73 | 110 | 0.00 |
| 15 | 221 | 0.19 | 42 | 107 | 0.01 | 58 | 213 | 0.14 | 73 | 118 | 0.13 |
| 15 | 229 | 0.74 | 42 | 113 | 0.79 | 58 | 227 | 0.10 | 73 | 126 | 0.07 |
| 16 | 104 | 0.55 | 42 | 119 | 0.19 | 58 | 231 | 0.39 | 74 | 205 | 0.12 |
| 16 | 104 | 0.75 | 42 | 125 | 0.22 | 59 | 106 | 0.32 | 74 | 211 | 0.39 |
| 17 | 104 | 0.73 | 46 | 103 | 0.23 | 59 | 109 | 0.32 | 74 | 216 | 0.24 |
| 17 | 108 | 0.05 | 46 | 109 | 0.02 | 60 | 104 | 0.33 | 74 | 220 | 0.20 |
| 17 | 122 | 0.03 | 46 | 115 | 0.53 | 60 | 104 | 0.78 | 75 | 107 | 0.38 |
| 18 | 105 | 0.01 | 46 | 121 | 0.19 | 60 | 109 | 0.70 | 75 | 115 | 0.00 |
| 18 | 111 | 0.01 | 47 | 213 | 0.09 | 61 | 105 | 0.05 | 75 | 123 | 0.41 |
| 18 | 117 | 0.01 | 47 | 217 | 0.05 | 61 | 109 | 0.19 | 75 | 131 | 0.07 |
| 18 | 123 | 0.84 | 47 | 221 | 0.00 | 61 | 115 | 0.12 | 76 | 213 | 0.04 |
| 28 | 111 | 0.05 | 47 | 225 | 0.01 | 61 | 119 | 0.05 | 76 | 219 | 0.35 |
| 28 | 118 | 0.38 | 48 | 104 | 0.44 | 62 | 217 | 0.05 | 76 | 225 | 0.34 |
| 29 | 203 | 0.08 | 48 | 108 | 0.34 | 62 | 219 | 0.02 | 76 | 231 | 0.08 |
| 29 | 206 | 0.08 | 49 | 113 | 0.01 | 62 | 225 | 0.09 | 77 | 106 | 0.01 |
| 29 | 210 | 0.31 | 49 | 117 | 0.26 | 62 | 231 | 0.07 | 77 | 110 | 0.08 |
| 29 | 214 | 0.63 | 50 | 105 | 0.16 | 65 | 121 | 0.40 | 77 | 112 | 0.05 |
| 30 | 105 | 0.10 | 50 | 115 | 0.05 | 65 | 123 | 0.05 | 77 | 115 | 0.08 |
| 30 | 107 | 0.18 | 50 | 121 | 0.15 | 66 | 110 | 0.08 | 78 | 104 | 0.10 |
| 30 | 117 | 0.21 | 50 | 129 | 0.03 | 66 | 117 | 0.30 | 78 | 107 | 0.05 |
| 30 | 127 | 0.12 | 51 | | 0.02 | 66 | 122 | 0.03 | 78 | 111 | 0.01 |
| 31 | 207 | 0.03 | 51 | 114 | 0.09 | 66 | 128 | 0.06 | 78 | 115 | 0.05 |
| 31 | 215 | 0.00 | 51 | 120 | 0.03 | 67 | 207 | 0.15 | 79 | 111 | 0.04 |
| 31 | 223 | 0.24 | 51 | 126 | 0.14 | 67 | 209 | 0.21 | 79 | 117 | 0.03 |
| 31 | 227 | 0.09 | 52 | 105 | 0.08 | 67 | 213 | 0.24 | 79 | 123 | 0.09 |
| 32 | 104 | 0.20 | 52 | 108 | 0.11 | 68 | 107 | 0.00 | 79 | 129 | 0.14 |
| 32 | 107 | 0.20 | 52 | 112 | 0.43 | 68 | 115 | 0.07 | 80 | 215 | 0.04 |
| 32 | 114 | 0.02 | 53 | 105 | 0.21 | 68 | 123 | 0.20 | 80 | 221 | 0.05 |
| 33 | 105 | 0.30 | 53 | 111 | 0.04 | 68 | 131 | 0.06 | 80 | 227 | 0.56 |
| 33 | 111 | 0.91 | 53 | 117 | 0.03 | 69 | 208 | 0.06 | 81 | 105 | 0.06 |
| 33 | 117 | 0.05 | 53 | 121 | 0.00 | 69 | 213 | 0.12 | 81 | 108 | 0.09 |

| <u>Sta</u> 81 | <u>Smp</u> | StdDev 0.06 | <u>Sta</u> | <u>Smp</u> 211 | <u>StdDev</u> 0.02 | <u>Sta</u> | Smp 205 | <u>StdDev</u> 0.03 | <u>Sta</u> | <u>Smp</u> | <u>StdDev</u> 0.07 |
|------------------|------------|----------------|------------|-------------------|--------------------|------------|----------------|--------------------|------------|------------|--------------------|
| 82 | 104 | 0.15 | 101 | 219 | 0.02 | 116 | 213 | 0.09 | 129 | 115 | 0.05 |
| 82 | 107 | 0.15 | 101 | 231 | 0.06 | 116 | 221 | 0.17 | 129 | 122 | 0.18 |
| 82 | 110 | 0.13 | 102 | 105 | 0.10 | 116 | 229 | 0.06 | 129 | 131 | 0.06 |
| 88 | 101 | 0.00 | 102 | 115 | 0.10 | 117 | 103 | 0.18 | 130 | 101 | 0.49 |
| 88 | 104 | 0.11 | 102 | 121 | 0.03 | 117 | 109 | 0.15 | 130 | 109 | 0.12 |
| 88 | 104 | 0.11 | 102 | 129 | 0.03 | 117 | 125 | 0.10 | 130 | 117 | 0.12 |
| 89 | 201 | 0.07 | 103 | 101 | 0.03 | 117 | 135 | 0.10 | 130 | 125 | 0.05 |
| 89 | 201 | 0.00 | 103 | 119 | 0.10 | 118 | 101 | 0.12 | 131 | 105 | 0.03 |
| 89 | 204 | 0.00 | 103 | 136 | 0.21 | 118 | 112 | 0.13 | 131 | 111 | 0.05 |
| 90 | 101 | 0.11 | 103 | 105 | 0.01 | 118 | 124 | 0.04 | 131 | 119 | 0.03 |
| 90 | 101 | 0.07 | 104 | 115 | 0.03 | 118 | 136 | 0.13 | 131 | 127 | 0.01 |
| 90 | 104 | 0.04 | 104 | 125 | | 119 | | 0.03 | 132 | 101 | |
| 91 | 108 | | 104 | 135 | 0.09 | | 101 111 | | 132 | 113 | 0.06 |
| | | 0.03 | | | 0.13 | 119 | 121 | 0.02 | | | 0.14 |
| 91 | 115 | 0.16 | 105 | 209 | 0.07 | 119 | | 0.06 | 132 | 124 | 0.03 |
| 91 | 121 | 0.05 | 105 | 213 | 0.01 | 119 | 133 | 0.00 | 132 | 136 | 0.03 |
| 91 | 127 | 0.06 | 105 | 223 | 0.06 | 120 | 201 | 0.05 | 133 | 101 | 0.01 |
| 92 | 209 | 0.12 | 105 | 232 | 0.13 | 120 | 211 | 0.00 | 133 | 113 | 0.15 |
| 92 | 217 | 0.03 | 106 | 105 | 0.04 | 120 | 221 | 0.04 | 133 | 125 | 0.11 |
| 92 | 225 | 0.03 | 106 | 109 | 0.03 | 120 | 231 | 0.04 | 133 | 135 | 0.07 |
| 92 | 234 | 0.07 | 106 | 121 | 0.28 | 121 | 205 | 0.09 | 134 | 201 | 0.05 |
| 93 | 101 | 0.36 | 106 | 129 | 0.09 | 121 | 211 | 0.21 | 134 | 211 | 0.09 |
| 93 | 105 | 0.36 | 107 | 101 | 0.20 | 121 | 223 | 0.08 | 134 | 221 | 0.11 |
| 93 | 108 | 0.12 | 107 | 112 | 0.17 | 121 | 231 | 0.63 | 134 | 231 | 0.03 |
| 93 | 113 | 0.12 | 107 | 124 | 0.09 | 122 | 101 | 0.02 | 135 | 203 | 0.11 |
| 94 | 105 | 0.01 | 108 | 107 | 0.05 | 122 | 112 | 0.01 | 135 | 212 | 0.06 |
| 94 | 111 | 0.24 | 108 | 117 | 0.00 | 122 | 124 | 0.16 | 135 | 219 | 0.08 |
| 94 | 117 | 0.03 | 108 | 127 | 0.01 | 122 | 136 | 0.02 | 135 | 229 | 0.01 |
| 94 | 123 | 0.24 | 108 | 135 | 0.15 | 123 | 103 | 0.03 | 136 | 101 | 0.11 |
| 95 | 101 | 0.17 | 109 | 105 | 0.04 | 123 | 113 | 0.05 | 136 | 107 | 0.10 |
| 95 | 112 | 0.59 | 109 | 121 | 0.19 | 123 | 123 | 0.19 | 136 | 113 | 0.08 |
| 95 | 124 | 0.14 | 109 | 129 | 0.12 | 123 | 135 | 0.08 | 136 | 119 | 0.01 |
| 96 | 107 | 0.03 | 110 | 212 | 0.63 | 124 | 102 | 0.13 | 137 | 103 | 0.04 |
| 96 | 123 | 0.05 | 110 | 215 | 0.03 | 124 | 112 | 0.06 | 137 | 109 | 0.13 |
| 97 | 209 | 0.18 | 110 | 219 | 0.15 | 124 | 122 | 0.65 | 137 | 115 | 0.06 |
| 97 | 215 | 0.00 | 110 | 227 | 0.01 | 124 | 132 | 0.21 | 137 | 123 | 0.14 |
| 97 | 221 | 0.27 | 111 | 107 | 0.07 | 125 | 301 | 0.01 | 138 | 105 | 0.24 |
| 97 | 227 | 0.06 | 111 | 109 | 0.01 | 125 | 312 | 0.13 | 138 | 111 | 0.01 |
| 98 | 107 | 0.01 | 111 | 115 | 0.03 | 125 | 325 | 0.05 | 138 | 119 | 0.09 |
| 98 | 113 | 0.05 | 111 | 123 | 0.10 | 126 | 101 | 0.03 | 138 | 127 | 0.06 |
| 98 | 122 | 0.11 | 112 | 105 | 0.03 | 126 | 111 | 0.06 | 140 | 104 | 0.22 |
| 98 | 130 | 0.05 | 112 | 113 | 0.06 | 126 | 121 | 0.12 | 140 | 111 | 0.08 |
| 99 | 101 | 0.03 | 112 | 121 | 0.15 | 126 | 131 | 0.07 | 140 | 121 | 0.01 |
| 99 | 112 | 0.19 | 112 | 129 | 0.07 | 127 | 205 | 0.01 | 140 | 131 | 0.06 |
| 99 | 124 | 0.01 | 114 | 112 | 0.10 | 127 | 215 | 0.00 | 141 | 101 | 0.08 |
| 99 | 136 | 0.09 | 114 | 123 | 0.05 | 127 | 225 | 0.64 | 141 | 113 | 0.11 |
| 100 | 107 | 0.12 | 114 | 134 | 0.04 | 127 | 233 | 0.25 | 141 | 125 | 0.02 |
| 100 | 113 | 0.08 | 115 | 107 | 0.11 | 128 | 205 | 0.11 | 141 | 135 | 0.12 |
| 100 | 119 | 0.07 | 115 | 115 | 0.04 | 128 | 211 | 0.14 | 142 | 105 | 0.21 |
| 100 | 125 | 0.25 | 115 | 123 | 0.18 | 128 | 221 | 0.21 | 142 | 111 | 0.01 |
| 101 | 204 | 0.52 | 115 | 131 | 0.25 | 128 | 229 | 0.25 | 142 | 119 | 0.02 |
| | | | I | | | ı | | | ı | | |

| Sta | Smp | StdDev |
|-----|-----|--------|-----|-----|--------|-----|-----|--------|-----|-----|--------|
| 142 | 129 | 0.11 | 151 | 118 | 0.06 | 159 | 111 | 0.03 | 169 | 210 | 0.02 |
| 143 | 105 | 0.02 | 151 | 125 | 0.10 | 159 | 119 | 0.07 | 169 | 220 | 0.01 |
| 143 | 111 | 0.12 | 152 | 103 | 0.14 | 159 | 125 | 0.17 | 169 | 225 | 0.06 |
| 143 | 121 | 0.27 | 152 | 112 | 0.12 | 160 | 101 | 0.09 | 170 | 111 | 0.09 |
| 143 | 129 | 0.07 | 152 | 124 | 0.20 | 160 | 112 | 0.09 | 170 | 119 | 0.11 |
| 144 | 104 | 0.24 | 152 | 125 | 0.25 | 160 | 124 | 0.05 | 170 | 125 | 0.08 |
| 144 | 110 | 0.11 | 153 | 105 | 0.05 | 161 | 107 | 0.06 | 171 | 107 | 0.12 |
| 144 | 117 | 0.02 | 153 | 113 | 0.05 | 161 | 115 | 0.04 | 171 | 115 | 0.02 |
| 144 | 125 | 0.10 | 153 | 121 | 0.03 | 161 | 122 | 0.00 | 171 | 121 | 0.04 |
| 145 | 101 | 0.06 | 153 | 129 | 0.07 | 161 | 128 | 0.07 | 171 | 125 | 0.02 |
| 145 | 107 | 0.01 | 154 | 101 | 0.06 | 162 | 204 | 0.15 | 172 | 202 | 0.05 |
| 145 | 113 | 0.17 | 154 | 107 | 0.06 | 162 | 208 | 0.09 | 172 | 217 | 0.09 |
| 145 | 119 | 0.04 | 154 | 117 | 0.04 | 162 | 225 | 0.11 | 172 | 219 | 0.09 |
| 146 | 103 | 0.14 | 154 | 131 | 0.07 | 163 | 205 | 0.23 | 172 | 222 | 0.00 |
| 146 | 111 | 0.28 | 155 | 105 | 0.07 | 163 | 211 | 0.13 | 175 | 203 | 0.14 |
| 146 | 119 | 0.14 | 155 | 111 | 0.01 | 163 | 219 | 0.07 | 175 | 211 | 0.15 |
| 146 | 128 | 0.09 | 155 | 119 | 0.18 | 163 | 227 | 0.05 | 175 | 217 | 0.11 |
| 147 | 101 | 0.26 | 155 | 125 | 0.01 | 164 | 101 | 0.09 | 176 | 101 | 0.43 |
| 147 | 112 | 0.21 | 156 | 103 | 0.29 | 164 | 112 | 0.07 | 176 | 112 | 0.03 |
| 147 | 125 | 0.11 | 156 | 109 | 0.00 | 164 | 124 | 0.27 | 177 | 110 | 0.01 |
| 147 | 136 | 0.08 | 156 | 123 | 0.01 | 166 | 209 | 0.02 | 177 | 113 | 0.06 |
| 148 | 101 | 0.08 | 156 | 129 | 0.06 | 166 | 215 | 0.17 | 178 | 105 | 0.01 |
| 148 | 111 | 0.09 | 157 | 109 | 0.01 | 166 | 221 | 0.15 | 178 | 109 | 0.03 |
| 148 | 119 | 0.02 | 157 | 115 | 0.06 | 167 | 205 | 0.01 | 178 | 115 | 0.05 |
| 148 | 131 | 0.12 | 157 | 118 | 0.09 | 167 | 211 | 0.22 | 179 | 103 | 0.06 |
| 150 | 201 | 0.01 | 157 | 119 | 0.07 | 167 | 219 | 0.05 | 179 | 112 | 0.04 |
| 150 | 207 | 0.00 | 158 | 104 | 0.20 | 167 | 225 | 0.09 | 180 | 108 | 0.24 |
| 150 | 215 | 0.04 | 158 | 115 | 0.04 | 168 | 104 | 0.30 | 180 | 113 | 0.12 |
| 150 | 225 | 0.04 | 158 | 119 | 0.01 | 168 | 113 | 0.07 | 181 | 106 | 0.13 |
| 151 | 105 | 0.01 | 158 | 125 | 0.16 | 168 | 123 | 0.03 | 181 | 108 | 0.07 |
| 151 | 111 | 0.23 | 159 | 105 | 0.06 | 168 | 125 | 0.04 | 182 | 103 | 0.02 |
| | | | | | | | | | | | |

APPENDIX 5: Nutrient Measurement techniques on WOCE P14S and P15S (CGC96) (Calvin Mordy, NOAA-PMEL)

Nutrient samples were analyzed for dissolved phosphate, silicic acid, nitrate, and nitrite using protocols of Gordon et al., 1993. Samples were collected in 20 ml high-density polyethylene scintillation vials closed with teflon lined polyethylene caps. All vials and caps were rinsed with 10% HCl prior to each station. Samples were usually analyzed immediately after collection; however, several samples were stored for up to 12 hours at 4-6 degrees C. Samples were analyzed using an Alpkem RFA 300 modified with a custom heating coil and Spectro-100 UV/VIS detectors from Thermo Separation Products. Analytical temperatures were logged twice during every run and ranged from 16 to 25 degrees C. The following analytical methods were employed:

Phosphate was converted to phosphomolybdic acid and reduced with ascorbic acid to form phosphomolybdous acid in a reaction stream heated to 42 degrees C (Bernhardt and Wilhelms, 1967).

Silicic acid was converted to silicomolybdic acid and reduced with stannous chloride to form silicomolybdous acid or molybdenum blue (Armstrong, 1967).

Nitrite was diazotized with sulfanilamide and coupled with NEDA to form a red azo dye.

(NO3- + NO2-) was measured by first reducing nitrate to nitrite in a copperized cadmium coil, and then analyzing for nitrite. Nitrate was determined from the difference of (NO3- + NO2-) and NO2- (Armstrong, 1967).

Concentrations were converted to micromoles/kg by calculating sample densities using the laboratory temperature during analysis, the bottle or CTD salinity, and the international equation of state (UNESCO, 1981).

Primary standards were prepared by dissolving standard material in deionized water, and working standards were freshly made at each station in low nutrient seawater. Standard material for silicic acid was sodium fluorosilicate which had been referenced against a fused-quartz standard. All analysis were within the linear range of the instrument.

Analytical precision was determined from replicate analysis (2 to 7 measurements) on one or more samples at almost every station. Average standard deviations (micromoles/kg) for replicate analysis were 0.008 for phosphate (n = 205), 0.08 for silicic acid (n = 408), 0.05 for nitrate (n = 378) and 0.004 for nitrite (n = 15, for samples > 0.05 mmoles/kg).

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APPENDIX 6a: CFC-11 and CFC-12 Measurement techniques on WOCE P14S and P15S (Discussion provided by J.Bullister, NOAA-PMEL)

Specially designed 10 liter water sample bottles were used on the cruise to reduce CFC contamination. These bottles have the same outer dimensions as standard 10 liter Niskin bottles, but use a modified end-cap design to minimize the contact of the water sample with the end-cap O-rings after closing. The O-rings used in these water sample bottles were vacuum-baked prior to the first station. Stainless steel springs covered with a nylon powder coat were substituted for the internal elastic tubing standardly used to close Niskin bottles.

Water samples for CFC analysis were usually the first samples collected from the 10 liter bottles. Care was taken to co-ordinate the sampling of CFCs with other samples to minimize the time between the inital opening of each bottle and the completion of sample drawing. In most cases, dissolved oxygen, total CO2, alkalinity and pH samples were collected within several minutes of the initial opening of each bottle. To minimize contact with air, the CFC samples were drawn directly through the stopcocks of the 10 liter bottles into 100 ml precision glass syringes equipped with 2-way metal stopcocks. The syringes were immersed in a holding tank of clean surface seawater until analyses.

To reduce the possibility of contamination from high levels of CFCs frequently present in the air inside research vessels, the CFC extraction/analysis system and syringe holding tank were housed in a modified 20' laboratory van on the deck of the ship.

For air sampling, a ~100 meter length of 3/8" OD Dekaron tubing was run from the CFC lab van to the bow of the ship. Air was sucked through this line into the CFC van using an Air Cadet pump. The air was compressed in the pump, with the downstream pressure held at about 1.5 atm using a back-pressure regulator. A tee allowed a flow (~100 cc/min) of the compressed air to be directed to the gas sample valves, while the bulk flow of the air (>7 liter/minute) was vented through the back pressure regulator.

Concentrations of CFC-11 and CFC-12 in air samples, seawater and gas standards on the cruise were measured by shipboard electron capture gas chromatography (EC-GC), using techniques similiar to those described by Bullister and Weiss (1988). For seawater analyses, a ~30-ml aliquot of seawater from the glass syringe was transferred into the glass sparging chamber. The dissolved CFCs in the seawater sample were extracted by passing a supply of CFC-free purge gas through the sparging chamber for a period of 4 minutes at ~70 cc/min. Water vapor was removed from the purge gas while passing through a short tube of magnesium perchlorate dessicant. The sample gases were concentrated on a cold-trap consisting of a 3-inch section of 1/8-inch stainless steel tubing packed with Porapak N (60-80 mesh) immersed in a bath of isopropanol held at -20 degrees C. After 4 minutes of purging the seawater sample, the sparging chamber was closed and the trap isolated. The cold isopropanol in the bath was forced away from the trap which was heated electrically to 125 degrees C. The sample gases held in the trap were then injected onto a precolumn (12 inches of 1/8-inch O.D. stainless steel tubing packed with 80-100 mesh Porasil C, held at 90 degrees C), for the initial separation of the

CFCs and other rapidly eluting gases from more slowly eluting compounds. The CFCs then passed into the main analytical column (10 feet, 1/8-inch stainless steel tubing packed with Porasil C 80-100 mesh, held at 90 degrees C), and then into the EC detector.

The CFC analytical system was calibrated frequently using standard gas of known CFC composition. Gas sample loops of known volume were thoroughly flushed with standard gas and injected into the system. The temperature and pressure was recorded so that the amount of gas injected could be calculated. The procedures used to transfer the standard gas to the trap, precolumn, main chromatographic column and EC detector were similar to those used for analyzing water samples. Two sizes of gas sample loops were present in the analytical system. Multiple injections of these loop volumes could be done to allow the system to be calibrated over a relatively wide range of CFC concentrations. Air samples and system blanks (injections of loops of CFC-free gas) were injected and analyzed in a similar manner. The typical analysis time for seawater, air, standard and blank samples was about 12 minutes.

Concentrations of CFC-11 and CFC-12 in air, seawater samples and gas standards are reported relative to the SIO93 calibration scale (Cunnold, et. al., 1994). CFC concentrations in air and standard gas are reported in units of mole fraction CFC in dry gas, and are typically in the parts-per-trillion (ppt) range. Dissolved CFC concentrations are given in units of picomoles of CFC per kg seawater (pmol/kg). CFC concentrations in air and seawater samples were determined by fitting their chromatographic peak areas to multi-point calibration curves, generated by injecting multiple sample loops of gas from a CFC working standard (PMEL cylinder 33790) into the analytical instrument. The concentrations of CFC-11 and CFC-12 in this working standard were calibrated before and after the cruise versus a primary standard (36743) (Bullister, 1984). No measurable drift in the concentrations of CFC-11 and CFC-12 in the working standard could be detected during this interval. Full range calibration curves were run at intervals of ~ 3 days during the cruise. Single injections of a fixed volume of standard gas at one atmosphere were run much more frequently (at intervals of 1 to 2 hours) to monitor short term changes in detector sensitivity.

Extremely low (<0.01 pmol/kg) CFC concentrations were measured in deep water (2000-3000 meters) from about 30oS to the equator along the P15S section, as expected from CFC measurements made during the earlier occupation of this section in 1990 (Wisegarveret al, 1995), and from other transient tracer studies made in this region of the southwest Pacific. Based on the median of CFC concentration measurements in the deep water of this region, which is believed to be nearly CFC-free, a blank correction of 0.003 pmol/kg for CFC-11 and 0 pmol/kg for CFC-12 have been applied to the data set. For very low concentration water samples, subtraction of the water sample CFC-11 blank from the measured CFC-11 water sample concentration yields a small negative reported value.

On this expedition, we estimate precisions (1 standard deviation) of about 1% or 0.005 pmol/kg (whichever is greater) for dissolved CFC-11 and CFC-12 measurements (see listing of replicate samples given at the end of this report). A number of water samples had clearly anomolous CFC-11 and/or CFC-12 concentrations relative to adjacent

samples. These anomolous samples appeared to occur more or less randomly during the cruise, and were not clearly associated with other features in the water column (eg. elevated oxygen concentrations, salinity or temperature features, etc.). This suggests that the high values were due to individual, isolated low-level CFC contamination events. These samples are included in this report and are give a quality flag of either 3 (questionable measurement) or 4 (bad measurement). A total ~24 analyses of CFC-11 were assigned a flag of 3 and ~33 analyses of CFC-12 were assigned a flag of 3. A total of ~31 analyses of CFC-11 were assigned a flag of 4 and ~178 CFC-12 samples assigned a flag of 4.

A value of -9.0 is used for missing values in the listings.

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APPENDIX 6b: CFC Air Measurements on P14S and P15S (CGC96)

(interpolated to station locations)

| STATION NUMBER | Latitude | Longitude | Date | F11 PPT | F12 PPT |
|-------------------|------------------------|--------------------------|------------------------|----------------|----------------|
| 1 | 45 49.5 S | 153 05.1 E | 6 Jan 96 | 260.5 | 519.1 |
| 2 | 48 19.1 S | 158 29.9 E | 7 Jan 96 | 260.5 | 519.1 |
| 3 | 50 05.0 S | 162 29.3 E | 8 Jan 96 | 260.5 | 519.1 |
| 4 | 53 00.1 S | 169 59.3 E | 9 Jan 96 | 260.5 | 519.1 |
| 5 | 53 29.9 S | 170 29.7 E | 9 Jan 96 | 260.5 | 519.1 |
| 6 | 53 59.9 S | 171 00.1 E | 9 Jan 96 | 260.5 | 519.1 |
| 7 | 54 10.2 S | 171 10.8 E | 9 Jan 96 | 260.5 | 519.1 |
| 8 | 54 19.8 S | 171 20.2 E | 9 Jan 96 | 260.5 | 519.1 |
| 9 | 54 30.3 S | | 9 Jan 96 | 260.4 | |
| 10 | 54 59.7 S | | 10 Jan 96 | 260.5 | |
| 11 | 55 30.4 S | 172 27.0 E | 10 Jan 96 | 260.2 | 519.5 |
| 12 | 55 59.8 S | 173 00.6 E | 10 Jan 96 | 260.2 | 519.5 |
| 13 | 56 29.2 S | 173 30.2 E | 11 Jan 96 | 260.2 | 519.4 |
| 14 | 56 59.7 S | 173 58.6 E | 11 Jan 96 | 260.2 | 519.4 |
| 15 | 57 30.3 S | 173 58.5 E | 11 Jan 96 | 260.2 | 519.4 |
| 16 | 58 00.2 S | 173 59.5 E | 12 Jan 96 | 260.2 | 519.4 |
| 17 | 58 30.2 S | 173 58.2 E | 12 Jan 96 | 260.4 | 519.7 |
| 18 | 58 59.8 S | 174 00.0 E | 12 Jan 96 | | |
| 19 | 59 28.7 S | 173 59.7 E | 12 Jan 96 | | |
| 20 | 59 57.9 S | 173 57.9 E | 13 Jan 96 | | |
| 21 | 60 30.3 S | | 13 Jan 96 | 259.4 | 519.3 |
| 22 | 60 59.1 S | 173 58.9 E | 14 Jan 96 | 259.4 | 519.3 |
| 23 | 61 30.0 S | 174 00.2 E | 14 Jan 96 | 259.4 | 519.3 |
| 24 | 62 00.0 S | 173 16.1 E | 14 Jan 96 | 259.4 | 519.3 |
| 25 26 | 62 26.9 S 62 44.7 S | 172 35.2 E 172 09.0 E | 14 Jan 96 | 259.4 259.4 | 519.3 519.3 |
| 26 27 | 62 44.7 S | 172 09.0 E 171 44.9 E | 15 Jan 96 15 Jan 96 | 259.4 | |
| 28 | 63 30.1 S | 170 59.6 E | 15 Jan 96 | 259.4 | |
| 29 | 63 59.8 S | 171 06.6 E | 16 Jan 96 | 259.4 | 519.3 |
| 30 | 64 40.6 S | 170 58.6 E | 16 Jan 96 | 259.4 | 519.3 |
| 31 | 65 20.2 S | 170 60.0 E | 16 Jan 96 | 259.4 | 519.3 |
| 32 | 66 00.9 S | 171 01.6 E | 17 Jan 96 | 259.4 | 519.3 |
| 33 | 66 59.6 S | 170 00.0 W | 18 Jan 96 | 261.4 | 522.5 |
| 34 | 66 20.3 S | 169 60.0 W | 18 Jan 96 | 261.4 | 522.5 |
| 35 | | 170 00.3 W | | | |
| 36 | | 170 00.9 W | | | |
| 37 | 64 30.1 S | 169 59.9 W | 19 Jan 96 | 260.3 | 523.7 |
| 38 | 63 59.7 S | 170 02.0 W | 19 Jan 96 | 260.3 | 523.7 |
| 39 | 63 30.1 S | 170 00.3 W | 20 Jan 96 | 260.3 | 523.7 |
| 40 | 62 59.7 S | 170 01.4 W | 20 Jan 96 | 260.0 | 522.5 |
| 41 | 62 30.0 S | 169 59.8 W | 20 Jan 96 | 259.3 | 521.5 |
| 42 | 62 00.2 S | 169 59.9 W | 20 Jan 96 | 259.3 | 521.5 |
| 43 | 61 29.5 S | 169 60.0 W | 21 Jan 96 | 259.2 | 523.0 |
| 44 | 61 00.1 S | 170 00.3 W | 21 Jan 96 | 259.2 | 523.0 |
| 45 | 60 29.7 S | 169 59.6 W | 22 Jan 96 | 259.0 | 522.9 |
| 46 | 60 00.3 S | 170 00.3 W | 22 Jan 96 | 259.0 | 522.9 |
| 47 | 59 30.2 S | 169 59.9 W | 22 Jan 96 | 259.0 | 522.9 |
| 48 | 58 59.9 S | 170 00.2 W | 22 Jan 96 | 259.8 | 524.5 |
| 49 | 58 29.6 S | 170 00.8 W | 23 Jan 96 | 259.8 | 524.5 |

| STATION NUMBER | | Longitude | Date | | F12 PPT |
|-------------------|------------------------|--|----------------------|----------------|----------------|
| 50 | | 170 00.8 W | | | |
| 51 | 57 30.1 S | 170 00.4 W | 23 Jan 96 | 259.8 | 524.5 |
| 52 | 57 00.2 S | 170 00.2 W | 24 Jan 96 | 259.8 | 524.5 |
| 53 | 56 29.9 S | 169 59.8 W | 24 Jan 96 | 259.8 | 524.5 |
| 54 | 55 60.0 S | 170 01.8 W | 24 Jan 96 | 261.8 | 521.8 |
| 55 | 55 29.9 S | | | | |
| 56 | 54 59.8 S | 169 60 0 W | 25 Jan 96 | 261.2 | 520.6 |
| 57 | 54 29.4 S | 170 00.1 W | 25 Jan 96 | 261.2 | |
| 58 | 54 00.1 S | 169 59.3 W | 25 Jan 96 | 261.2 | |
| 59 | | 169 59.4 W | | | |
| 60 | | 169 59.6 W | | | |
| 61 | | 170 00.5 W | | | |
| 62 | 52 29.9 S | | | | |
| 63 | 52 00.1 S | | 26 Jan 96 | 261.3 | 520.1 |
| 64 | 51 30.0 S | | 27 Jan 96 | 261.3 | 520.1 |
| 65 | 51 00.2 S | 170 00.4 W 169 59.6 W | 27 Jan 96 | 261.3 | 520.1 |
| 66 | 50 29.9 S | 169 59.6 W | 27 Jan 96 | 260.2 | 519.6 |
| 67 | 50 00.4 S | 169 59.9 W | 28 Jan 96 | | |
| 68 | | 170 00.9 W | | | |
| 69 | | 169 59.4 W | | | |
| 70 | | 170 00.2 W | | | |
| 71 | | 170 00.3 W | | | |
| 72 | 47 30.2 S | | 29 Jan 96 | 260.4 | 520.1 |
| 73 | 47 06.5 S | 170 27.7 W 170 54.7 W | 29 Jan 96 | 260.4 | 520.1 |
| 74 | 46 43.4 S | 170 54.7 W | 30 Jan 96 | 260.4 | 520.1 |
| 75 | 46 20.0 S | 171 22.2 W | 30 Jan 96 | 260.4 | 520.1 |
| 76 | 45 57.0 S | | 30 Jan 96 | | |
| 77 | 45 33.6 S | | | | |
| 78 | 45 10.6 S | | | | |
| 79 | 44 50.1 S | | | | |
| 80 | 44 31.8 S | | | | |
| 81 | 44 19.2 S | 173 44.7 W | 31 Jan 96 | 261.0 | 520.5 |
| 82 | 44 U9.4 S | 173 56.3 W 174 17.7 W 174 32.2 W | 1 Feb 96 | ∠b⊥.U | 520.5 |
| 83 | 43 50.9 S | 1/4 1/./ W | 1 Feb 96 | ∠61.U | 520.5 |
| 84 85 | 43 30.0 S | 174 32.2 W 174 59.9 W | 1 Feb 96 | 261.0 | 520.5 |
| | 43 15.2 S 42 55.9 S | | | | |
| 86 87 | | 174 47.2 W | 1 Feb 96 | 261.0 | 520.5 |
| 87 88 | 42 44.8 S 42 24.1 S | 174 39.3 W 174 24.4 W | 1 Feb 96 1 Feb 96 | 261.0 261.0 | 520.5 520.5 |
| 89 | 42 24.1 S 42 10.0 S | 174 24.4 W 174 15.0 W | 2 Feb 96 | 261.0 | 520.5 |
| 90 | 41 42.8 S | 174 15.0 W | 2 Feb 96 2 Feb 96 | 261.0 | 520.5 |
| 91 | 41 42.8 S 41 16.0 S | 173 38.6 W | 2 Feb 96 | 261.0 | 520.5 |
| 92 | 40 49.5 S | 173 19.5 W | 2 Feb 96 | 261.0 | 520.5 |
| 93 | 40 43.5 S | 173 12.3 W | 2 Feb 96 | 261.0 | 520.5 |
| 94 | 40 23.5 S | 173 02.0 W | 13 Feb 96 | 260.4 | 520.5 |
| 95 | 39 57.7 S | 173 01.7 W | 14 Feb 96 | 260.4 | 521.7 |
| 96 | 39 31.0 S | 172 42.2 W | 14 Feb 96 | 260.1 | 521.7 |
| 97 | 39 04.3 S | 172 23.2 W | 14 Feb 96 | 260.1 | 521.7 |
| 98 | 38 37.8 S | 172 07.7 W | 14 Feb 96 | 260.1 | 521.7 |
| , , | 20 27.0 2 | W | | 260.1 | 521.7 |

| | | Longitude | | | F12 PPT |
|-----|-----------|--------------------------|-------------|-----------|------------|
| 100 | | 171 12.0 W | | 260.1 | |
| 101 | | 170 53.7 W | | | |
| 102 | | 170 37.0 W | | | 521.7 |
| 103 | 36 27.0 S | | | | 521.9 |
| 104 | 36 00.2 S | 170 00.3 W | 16 Feb 96 | | 521.9 |
| 105 | 35 40.3 S | 170 00.9 W | 16 Feb 96 | | 521.9 |
| 106 | 35 20.0 S | 170 00.1 W | 16 Feb 96 | 260.8 | 521.9 |
| 107 | 35 00.5 S | 170 00.1 W 169 59.6 W | 17 Feb 96 | 260.8 | 521.9 |
| 108 | 34 30.2 S | 170 00.2 W | | 260.8 | 521.9 |
| 109 | 33 59.8 S | | | | 521.9 |
| 110 | 33 29.9 S | | | | 521.9 |
| 111 | 33 00.1 S | | | | 521.9 |
| 112 | 32 30.1 S | | | | 521.9 |
| 113 | 31 59.8 S | | | | 521.9 |
| 114 | 31 30.0 S | | 19 Feb 96 | 260.6 | 521.7 |
| 115 | 31 00.4 S | 169 59.3 W 169 59.7 W | 19 Feb 96 | 260.6 | 521.9 |
| 116 | 30 30.3 S | 169 59.8 W | 19 Feb 96 | 260.6 | 521.9 |
| 117 | 30 00.2 S | | 19 Feb 96 | 260.6 | 521.9 |
| 118 | 29 30.2 S | 169 59.8 W | 20 Feb 96 | 260.6 | 521.9 |
| 119 | 29 00.8 S | | | 260.6 | 521.9 |
| 120 | 28 30.5 S | 169 59.8 W | 20 Feb 96 | 260.6 | 521.9 |
| 121 | 28 00.3 S | 169 59.6 W | 21 Feb 96 | 260.6 | 521.9 |
| 122 | 27 30.1 S | | 21 Feb 96 | 260.6 | 521.9 |
| 123 | 27 00.3 S | 169 59.5 W 169 59.4 W | 21 Feb 96 | 260.8 | 522.1 |
| 124 | 26 29.7 S | 169 59.4 W | 21 Feb 96 | 260.6 | 521.9 |
| 125 | 26 00.3 S | 169 59.7 W | | 260.6 | 521.9 |
| 126 | 25 30.0 S | 169 60.0 W | 22 Feb 96 | 260.6 | 521.9 |
| 127 | 25 00.1 S | | 22 1 00 7 0 | | 522.3 |
| 128 | 24 30.1 S | 170 00.1 W | 23 Feb 96 | 260.9 | 522.3 |
| 129 | 23 59.8 S | | 23 Feb 96 | 261.3 | 522.7 |
| 130 | 23 30.1 S | | | | 522.7 |
| 131 | 22 59.8 S | 169 59.7 W | 23 Feb 96 | 261.3 | 522.7 |
| 132 | 22 30.0 S | 169 59.9 W 169 59.9 W | 24 Feb 96 | 261.3 | 522.7 |
| 133 | 22 00.0 S | 169 59.9 W | 24 Feb 96 | 261.3 | 522.7 |
| 134 | 21 30.4 S | 170 00.1 W | 24 Feb 96 | 261.3 | 522.7 |
| 135 | | 169 59.6 W | 25 Feb 96 | | 524.4 |
| 136 | 20 29.9 S | 170 00.1 W | 25 Feb 96 | 262.1 | 524.4 |
| 137 | 20 00.0 S | 170 00.1 W | 25 Feb 96 | 262.1 | 524.4 |
| 138 | 19 29.9 S | 170 00.1 W | 25 Feb 96 | 262.1 | 524.4 |
| 139 | 19 00.1 S | 170 03.4 W | 26 Feb 96 | 262.1 | 524.4 |
| 140 | 18 30.3 S | 170 00.1 W | 26 Feb 96 | 262.1 | 524.4 |
| 141 | 17 60.0 S | 169 60.0 W | 26 Feb 96 | 262.1 | 524.4 |
| 142 | 17 30.1 S | 169 60.0 W | 26 Feb 96 | 262.1 | 524.4 |
| 143 | 17 00.1 S | 169 59.8 W | 27 Feb 96 | 262.3 | 525.0 |
| 144 | 16 30.3 S | 169 59.9 W | 27 Feb 96 | 262.7 | 525.9 |
| 145 | 16 00.2 S | 169 59.9 W | 27 Feb 96 | 262.7 | 525.9 |
| 146 | 15 29.8 S | 170 00.1 W | 27 Feb 96 | 262.8 | 525.6 |
| 147 | 15 00.2 S | 170 00.0 W | 28 Feb 96 | 262.8 | 525.6 |
| 148 | 14 40.0 S | 169 59.9 W | 28 Feb 96 | 262.9 | 525.5 |
| 149 | 14 16.9 S | 169 59.8 W | 28 Feb 96 | 262.9 | 525.5 |

| STATION NUMBER | Latitude | Longitude | Date | F11 PPT | F12 PPT |
|-------------------|-----------|------------|-----------|------------|------------|
| 150 | 13 58.3 S | 169 60.0 W | 28 Feb 96 | 262.9 | 525.5 |
| 151 | 13 49.1 S | 170 00.1 W | 28 Feb 96 | 262.9 | 525.5 |
| 152 | 13 30.1 S | 169 60.0 W | 29 Feb 96 | 262.9 | 525.5 |
| 153 | 12 59.9 S | 170 00.0 W | 29 Feb 96 | 262.9 | 525.5 |
| 154 | 12 29.9 S | 169 59.9 W | 29 Feb 96 | 262.9 | 525.5 |
| 155 | 12 00.1 S | 170 00.1 W | 29 Feb 96 | 262.9 | 525.5 |
| 156 | 11 30.0 S | 169 59.9 W | 1 Mar 96 | 262.9 | 525.5 |
| 157 | 11 00.1 S | 169 59.9 W | 1 Mar 96 | 262.9 | 525.5 |
| 158 | 10 30.1 S | 169 59.8 W | 1 Mar 96 | 262.9 | 525.5 |
| 159 | 09 55.6 S | 169 37.7 W | 1 Mar 96 | 262.6 | 525.3 |
| 160 | 09 30.1 S | 168 59.9 W | 2 Mar 96 | 262.6 | 525.3 |
| 161 | 08 59.9 S | 168 52.6 W | 2 Mar 96 | 262.6 | 525.0 |
| 162 | 08 29.9 S | 168 44.9 W | 2 Mar 96 | 262.6 | 525.0 |
| 163 | 08 00.0 S | 168 37.0 W | 2 Mar 96 | 262.6 | 525.0 |
| 164 | 07 30.1 S | 168 44.9 W | 3 Mar 96 | 262.6 | 525.0 |
| 165 | 06 60.0 S | 168 44.9 W | 3 Mar 96 | 262.8 | 526.1 |
| 166 | 06 30.1 S | 168 44.9 W | 3 Mar 96 | 262.7 | 526.5 |
| 167 | 06 00.0 S | 168 45.0 W | 4 Mar 96 | 262.7 | 526.5 |
| 168 | 05 30.1 S | 168 45.0 W | 4 Mar 96 | 262.7 | 526.5 |
| 169 | 05 00.0 S | 168 44.9 W | 4 Mar 96 | 262.7 | 526.5 |
| 170 | 03 60.0 S | 168 45.1 W | 4 Mar 96 | 262.7 | 526.5 |
| 171 | 03 00.0 S | 168 45.0 W | 5 Mar 96 | 263.0 | 527.3 |
| 172 | 02 00.1 S | 168 45.0 W | 5 Mar 96 | 263.5 | 528.4 |
| 173 | 01 00.1 S | 168 45.2 W | 6 Mar 96 | 263.5 | 528.4 |
| 174 | 00 00.1 S | 168 45.0 W | 6 Mar 96 | 263.5 | 528.4 |
| 175 | 07 44.8 S | 168 40.2 W | 8 Mar 96 | 262.7 | 526.5 |
| 176 | 08 15.1 S | 168 41.3 W | 8 Mar 96 | 262.7 | 526.5 |
| 177 | 10 08.7 S | 168 58.8 W | 8 Mar 96 | 262.7 | 526.5 |
| 178 | 10 04.1 S | 169 12.7 W | 8 Mar 96 | 262.7 | 526.5 |
| 179 | 09 55.2 S | 169 37.7 W | 9 Mar 96 | 262.7 | 526.5 |
| 180 | 09 47.0 S | 170 03.5 W | 9 Mar 96 | 262.7 | 526.5 |
| 181 | 09 41.6 S | 170 19.5 W | 9 Mar 96 | 262.7 | 526.5 |
| 182 | 09 35.7 S | 170 36.1 W | 9 Mar 96 | 262.7 | 526.5 |

APPENDIX 6c: Replicate CFC-11 measurements on P14S and P15S (CGC96)

| STATION NUMBER | SAMP NO. | F11 pM/kg | F11 Stdev | STATION NUMBER | SAMP NO. | F11 pM/kg | F11 Stdev |
|-------------------|-------------|----------------|----------------|-------------------|-------------|----------------|----------------|
| 1 | 112 | 0.092 | 0.007 | 45 | 110 | 0.184 | 0.002 |
| 4 | 110 | 4.157 | 0.012 | 45 | 115 | 1.009 | 0.013 |
| 5 | 113 | 4.117 | 0.008 | 45 | 123 | 5.791 | 0.022 |
| 9 | 202 | 0.136 | 0.015 | 46 | 103 | 0.049 | 0.007 |
| 9 | 234 | 4.672 | 0.035 | 46 | 129 | 5.699 | 0.029 |
| 10 | 201 | 0.155 | 0.003 | 48 | 101 | 0.060 | 0.001 |
| 10 | 211 | 0.050 | 0.001 | 48 | 110 | 0.034 | 0.001 |
| 10 | 214 | 0.095 | 0.004 | 49 | 101 | 0.080 | 0.001 |
| 11 | 101 | 0.148 | 0.007 | 49 | 111 | 0.044 | 0.005 |
| 14 | 101 | 0.143 | 0.000 | 49 | 120 | 0.727 | 0.001 |
| 14 | 134 | 4.542 | 0.030 | 49 | 129 | 4.880 | 0.019 |
| 15 | 201 | 0.144 | 0.001 | 50 | 104 | 0.045 | 0.008 |
| 15 | 234 | 4.674 | 0.009 | 50 | 116 | 0.198 | 0.008 |
| 16 | 101 | 0.148 | 0.002 | 50 | 132 | 5.214 | 0.038 |
| 16 | 110 | 0.047 | 0.003 | 52 | 101 | 0.090 | 0.000 |
| 17 | 103 | 0.134 | 0.002 | 52 | 110 | 0.040 | 0.009 |
| 17 | 133 | 5.035 | 0.037 | 52 | 113 | 0.058 | 0.002 |
| 18 | 134 | 4.864 | 0.061 | 52 | 121 | 1.006 | 0.009 |
| 21 | 123 | 5.464 | 0.042 | 52 | 132 | 5.044 | 0.006 |
| 25 | 110 | 0.087 | 0.001 | 53 | 103 | 0.084 | 0.003 |
| 28 | 101 | 0.180 | 0.005 | 53 | 125 | 3.138 | 0.019 |
| 28 | 112 | 0.226 | 0.001 | 54 | 102 | 0.082 | 0.017 |
| 28 | 124 | 6.359 | 0.131 | 54 | 114 | 0.074 | 0.000 |
| 29 | 201 | 0.496 | 0.001 | 54 | 132 | 4.758 | 0.088 |
| 29 | 212 | 0.250 | 0.001 | 56 | 103 | 0.078 | 0.000 |
| 29 | 230 | 6.393 | 0.097 | 56 | 111 | 0.070 | 0.001 |
| 30 | 101 | 1.373 | 0.007 | 56 | 132 | 4.654 | 0.025 |
| 30 | 133 | 6.172 | 0.033 | 57 | 103 | 0.073 | 0.023 |
| 31 | 203 | 1.422 | 0.033 | 58 | 211 | 0.075 | 0.004 |
| 31 | 225 | 0.662 | 0.019 | 58 | 232 | 4.508 | 0.036 |
| 32 | 111 | 0.002 | 0.006 | 61 | 103 | 0.086 | 0.006 |
| 32 | 115 | 0.124 | 0.006 | 61 | 113 | 0.083 | 0.003 |
| 33 | 103 | 0.124 | 0.002 | 61 | 123 | 3.373 | 0.003 |
| 33 | 131 | 4.790 | 0.014 | 61 | 131 | 4.015 | 0.003 |
| 34 | 101 | 0.579 | 0.006 | 62 | 203 | 0.068 | 0.003 |
| 34 | 103 | 0.542 | 0.000 | 63 | 103 | 0.052 | 0.003 |
| 34 | 103 | 0.190 | 0.001 | 63 | 122 | 4.015 | 0.002 |
| 35 | 107 | 0.190 | 0.003 | 65 | 101 | 0.090 | 0.021 |
| 35 | 101 | 0.524 | 0.004 | 65 | 110 | 0.090 | 0.002 |
| 35 | 133 | 6.287 | 0.029 | 65 | 114 | 2.096 | 0.003 |
| 39 | 101 | | | 65 | 122 | 4.111 | |
| 39 | 101 | 0.128 | 0.001 0.107 | 66 | | | 0.004 |
| 39 | 121 | 6.277 6.638 | 0.107 | 66 | 101 133 | 0.082 3.836 | 0.001 0.007 |
| | | | | | | | |
| 40 40 | 101 133 | 0.108 6.720 | 0.005 0.006 | 67 67 | 202 233 | 0.071 | 0.000 |
| | | | | 68 | | 3.457 | 0.002 |
| 41 | 103 | 0.077 | 0.007 | 69 | 102 | 0.067 | 0.003 |
| 41 | 133 | 6.678 | 0.030 | | 201 | 0.080 | 0.001 |
| 42 | 101 | 0.093 | 0.001 | 69 70 | 231 | 3.791 | 0.000 |
| 42 | 133 | 6.521 | 0.013 | 70 | 101 | 0.072 | 0.001 |
| 43 | 111 | 0.186 | 0.000 | 70 | 107 | 0.026 | 0.000 |
| 43 | 120 | 5.799 | 0.006 | 71 | 104 | 0.051 | 0.001 |

| STATION NUMBER | SAMP NO. | F11 pM/kg | F11 Stdev | STATION NUMBER | SAMP NO. | F11 pM/kg | |
|-------------------|-------------|----------------|--------------|-------------------|-------------|----------------|----------------|
| | 128 | | 0.007 | 106 | 134 | | 0.013 |
| 71 72 | 101 | 4.000 0.084 | 0.007 | 108 | | | |
| 73 | | 0.004 | 0.005 | 108 | | | |
| 73 | 115 | 0.070 | 0.003 | 109 | | | |
| 73 | 133 | 3.444 | 0.003 | 110 | | | 0.001 |
| 74 | 202 | 0.088 | 0.006 | 110 | | 2.336 | 0.001 |
| 75 | 102 | 0.095 | 0.001 | 112 | 102 | 0.020 | 0.023 |
| 75 | 128 | 3.592 | 0.027 | 112 | 132 | 2.632 | 0.008 |
| 76 | 201 | 0.101 | 0.003 | 113 | 101 | 0.015 | 0.000 |
| 76 | 203 | 0.082 | 0.001 | 114 | 104 | 0.012 | 0.000 |
| 76 | 208 | 0.037 | 0.003 | 114 | | 2.035 | 0.006 |
| 77 | 102 | 0.089 | 0.000 | 115 | | | 0.001 |
| 77 | 112 | 0.063 | 0.002 | 116 | | | 0.001 |
| 77 | 133 | 3.101 | 0.001 | 116 | | | 0.000 |
| 78 | 101 | 0.094 | 0.005 | 116 | | 0.596 | 0.005 |
| 79 | 102 | 0.045 | 0.001 | 116 | 234 | 1.946 | 0.007 |
| 79 | 132 | 2.876 | 0.002 | 117 | 101 | 0.013 | 0.002 |
| 80 | 203 | 0.030 | 0.004 | 117 | 107 | 0.005 | 0.000 |
| 81 | 109 | 0.796 | 0.004 | 118 | 103 | 0.011 | 0.000 |
| 83 | 101 | 0.372 | 0.002 | 118 | 128 | | 0.001 |
| 83 | 105 | 1.986 | 0.003 | 119 | | | 0.002 |
| 86 | | 0.199 | 0.006 | 120 | | | 0.000 |
| 87 | 101 | 0.030 | 0.003 | 120 | | | 0.001 |
| 88 | 101 | 0.016 | 0.001 | 120 | 227 | 1.996 | 0.040 |
| 88 | 104 | 0.005 | 0.001 | 120 | 234 | 2.237 | 0.008 |
| 88 | 113 | 1.807 | 0.007 | 121 | 201 | 0.010 | 0.001 |
| 88 | 125 | 3.050 | 0.021 | 122 | 102 | 0.011 | 0.000 |
| 89 | 202 | 0.018 | 0.000 | 122 | 105 | 0.004 | 0.002 |
| 89 | 206 | 0.012 | 0.003 | 122 | 132 | 2.404 | 0.000 |
| 89 | 232 | 2.466 | 0.001 | 123 | 101 | 0.009 | 0.000 |
| 90 | 103 | 0.012 | 0.003 | 124 | 101 | 0.009 | 0.000 |
| 92 | 201 | 0.054 | 0.004 | 124 | 130 | 2.283 | 0.015 |
| 93 | 102 | 0.058 | 0.000 | 124 | | 1.766 | 0.003 |
| 94 | 102 | 0.055 | 0.002 | 125 | 303 | 0.009 | 0.001 |
| 94 | 112 | 0.009 | 0.002 | 125 | 334 | 1.959 | 0.018 |
| 94 | 130 | 2.911 | 0.013 | 126 | 101 | 0.008 | 0.001 |
| 95 | 101 | 0.065 | 0.000 | 126 | 132 | 2.142 | 0.012 |
| 96 | 102 | 0.055 | 0.001 | 127 | 201 | 0.013 | 0.000 |
| 96 | 119 | 0.344 | 0.008 | 127 | 210 | 0.001 | 0.001 |
| 96 | 135 | 2.563 | 0.001 | 127 | 226 | 1.524 | 0.002 |
| 97 | 201 | 0.068 | 0.002 | 127 | 235 | 1.814 | 0.013 |
| 98 | 102 | 0.046 | 0.002 | 128 | 201 | 0.013 | 0.002 |
| 98 | 134 | 2.506 | 0.007 | 129 | 102 | 0.009 | 0.000 |
| 100 | 101 | 0.067 | 0.006 | 129 | 135 | 1.755 | 0.020 |
| 100 | 118 | 0.095 | 0.000 | 130 | 101 | 0.011 | 0.001 |
| 101 | 227 | 2.735 | 0.014 | 130 | 107 | 0.007 | 0.001 |
| 102 | 102 | 0.031 | 0.000 | 130 | 125 | 1.222 | 0.006 |
| 102 | 124 | 1.114 | 0.008 | 131 | 134 | 1.935 | 0.008 |
| 104 | 101 | 0.029 | 0.001 | 132 | 102 | 0.013 | 0.001 |
| 104 | 132 | 3.014 | 0.022 | 132 | 119 | 0.003 | 0.001 |
| 105 | 201 | 0.018 | 0.002 | 132 | 133 | 1.930 | 0.011 |
| 105 | 203 | 0.006 | 0.001 | 133 | 101 | 0.011 | 0.001 |
| 105 106 | 205 | 0.002 | 0.002 | 134 134 | 201 235 | 0.012 1.630 | 0.000 0.005 |
| TOD | 102 | 0.029 | 0.000 | 134 | 433 | 1.030 | 0.005 |

| STATION NUMBER | SAMP NO. | F11 pM/kg | F11 Stdev | STATION NUMBER | SAMP NO. | F11 pM/kg | F11 Stdev |
|-------------------|-------------|--------------|--------------|-------------------|-------------|--------------|--------------|
| 135 | 201 | 0.013 | 0.002 | 158 | 102 | 0.006 | 0.000 |
| 135 | 215 | -0.001 | 0.002 | 159 | 102 | 0.008 | 0.002 |
| 135 | 234 | 1.919 | 0.001 | 159 | 103 | 0.005 | 0.001 |
| 136 | 103 | 0.010 | 0.000 | 159 | 134 | 1.553 | 0.012 |
| 137 | 101 | 0.010 | 0.002 | 160 | 103 | 0.006 | 0.001 |
| 137 | 121 | 0.003 | 0.002 | 161 | 103 | 0.003 | 0.001 |
| 137 | 133 | 1.892 | 0.002 | 161 | 131 | 1.715 | 0.014 |
| 140 | 102 | 0.009 | 0.000 | 162 | 201 | 0.005 | 0.001 |
| 140 | 133 | 1.872 | 0.004 | 163 | 201 | 0.005 | 0.000 |
| 141 | 101 | 0.011 | 0.001 | 163 | 229 | 1.620 | 0.002 |
| 142 | 102 | 0.015 | 0.002 | 164 | 104 | 0.002 | 0.001 |
| 142 | 123 | 0.071 | 0.000 | 166 | 201 | 0.003 | 0.001 |
| 142 | 135 | 1.641 | 0.007 | 167 | 201 | 0.003 | 0.002 |
| 143 | 101 | 0.011 | 0.000 | 167 | 230 | 1.936 | 0.007 |
| 144 | 102 | 0.006 | 0.001 | 169 | 201 | 0.004 | 0.001 |
| 144 | 129 | 1.962 | 0.011 | 169 | 226 | 0.055 | 0.002 |
| 145 | 103 | 0.005 | 0.002 | 169 | 235 | 1.666 | 0.013 |
| 146 | 102 | 0.007 | 0.001 | 170 | 101 | 0.004 | 0.001 |
| 146 | 125 | 0.351 | 0.001 | 170 | 129 | 1.045 | 0.003 |
| 146 | 131 | 1.827 | 0.011 | 171 | 101 | 0.005 | 0.001 |
| 147 | 101 | 0.009 | 0.000 | 171 | 128 | 0.343 | 0.003 |
| 148 | 121 | 0.719 | 0.000 | 172 | 221 | 0.176 | 0.000 |
| 150 | 234 | 1.566 | 0.003 | 172 | 233 | 1.741 | 0.001 |
| 151 | 102 | 0.006 | 0.001 | 173 | 201 | 0.003 | 0.002 |
| 151 | 135 | 1.552 | 0.018 | 173 | 225 | 0.056 | 0.004 |
| 152 | 101 | 0.007 | 0.002 | 173 | 231 | 1.689 | 0.001 |
| 153 | 102 | 0.006 | 0.000 | 174 | 101 | -0.000 | 0.000 |
| 153 | 132 | 1.689 | 0.002 | 175 | 204 | 0.003 | 0.000 |
| 154 | 101 | 0.006 | 0.001 | 176 | 101 | 0.005 | 0.001 |
| 154 | 103 | 0.006 | 0.000 | 177 | 101 | 0.003 | 0.000 |
| 155 | 102 | 0.006 | 0.000 | 177 | 104 | 0.000 | 0.000 |
| 155 | 122 | 0.009 | 0.001 | 178 | 101 | 0.005 | 0.000 |
| 155 | 134 | 1.566 | 0.003 | 179 | 101 | 0.005 | 0.000 |
| 156 | 102 | 0.008 | 0.002 | 180 | 101 | 0.005 | 0.001 |
| 157 | 104 | 0.004 | 0.001 | 181 | 101 | 0.006 | 0.000 |
| | | | | 182 | 101 | 0.006 | 0.001 |

APPENDIX 6d. Replicate CFC-12 measurements on P14S and P15S (CGC96)

| STATION NUMBER | SAMP NO. | F12 pM/kg | F12 Stdev | STATION NUMBER | SAMP NO. | F12 pM/kg | F12 Stdev |
|-------------------|-------------|--------------|----------------|-------------------|-------------|--------------|--------------|
| 1 | 112 | 0.043 | 0.007 | 45 | 123 | 2.837 | 0.029 |
| 4 | 110 | 2.188 | 0.007 | 46 | 103 | 0.025 | 0.001 |
| 5 | 113 | 2.131 | 0.012 | 46 | 129 | 2.800 | 0.030 |
| 9 | 202 | 0.070 | 0.007 | 48 | 101 | 0.028 | 0.001 |
| 9 | 234 | 2.408 | 0.013 | 48 | 110 | 0.025 | 0.002 |
| 10 | 201 | 0.080 | 0.003 | 49 | 101 | 0.040 | 0.001 |
| 10 | 214 | 0.050 | 0.002 | 49 | 111 | 0.027 | 0.004 |
| 11 | 101 | 0.083 | 0.010 | 49 | 120 | 0.349 | 0.003 |
| 14 | 101 | 0.070 | 0.001 | 49 | 129 | 2.413 | 0.021 |
| 14 | 134 | 2.317 | 0.007 | 50 | 104 | 0.027 | 0.000 |
| 15 | 201 | 0.072 | 0.002 | 50 | 116 | 0.097 | 0.001 |
| 15 | 234 | 2.395 | 0.011 | 50 | 132 | 2.642 | 0.018 |
| 16 | 101 | 0.070 | 0.003 | 52 | 101 | 0.044 | 0.001 |
| 16 | 110 | 0.021 | 0.002 | 52 | 110 | 0.021 | 0.006 |
| 17 | 103 | 0.066 | 0.001 | 52 | 113 | 0.030 | 0.004 |
| 17 | 133 | 2.571 | 0.031 | 52 | 121 | 0.476 | 0.008 |
| 18 | 134 | 2.457 | 0.015 | 52 | 132 | 2.556 | 0.008 |
| 21 | 123 | 2.772 | 0.035 | 53 | 103 | 0.046 | 0.000 |
| 25 | 110 | 0.038 | 0.004 | 53 | 125 | 1.531 | 0.004 |
| 28 | 101 | 0.082 | 0.003 | 54 | 102 | 0.044 | 0.002 |
| 28 | 112 | 0.106 | 0.001 | 54 | 114 | 0.042 | 0.002 |
| 28 | 124 | 3.075 | 0.054 | 54 | 132 | 2.414 | 0.032 |
| 29 | 201 | 0.228 | 0.003 | 56 | 103 | 0.043 | 0.004 |
| 29 | 212 | 0.228 | 0.003 | 56 | 111 | 0.043 | 0.004 |
| 29 | 230 | 3.072 | 0.048 | 56 | 132 | 2.422 | 0.001 |
| 30 | 101 | 0.646 | 0.013 | 57 | 103 | 0.032 | 0.007 |
| 30 | 133 | 2.976 | 0.013 | 58 | 211 | 0.032 | 0.002 |
| 31 | 203 | 0.682 | 0.008 | 58 | 232 | 2.323 | 0.020 |
| 31 | 203 | 0.002 | 0.084 | 61 | 103 | 0.038 | 0.020 |
| 33 | 103 | 0.413 | 0.003 | 61 | 113 | 0.038 | 0.003 |
| 33 | 131 | 2.343 | 0.003 | 61 | 123 | 1.680 | 0.002 |
| | | | | | | 2.128 | |
| 34 | 101 | 0.286 | 0.001 | 61 | 131 | | 0.030 |
| 34 | 103 | 0.306 | 0.033 | 62 63 | 203 | 0.034 | 0.004 |
| 34 | 107 | 0.104 | 0.004 0.008 | 63 63 | 103 122 | 0.028 | 0.000 |
| 35 | 101 | 0.265 | | | | 2.119 | 0.011 |
| 35 35 | 103 | 0.245 | 0.001 | 65 65 | 101 | 0.049 | |
| | 133 | 3.094 | 0.002 | 65 | 110 | 0.050 | 0.002 |
| 39 | 101 | 0.061 | 0.001 | 65 | 114 | 1.009 | 0.016 |
| 39 | 121 | 3.011 | 0.075 | 65 | 122 | 2.133 | 0.012 |
| 39 | 124 | 3.165 | 0.026 | 66 | 101 | 0.046 | 0.008 |
| 40 | 101 | 0.064 | 0.004 | 66 | 133 | 2.050 | 0.001 |
| 40 | 133 | 3.191 | 0.001 | 67 | 202 | 0.040 | 0.000 |
| 41 | 103 | 0.039 | 0.003 | 67 | 233 | 1.864 | 0.013 |
| 41 | 133 | 3.186 | 0.005 | 68 | 102 | 0.037 | 0.002 |
| 42 | 101 | 0.053 | 0.002 | 69 | 201 | 0.041 | 0.001 |
| 42 | 133 | 3.133 | 0.007 | 69 | 231 | 2.000 | 0.005 |
| 43 | 111 | 0.090 | 0.004 | 70 | 101 | 0.039 | 0.003 |
| 43 | 120 | 2.826 | 0.011 | 70 | 107 | 0.014 | 0.001 |
| 45 | 101 | 0.033 | 0.002 | 71 | 104 | 0.032 | 0.001 |
| 45 | 110 | 0.088 | 0.008 | 72 | 101 | 0.045 | 0.000 |
| 45 | 115 | 0.472 | 0.002 | 73 | 103 | 0.043 | 0.002 |

| STATION NUMBER | SAMP NO. | F12 pM/kg | F12 Stdev | STATION NUMBER | SAMP NO. | F12 pM/kg | F12 Stdev |
|-------------------|-------------|----------------|----------------|-------------------|-------------|--------------|--------------|
| 73 | 115 | 0.144 | 0.000 | 116 | 223 | 0.306 | 0.000 |
| 73 | 133 | 1.841 | 0.009 | 116 | 234 | 1.094 | 0.017 |
| 74 | 202 | 0.056 | 0.007 | 117 | 101 | 0.009 | 0.003 |
| 75 | 128 | 1.863 | 0.011 | 117 | 107 | 0.004 | 0.001 |
| 76 | 201 | 0.053 | 0.004 | 118 | 103 | 0.007 | 0.000 |
| 76 | 203 | 0.059 | 0.004 | 118 | 128 | 1.166 | 0.003 |
| 77 | 102 | 0.058 | 0.002 | 119 | 103 | 0.007 | 0.000 |
| 77 | 133 | 1.695 | 0.012 | 120 | 201 | 0.008 | 0.000 |
| 78 | 101 | 0.076 | 0.007 | 120 | 205 | 0.007 | 0.000 |
| 79 | 132 | 1.610 | 0.013 | 120 | 227 | 0.988 | 0.002 |
| 81 | 109 | 0.474 | 0.008 | 120 | 234 | 1.227 | 0.003 |
| 83 | 101 | 0.235 | 0.007 | 121 | 201 | 0.007 | 0.001 |
| 83 | 105 | 1.014 | 0.014 | 122 | 102 | 0.007 | 0.001 |
| 86 | 101 | 0.153 | 0.005 | 122 | 105 | 0.004 | 0.000 |
| 88 | 113 | 0.959 | 0.018 | 122 | 132 | 1.295 | 0.003 |
| 88 | 125 | 1.701 | 0.001 | 123 | 101 | 0.005 | 0.000 |
| 89 | 232 | 1.394 | 0.025 | 124 | 101 | 0.006 | 0.001 |
| 90 | 103 | 0.004 | 0.003 | 124 | 130 | 1.213 | 0.009 |
| 93 | 102 | 0.035 | 0.001 | 124 | 135 | 1.000 | 0.005 |
| 94 | 102 | 0.031 | 0.004 | 125 | 303 | 0.004 | 0.000 |
| 94 | 130 | 1.535 | 0.001 | 125 | 334 | 1.081 | 0.004 |
| 95 | 101 | 0.034 | 0.001 | 126 | 101 | 0.004 | 0.001 |
| 96 | 102 | 0.034 | 0.000 | 126 | 132 | 1.174 | 0.000 |
| 96 | 119 | 0.020 | 0.003 | 127 | 201 | 0.007 | 0.000 |
| 96 | 135 | 1.402 | 0.003 | 127 | 210 | 0.007 | 0.000 |
| 97 | 201 | 0.037 | 0.008 | 127 | 226 | 0.755 | 0.001 |
| 98 | 102 | 0.037 | 0.004 | 127 | 235 | 1.029 | 0.002 |
| 98 | 134 | 1.365 | 0.000 | 128 | 201 | 0.007 | 0.004 |
| 100 | 101 | 0.041 | 0.011 | 129 | 102 | 0.007 | 0.000 |
| 100 | 118 | 0.041 | 0.005 | 129 | 135 | 0.003 | 0.006 |
| 100 | 135 | 1.310 | 0.003 | 130 | 101 | 0.005 | 0.000 |
| 101 | 227 | 1.374 | 0.003 | 130 | 107 | 0.003 | 0.000 |
| 101 | 102 | 0.018 | 0.023 | 130 | 125 | 0.600 | 0.001 |
| 102 | 102 | 0.565 | 0.002 | 131 | 134 | 1.077 | 0.004 |
| | 101 | | 0.003 | 132 | 102 | 0.006 | 0.000 |
| 104 | | 0.017 1.615 | | | 119 | 0.008 | 0.001 |
| 104 | 132 | | 0.018 | 132 | | | |
| 105 | 201 | 0.014 | 0.001 0.000 | 133 | 101 | 0.006 | 0.000 |
| 105 | 203 | 0.006 | | 134 | 201 | 0.007 | 0.001 |
| 105 | 205 | 0.003 | 0.000 | 134 | 235 | 0.935 | 0.018 |
| 106 | 102 | 0.018 | 0.003 | 135 | 201 | 0.008 | 0.000 |
| 106 | 134 | 1.288 | 0.015 | 135 | 215 | 0.001 | 0.001 |
| 108 | 101 | 0.012 | 0.001 | 135 | 234 | 1.073 | 0.004 |
| 108 | 134 | 1.382 | 0.000 | 136 | 103 | 0.005 | 0.000 |
| 109 | 101 | 0.013 | 0.003 | 137 | 101 | 0.006 | 0.001 |
| 110 | 202 | 0.011 | 0.000 | 137 | 121 | 0.002 | 0.000 |
| 110 | 234 | 1.267 | 0.024 | 137 | 133 | 1.059 | 0.005 |
| 112 | 102 | 0.012 | 0.001 | 140 | 102 | 0.004 | 0.000 |
| 112 | 132 | 1.398 | 0.006 | 140 | 133 | 1.056 | 0.003 |
| 113 | 101 | 0.010 | 0.001 | 141 | 101 | 0.006 | 0.000 |
| 114 | 104 | 0.009 | 0.000 | 142 | 102 | 0.006 | 0.001 |
| 114 | 135 | 1.135 | 0.012 | 142 | 123 | 0.045 | 0.007 |
| 115 | 101 | 0.009 | 0.001 | 142 | 135 | 0.946 | 0.012 |
| 116 | 201 | 0.010 | 0.000 | 143 | 101 | 0.005 | 0.001 |
| 116 | 204 | 0.009 | 0.001 | 144 | 102 | 0.003 | 0.000 |

| STATION NUMBER | | F12 pM/kg | | STATION NUMBER | NO. | F12 pM/kg | |
|-------------------|-----|--------------|-------|-------------------|-----|--------------|-------|
| 144 | 129 | 1.056 | 0.009 | 160 | 103 | 0.002 | 0.001 |
| 145 | 103 | 0.002 | 0.001 | 161 | 103 | 0.000 | 0.001 |
| 146 | 102 | 0.003 | 0.001 | 161 | 131 | 0.935 | 0.008 |
| 146 | 125 | 0.192 | 0.003 | 162 | 201 | 0.003 | 0.000 |
| 146 | 131 | 1.012 | 0.006 | 163 | 201 | 0.002 | 0.001 |
| 147 | 101 | 0.003 | 0.000 | 163 | 229 | 0.848 | 0.001 |
| 148 | 121 | 0.369 | 0.007 | 164 | 104 | 0.000 | 0.001 |
| 150 | 234 | 0.914 | 0.004 | 167 | 201 | 0.002 | 0.000 |
| 151 | 102 | 0.001 | 0.002 | 167 | 230 | 1.042 | 0.006 |
| 151 | 135 | 0.888 | 0.006 | 169 | 201 | 0.002 | 0.001 |
| 152 | 101 | 0.005 | 0.002 | 169 | 226 | 0.029 | 0.002 |
| 153 | 102 | 0.003 | 0.000 | 169 | 235 | 0.937 | 0.004 |
| 153 | 132 | 0.946 | 0.003 | 170 | 101 | 0.009 | 0.000 |
| 154 | 101 | 0.001 | 0.002 | 170 | 129 | 0.551 | 0.002 |
| 154 | 103 | 0.001 | 0.000 | 171 | 101 | 0.000 | 0.001 |
| 155 | 102 | 0.002 | 0.001 | 171 | 128 | 0.180 | 0.002 |
| 155 | 122 | 0.004 | 0.001 | 172 | 221 | 0.089 | 0.001 |
| 155 | 134 | 0.892 | 0.013 | 172 | 233 | 0.949 | 0.006 |
| 156 | 102 | 0.003 | 0.001 | 173 | 201 | 0.000 | 0.000 |
| 157 | 104 | 0.001 | 0.000 | 173 | 225 | 0.020 | 0.002 |
| 158 | 102 | 0.003 | 0.001 | 173 | 231 | 0.879 | 0.007 |
| 159 | 102 | 0.002 | 0.000 | 174 | 101 | 0.000 | 0.000 |
| 159 | 103 | 0.002 | 0.001 | 178 | 101 | 0.003 | 0.000 |
| 159 | 134 | 0.910 | 0.038 | 179 | 101 | 0.002 | 0.000 |
| | | | | 180 | 101 | 0.004 | 0.002 |
| | | | | 181 | 101 | 0.004 | 0.000 |
| | | | | 182 | 101 | 0.004 | 0.001 |

APPENDIX 7 Carbon Measurement techniques on P14S an P15S

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Seawater samples were drawn from the PVC bottles with a 25-cm length of silicon tubing. One end of the tubing was fit over the petcock of the PVC bottle and the other end was attached over the opening of a 10-cm glass spectrophotometric cell. The spectrophotometric cell was rinsed three to four times with a total volume of approximately 200 mL of seawater; the Teflon(tm) endcaps were also rinsed and then used to trap a sample of seawater in the glass cell. While drawing the sample, care was taken to make sure that no air bubbles were trapped within the cell.

Seawater pH was measured using a three-wavelength spectrophotometric procedure (Byrne, 1987) and the indicator calibration of Clayton and Byrne (1993). The indicator was a 8.0-mM solution of Kodak(tm) m-cresol purple sodium salt (C21H17O5Na) in a 10% ethanol solution; the absorbance ratio of the concentrated indicator solution (RI = 578A/434A) was 1.00. All absorbance ratio measurements were obtained in the thermostatted (25.0 +/- 0.05C) cell compartments of HP 8453 diode array spectrophotometers. Periodically the spectrophotometric cells were cleaned with a 1 N HCl solution to preclude biological growth. Measurements of pH were taken at 25.0C on the total hydrogen ion concentration ([H+]t) scale, in mol/kg soln.

DISSOLVED INORGANIC CARBON (DIC)

The DIC analytical equipment was set up in a seagoing container modified for use as a laboratory. The analysis was done by coulometry; two analytical systems were used simultaneously on the cruise, each consisting of a coulometer (UIC, Inc.) coupled with a SOMMA (Single Operator Multiparameter Metabolic Analyzer) inlet system developed by Ken Johnson (Johnson et al., 1985,1987,1993; Johnson, 1992) of Brookhaven National Laboratory (BNL). Pipette volume was determined based on the procedures described in Handbook of Methods for CO2 Analysis (DOE, 1994).

In the coulometric analysis of DIC, all carbonate species are converted to CO2 (gas) by addition of excess hydrogen to the seawater sample, and the evolved CO2 gas is carried into the titration cell of the coulometer, where it reacts quantitatively with a proprietary reagent based on ethanolamine to generate hydrogen ions. These are subsequently titrated with coulometrically generated OH-. CO2 is thus measured by integrating the total charge required to achieve this. Samples were drawn from the PVC bottles into cleaned, precombusted 500-mL Pyrex(tm) bottles using Tygon(tm) tubing according to procedures outlined in the Handbook of Methods for CO2 Analysis (DOE, 1994). Bottles were rinsed once and filled from the bottom, overflowing half a volume, and care was taken not to entrain any bubbles. The tube was pinched off and withdrawn, creating a 5-mL headspace, and 0.2 mL of saturated HgCl2 solution was added as a preservative.

The sample bottles were sealed with glass stoppers lightly covered with Apiezon-L(tm) grease, and were stored at room temperature for a maximum of 12 hours prior to analysis.

The coulometers were calibrated by injecting aliquots of pure CO2 (99.995%) by means of an 8-port valve outfitted with two sample loops that had been calibrated at BNL (Wilke, 1993). All DIC values were corrected for dilution by 0.2 mL of HgCl2; total water volume was 540 mL. The correction factor used was 1.00037. The instruments were calibrated at the beginning, middle, and end of each coulometer cell solution with a set of the gas loop injections.

CRMs (Batch 29) were provided by Dr. Andrew Dickson (SIO), and was analyzed on both instruments over the duration of the cruise. The CRM certified value was 1902.54 +/-1.05 (n=14). The overall accuracy and precision for the CRMs on both instruments combined was -1.1 +/-0.9 (n=153). Replicate measurements from different PVC bottles tripped at the same depth, along with replicate measurements from the same PVC bottle was within +/-1.9 mol/kg DIC. DIC data reported for this cruise have been corrected to the Batch 29 CRM value by adding the difference between the certified value and the mean shipboard CRM value (certified value - shipboard analyses) on a per instrument/per leg basis.

TOTAL ALKALINITY (TA)

The titration system used to determine TA consisted of a Metrohm 665 Dosimat(tm) titrator and an Orion(tm) 720A pH meter controlled by a personal computer (Millero et al., 1993). The acid titrant, in a water-jacketed burette, and the seawater sample, in a water-jacketed cell, were kept at 25 +/- 0.1C with a Neslab(tm) constant-temperature bath. The plexiglass water-jacketed cells were similar to those used by Bradshaw et al. (1988), except that a larger volume (200 mL) was used to increase the precision. The cells had fill and drain valves with zero dead-volume to increase the reproducibility of the cell volume.

The HCl solutions used throughout the cruise were made, standardized, and stored in 500-mL glass bottles in the laboratory for use at sea. The 0.2487 M HCl solutions were made from 1 M Mallinckrodt(tm) standard solutions in 0.45 M NaCl to yield an ionic strength equivalent to that of average seawater (0.7 M). The acid was independently standardized using a coulometric technique (Taylor and Smith, 1959; Marinenko and Taylor, 1968) by the University of Miami and by Dr. Dickson. The two standardization techniques agreed to +/-0.0001 N.

The volume of HCl delivered to the cell is traditionally assumed to have a small uncertainty (Dickson, 1981) and is equated with the digital output of the titrator. Calibrations of the Dosimat(tm) burettes with Milli Q(tm) water at 25C indicated that the systems deliver 3.000 mL (the value for a titration of seawater) to a precision of 0.0004 mL. This uncertainty resulted in an error of 0.4 mol/kg in TA.

Internal consistency of each cell was checked before, during, and after the cruise by titrating CRM Batches 29 and 30 prepared by Dr. Dickson. The TA of CRM was determined by open cell (weighed) titration in the laboratory prior to the cruise and was found to be 2184.8 +/- 1.3 mol/kg (n= 15) and 2201.9 +/- 1.0 mol/kg (n = 21), respectively. A total of 85 CRM measurements made at sea yielded 2173.8 +/- 1.6 mol/kg for Batch 29 and 2190.8 +/- 1.7 mol/kg for Batch 30 on three different cells. This offset was due to

| changes in the values for each | volume cell and | of the cells. each leg. | All | TA | data | have | been | corrected | to | laboratory | CRM |
|--------------------------------|--------------------|----------------------------|-----|----|------|------|------|-----------|----|------------|-----|
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APPENDIX 8. Listing of CGC96 Bottle problems, with QC evaluations

* indicates no nutrient sample.

initial

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|----|--------|------|-------|--------|----------------------------|--|------------|--|--|--|
| St | n Samp | Cast | Fbtl | | Problem as annotated; | | fbtlnbr | | | |
| Nb | r no | no | nbr | Ctdprs | on deck logs | Comments | re-set to: | | | |
| | | | | | | | | | | |
| 1 | 106 | 1 | 3 | 3001.9 | Leaking, * | ctd-sal < .001,no 02,cfc,sil | 2 | | | |
| 2 | 110 | 1 | 3 | 3997.2 | Leaking, * | ctd-sal = 0,no 02,cfc,sil | 2 | | | |
| 2 | 121 | 1 | 3 | 1600.5 | Leaking, * | ctd-sal < .0014,no 02,sil, cfc=good | 2 | | | |
| 2 | 129 | 1 | 3 | 2235.5 | Leaking, * | no sal,02,cfc,sil | 3 | | | |
| 2 | 133 | 1 | 3 | 2236.5 | Leaking, * | no sal,02,sil cfc=OK | 3 | | | |
| 3 | 129 | 1 | 3 | 37.5 | Leaking, * | NO BOTTLE DATA FO STA=3 | 3 | | | |
| 4 | 104 | 1 | 3 | 117.7 | Leaking, high nutrients | ctd-sal < .001, O2=OK,cfc=OK,sil=high | 3 | | | |
| 4 | 109 | 1 | 3 | 9.3 | Leaking | ctd-sal =0085,02=0K, cfc=0K | 2 | | | |
| 5 | 107 | 1 | 3 | 465.9 | Stopcock pushed in | ctd-sal < 0.001,no 02,cfc | 3 | | | |
| 5 | 113 | 1 | 3 | 207.4 | Leaking | ctd-sal =0011,others=OK | 2 | | | |
| 5 | 114 | 1 | 3 | 180.8 | Top endcap cracked | ctd-sal=0.001,sil=OK,no cfc,O2 | 3 | | | |
| 6 | 103 | 1 | 4 | 1070.5 | Did not trip properly, * | no samples | 4 | | | |
| 6 | 110 | 1 | 3 | 490.8 | Leaking | ctd-sal=-0.0004,sil=OK, no others | 2 | | | |
| 7 | 108 | 1 | 3 | 724.9 | Leaking | ctd-sal=.0003,02,sil=OK,no cfc | 2 | | | |
| 7 | 120 | 1 | 3 | 154.8 | Leaking | ctd-sal=.0003,02,sil=OK, no cfc | 2 | | | |
| 8 | 108 | 1 | 3 | 1213.6 | Huge Leak at top cap, * | ctd-sal=.0007,no 02,cfc,sil | 3 | | | |
| 8 | 132 | 1 | 3 | 11.1 | Stopcock open, 131/132 | nut reps look OK ctd-sal=0.0001,o2=OK,no | cfc 3 | | | |
| 11 | 103 | 1 | 3 | 5120 | Stopcock pushed in,102/103 | nut reps=ok ctd-sal=0006,02,nuts=OK,no | cfc 2 | | | |
| 11 | 117 | 1 | 3 | 1317.8 | Leaking, * | no sal, nuts, cfc; O2=high BAD | 3 | | | |
| 12 | 203 | 2 | 4 | 4900.2 | no comment | ctd-sal=0.5, nuts-very low, o2=very high | fbtlnbr 4 | | | |
| 12 | 206 | 2 | 3 | 3699.8 | Leaking | ctd-sal=0.0009,o2,sil=OK | 2 | | | |
| 12 | 209 | 2 | 3 | 2504.4 | Leaking | ctd-sal=.0017,o2,sil=OK | 2 | | | |
| 13 | 106 | 1 | 3 | 3498.8 | Leaking | ctd-sal=0.0010,no o2,cfc,sil=OK | 2 | | | |
| 13 | 109 | 1 | 3 | 2293.5 | Leaking | ctd-sal=0.0017,no 02,cfc;sil=0K | 2 | | | |
| 14 | 117 | 1 | 3 | 1214 | Leaking, * | no sal,cfc,sil;02 a little high? | 3 | | | |
| 15 | 208 | 2 | 3 | 3561.8 | Leaking | ctd-sal=0.0013;no cfc;o2,sil=OK | 2 | | | |
| 15 | 213 | 2 | 3 | 2316.3 | Band broken on btm | ctd-sal=0.001;o2,cfc,sil=OK | 2 | | | |
| 15 | 217 | 2 | 3 | 1310 | Leaking, * | no sal,cfc,nuts; o2=high | 3 | | | |
| 15 | 225 | 2 | 3 | 427.1 | Stopcock pushed in | ctd-sal=-0.0009;no cfc,sil;o2-ctd=low | 3 | | | |
| 15 | 233 | 2 | 4 | 31.2 | Did not trip, * | | 4 | | | |
| 16 | 109 | 1 | 3 | 3188.9 | Leaking | ctd-sal=0.0010;o2,sil=OK,no cfc | 2 | | | |
| 16 | 117 | 1 | 3 | 1224.3 | Leaking | ctd-sal=0.0015;o2,sil=OK,no cfc | 2 | | | |
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|--------|------------|--------|--------|---------------|--|---|------------|
| Stn | Samp | | | | Problem as annotated; | | fbtlnbr |
| Nbr | no | no | nbr | Ctdprs | on deck logs | Comments | re-set to: |
| 17 | 120 | 1 | 3 | 926 4 | Leaking | ctd-sal=0.00008;o2,cfc,sil=OK | 2 |
| | 131 | 1 | 3 | | Leaking | ctd-sal=0.0012;02,sil=0K;no cfc | 2 |
| | 103 | 1 | 3 | | Leaking | ctd-sal=0.0012;02,sil,cfc=0K;ph? | 3 |
| | 133 | 1 | 4 | | Did not close, * | cca-sar-0.0013/02,srr,crc-ok/pii? | 4 |
| | 106 | 1 | 3 | | Leaking | ctd-sal=-0.0012;f12 a little high,no pH | 2 |
| | 110 | 1 | 3 | 1504.9 | _ | ctd-sal=0.0029; | 2 |
| | 117 | 1 | 3 | 420.1 | 5 | Ctu-sal=0.0029; | 3 |
| | 105 | | | 2889.9 | | | 4 |
| | 105 | 1 | 4 | | | ctd-sal <0.001;sil=OK | 3 |
| | | 1 | 3 | 2502.3 | - | Ctd-sal <0.001/S11=OK | 3 |
| | 109 114 | 1 1 | 3 | 1355.7 577 | Damaged bottle Stopcock pushed in | | 3 |
| | 103 | | 3 | 4702.5 | | | 4 |
| | 106 | 1 1 | 4 3 | 3502 | Did not trip properly, * Leaking, PO4 high, sil & NO3 ok | atd asl-0 0000:afa ail-0% | 2 |
| | | 1 | | | | ctd-sal=0.0009;cfc,sil=OK | |
| | 122 205 | 2 | 4 | 67.2 | | no gol où gfg gil | 4 |
| | 205 | | 4 | 3300.8 | Did not trip properly, * | no sal,o2,cfc,sil | 4 3 |
| | | 2 | 3 | 2899.0 | Did not trip properly, * | ctd-sal=0.0049;no cfc;o2,sil=OK | |
| | 109 115 | 1 1 | 3 3 | 603 | Vent open | ctd-sal=0.0010;o2,cfc,sil=OK | 2 4 |
| | | | | | Bottom open, * | -t-d1 (10 001)f0 -ilh OV | |
| | 104 | 1 | 3 | | Stopcock pushed in | ctd-sal<<0.001;cfc,o2,sil,ph=OK | 2 |
| | 105 | 1 | 4 | | Did not trip properly, * | | 4 |
| | 111 | 1 | 4 | | Did not close-lanyard hung up, * | | 4 |
| | 117 | 1 | 3 | 191.3 | - | ctd-sal=-0.001;o2,sil=0K;no cfc | 2 |
| | 209 | 2 | 3 | | Leaking | ctd-sal=0.0011;no cfc,o2;sil=OK | 2 |
| | 220 | 2 | 3 | | Leaking | ctd-sal=0.0002;sil,o2=OK;no cfc | 2 |
| | 226 | 2 | 3 | | Leaking | ctd-sal=0.0025;sil,o2,cfc=OK | 2 |
| | 104 120 | 1 | 3 3 | 3185.7 | Leaking | ctd-sal=0.0003;sil,o2,cfc=OK | 2 2 |
| | | 1 | | 436.3 | Leaking | ctd-sal = 0.0006;no cfc;o2,sil=OK | |
| | 229 | 2 | 4 | -9 | Did not trip properly, * | | 4 |
| | 230 | 2 | 4 | -9 0 | Did not trip properly, * | | 4 |
| | 231 232 | 2 | 4 | -9 0 | Did not trip properly, * | | 4 |
| | | | 4 | -9 0 | Did not trip properly, * | | 4 |
| | 233 | 2 | 4 | -9 0 | Did not trip properly, * | | 4 |
| | 234 | 2 | 4 | -9 45 1 | Did not trip properly, * | | 4 |
| | 131 | 1 | 3 | 45.1 | 5 | | 3 |
| 33 | 113 | 1 | 3 | 1136.4 | Stopcock pushed in | ctd-sal=-0.0002;o2,cfc,sil,ph=OK | 2 |

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| Ctn | Stn Samp Cast Fbtl | | | Problem as annotated; | | | | |
|-----|--------------------|---|---|-----------------------|--------------------------------------|--|----|--|
| | no | | | Ctdprs | on deck logs | Comments fbtlnl re-se | | |
| 34 | 110 | 1 | 3 | 1439.2 | Leaking | ctd-sal=0.0004;o2,sil=0K;no cfc,ph | 2 | |
| 35 | 131 | 1 | 3 | 59.1 | Leaking | ctd-sal=0.0176;no cfc,o2;sil=OK | 3 | |
| 36 | 101 | 1 | 3 | 2901 | Stopcock pushed in | no sal,cfc;o2,sil,ph=OK | 3 | |
| 36 | 102 | 1 | 3 | 2752.2 | Stopcock pushed in | no sal,cfc;o2,sil,ph=OK | 3 | |
| 37 | 107 | 1 | 3 | 1030.9 | Top may be been cracked by tag lines | ctd-sal=0.0002;o2,sil,cfc,ph=OK | 2 | |
| 37 | 108 | 1 | 3 | 921 | Top may be been cracked by tag lines | ctd-sal=0.0002;o2,sil,cfc,ph=OK | 2 | |
| 37 | 109 | 1 | 3 | 820 | Top may be been cracked by tag lines | ctd-sal=0.0067 | 3 | |
| 38 | 103 | 1 | 3 | 2099.4 | Stopcock pushed in | ctd-sal=-0.0012;o2,sil,ph=OK;no cfc; | 2 | |
| 38 | 122 | 1 | 3 | 41.4 | Leaking | ctd-sal=-0.0051;sil=OK;no cfc,ph,o2 | 2 | |
| 39 | 104 | 1 | 3 | 1897.4 | Stopcock pushed in | ctd-sal=-0.0005;o2,sil,ph=OK;no cfc | 2 | |
| 39 | 109 | 1 | 3 | 919.5 | Stopcock pushed in | no sal,cfc;sil,ph,o2=OK | 3 | |
| 40 | 131 | 1 | 3 | 43.3 | | ctd-sal=-0.0025;o2,ph,sil=OK;no cfc | 2 | |
| 40 | 134 | 1 | 3 | 10.7 | bottom leaking | ctd-sal=-0.0034;sil=OK;no cfc,o2,ph | 2 | |
| 41 | 130 | 1 | 3 | 8.3 | Leaking | ctd-sal=-0.0036;sal,o2,sil,ph=OK;no cfc | 2 | |
| 42 | 110 | 1 | 3 | 1693.4 | Stopcock pushed in | ctd-sal=-0.0009;o2,sil=OK;no cfc,ph | 2 | |
| 42 | 131 | 1 | 3 | 45.1 | Stopcock pushed in | ctd-sal = -0.0011;o2,sil=OK;no cfc,ph | 2 | |
| 43 | 103 | 1 | 3 | 2706.8 | no comment | sal,o2,cfc,nuts flagged | 3 | |
| 45 | 120 | 1 | 3 | 166.3 | Stopcock pushed in | ctd-sal=-0.0013;sil=OK;no cfc,ph,o2 | 3 | |
| 46 | 126 | 1 | 3 | 193.2 | Leaking | ctd-sal=-0.0010;o2,cfc,sil,ph=OK | 2 | |
| 46 | 131 | 1 | 3 | 67 | Leaking | ctd-sal=0.0042;sil=OK;no cfc,ph | 3 | |
| 47 | 201 | 2 | 3 | 4100.7 | Leaking | cts-sal=0.0011;o2-ctd high,sil=OK | 3 | |
| 47 | 231 | 2 | 3 | 82.1 | Leaking | ctd-sal=-0.0006;o2,sil=OK | 2 | |
| 48 | 106 | | | | | fo2=4 4% lower than surrounding points | | |
| 49 | 120 | 1 | 3 | 927 | Stopcock pushed in | ctd-sal=0.0011;02,cfc,sal=0K,no ph | 2 | |
| 50 | 101 | 1 | 3 | 4489.5 | Leaking | ctd-sal=0.0008;o2,ph,sil=OK;no cfc | 2 | |
| 50 | 102 | | | | | fo2=3:1.5% higher than rep and surrounding point | ts | |
| 50 | 111 | 1 | 3 | 2440 | Leaking | ctd-sal=0.0013;02,cfc,sil,ph=OK | 2 | |
| 50 | 114 | 1 | 3 | 1661.4 | Leaking | ctd-sal=0.0004;o2,sil,ph=OK;no cfc | 2 | |
| 51 | 104 | 1 | 3 | 4566.8 | Leaking | ctd-sal=0.0012;o2,sil,ph=OK;no cfc | 2 | |
| 52 | 112 | 1 | 3 | 2437.5 | Vent valve left open | ctd-sal=0.0021; | 3 | |
| 53 | 101 | 1 | 3 | 5144.9 | Stopcock pushed in | ctd-sal=0.0007;02,ph,sil=OK;no cfc | 2 | |
| 53 | 133 | 1 | 3 | 29.7 | Did not trip properly, * | | 3 | |
| 55 | 133 | 1 | 4 | 31.3 | "Bottom open, lanyard hung up",* | | 4 | |
| 56 | 116 | 1 | 3 | 1440.2 | Leaking, * | | 3 | |
| 56 | 117 | 1 | 3 | 1216.5 | Leaking, * | | 3 | |

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| | Samp | | | | Problem as annotated; | | fbtlnbr | | |
| Nbr | no | no | nbr | Ctdprs | on deck logs | Comments | re-set to: | | |
| 57 | 104 | 1 | 3 | 4565.9 | Leaking | | 3 | | |
| 57 | 116 | 1 | 3 | 1562.5 | Leaking | | 3 | | |
| 57 | 133 | 1 | 4 | 28.4 | Did not trip properly, * | | 4 | | |
| 59 | 103 | 1 | 3 | 4814.1 | Leaking | | 3 | | |
| 60 | 128 | 1 | 3 | 189.2 | Leaking | | 3 | | |
| 60 | 133 | 1 | 4 | 19.1 | <pre>"Empty, lanyard hung up", *</pre> | | 4 | | |
| 61 | 127 | 1 | 3 | 261.3 | Leaking | ctd-sal=0.0008;o2,sil=OK;no cfc,ph | 2 | | |
| 62 | 201 | 2 | 3 | 5171 | Leaking | ctd-sal=-0.0005;o2,sil=OK,no cfc,ph | 2 | | |
| 62 | 204 | 2 | 4 | 4439.4 | Stopcock pushed in | ctd-sal=0.0003;o2,sil=OK,no cfc,ph | 2 | | |
| 63 | 105 | 1 | 3 | 3495.9 | no comment | ctd-sal=0.0083;o2,cfc=high hp-high? | 3 | | |
| 64 | 116 | 1 | 4 | 478.4 | Did not trip properly, low nuts | | 4 | | |
| 64 | 117 | 1 | 4 | 365.8 | <pre>"Empty, lanyard hung up", *</pre> | | 4 | | |
| 66 | 116 | 1 | 3 | 1436.3 | Stopcock pushed in | | 3 | | |
| 66 | 126 | 1 | 3 | 291.2 | Leaking | | 3 | | |
| 67 | 219 | 2 | 3 | 1027.4 | no comment | ctd-sal=0.0056; | 3 | | |
| 67 | 226 | 2 | 3 | 319.9 | Leaking | ctd-sal=-0.0003;o2-ctd=4;ph,sil=OK | 2 | | |
| 67 | 231 | 2 | 3 | 79 | Leaking | ctd-sal=-0.011;o2,sil,ph,cfc=OK | 2 | | |
| 68 | 101 | 1 | 3 | 5334.9 | Leaking | ctd-sal=0.0003;sil,ph=OK;no cfc,o2=high | 3 | | |
| 69 | 227 | 2 | 3 | 265.5 | "Large leak, top" | | 4 | | |
| 70 | 116 | 1 | 3 | 1441.3 | Minor btm leak | sal,o2,ph,sil=OK | 2 | | |
| 71 | 131 | 1 | 3 | 79.2 | | sal,o2,ph,sil=OK | 2 | | |
| 71 | 134 | 1 | 4 | 9.7 | lanyard hangup | | 4 | | |
| 72 | 131 | 1 | 3 | 69.6 | | ctd-sal=-0.006 | 3 | | |
| 73 | 131 | 1 | 3 | 80.1 | | sal,o2,cfc,ph,sil=OK | 2 | | |
| 73 | 134 | 1 | 3 | 10.1 | leak bottom cap | no sal,o2,cfc,sil,ph | 3 | | |
| 74 | 201 | 2 | 3 | 5385.3 | Leaking, NO3 & sil low, | PO4 n/a=bad sal | 4 | | |
| 77 | 101 | 1 | 3 | 5056.0 | | fo2=3;02 >2% high | | | |
| 77 | 107 | 1 | 3 | 3565.6 | | fo2=3; O2 high | | | |
| 79 | 133 | 1 | 3 | 13.4 | Leaking | | 3 | | |
| 80 | 212 | 2 | 3 | 1075.3 | Leaking | | 2 | | |
| 80 | 228 | 2 | 4 | 119.4 | Leaking, high nutrients BAD sal | | 4 | | |
| 80 | 229 | 2 | 4 | 93.6 | Did not trip-no sample | | 4 | | |
| 80 | 230 | 2 | 4 | 69.1 | | | 4 | | |
| 80 | 231 | 2 | 4 | -9 | Did not trip-no sample | | 4 | | |
| 80 | 232 | 2 | 4 | -9 | Did not trip-no sample | | 4 | | |

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| Stn | Stn Samp Cast Fbtl | | | | Problem as annotated; | | fbtlnbr |
|-----|--------------------|---|---|--------|------------------------------------|---------------------------------|-------------|
| | no | | | Ctdprs | on deck logs | Comments | re-set to: |
| | | | | | | | |
| 80 | 233 | 2 | 4 | -9 | Did not trip-no sample | | 4 |
| 80 | 234 | 2 | 4 | -9 | Did not trip-no sample | | 4 |
| 81 | 104 | 1 | 3 | 2555.9 | Leaking | sal,o2,ph,sil=OK no cfc | 2 |
| 81 | 133 | 1 | 3 | 9.6 | Leaking, * | no samp | 3 |
| 83 | 103 | 1 | 3 | 725.5 | Small leak | sal,o2,sil,ph=OK;no cfc | 2 |
| 83 | 104 | 1 | 3 | 624.9 | Small leak | sal,o2,sil=OK;no cfc,ph | 2 |
| 83 | 116 | 1 | 3 | 130.9 | Leaking | sal,o2,sil,ph=OK;no cfc | 2 |
| 85 | 104 | 1 | 3 | 565.8 | "Small leak, bottom cap" | sal,o2,sil,ph-OK;no cfc | 2 2 2 |
| 85 | 121 | 1 | 3 | 10 | "Small leak, bottom cap" | sal,o2,sil,phcfc=OK | |
| 87 | 103 | 1 | 3 | 1314.2 | "Small leak, bottom cap" | sal,o2,ph,sil,cfc=OK | 2 |
| 89 | 222 | 2 | 3 | 230.6 | "Small leak, bottom cap" | sal,sil,ph=OK;o2 low,no cfc | 2 |
| 90 | 116 | 1 | 3 | 590.8 | Leaking | sal,o2,sil,ph=OK;no cfc | 2 |
| 91 | 116 | 1 | 3 | 623.8 | Small leak, bottom cap | sal:OK;o2sil,ph,cfc=OK | 2 |
| 91 | 133 | 1 | 3 | 9.2 | Leaking, * | | 3 |
| 92 | 222 | 2 | 3 | 474.9 | Small leak, bottom cap | sal,o2,sil=OK;no cfc.ph | 2 |
| 92 | 226 | 2 | 3 | 240.5 | Small leak, bottom cap | | 2 |
| 92 | 233 | 2 | 3 | 20.5 | Large leak, bottom cap | sal,o2=OK | 2 |
| 93 | 133 | 1 | 3 | 30.1 | Leaking | sal,o2,sil,cfc=OK;no ph | 2 |
| 94 | 101 | 1 | 3 | 4655.3 | Stopcock pushed in | sal,o2,sil=OK | 2 |
| 94 | 119 | 1 | 4 | 874.6 | | sal=high,o2,cfc,ph=low,sil=high | 4 |
| 94 | 121 | 1 | 3 | 676.8 | Leaking | sal,o2,cfc,sil,ph=OK | 2 |
| 95 | 136 | 1 | 3 | 2.4 | Leaking, * | sal OK, no other sample data | 3 |
| 97 | 224 | 2 | 3 | 525.8 | Leaking | sal,o2,sil,ph=OK;no cfc | 2 |
| 97 | 233 | 2 | 3 | 79.3 | Leaking | sal,o2,ph,sil=OK; no cfc | 2 |
| 99 | 116 | 1 | 3 | 1350.2 | Small leak, bottom cap | sal,o2,sil.ph=OK;no cfc | 2 |
| 99 | 133 | 1 | 3 | 79.6 | Small leak, bottom cap | sal,o2,sil.ph=OK;no cfc | 2 |
| 100 | 129 | 1 | 4 | 190.3 | Did not trip, lanyard hung up", * | | 4 |
| 100 | 130 | 1 | 4 | 145.7 | Did not trip, lanyard hung up", * | | 4 |
| 100 | 131 | 1 | 4 | -9 | "Did not trip, lanyard hung up", * | | 4 |
| 100 | 132 | 1 | 4 | -9 | "Did not trip, lanyard hung up", * | | 4 |
| 103 | 107 | 1 | 4 | 3564.9 | Vent left open | sal=OK,sil=BAD | 4 |
| 105 | 233 | 2 | 4 | 56.4 | "Did not trip, lanyard hung up", * | | 4 |
| 106 | 124 | 1 | 3 | 478 | Possible leak | sal,cfc,sil,ph=OK;no o2 | 2 |
| | 133 | 1 | 4 | 69.9 | Did not trip properly, * | _ | 4 |

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| Stn | Samp | | Fh+1 | | Problem as annotated; | | fbtlnbr |
|-----|------|---|------|--------|--------------------------|---|-------------|
| | no | | | Ctdprs | on deck logs | Comments | re-set to: |
| 107 | 129 | 1 | 3 | 190.4 | Leaking | sal=ok;sil,ph,o2=OK;no cfc | 2 |
| 107 | 130 | 1 | 3 | 143.9 | Leaking | sal=ok;sil,ph,o2=OK;no cfc | 2 |
| 107 | 133 | 1 | 4 | 69.9 | Lanyard hung up | | 4 |
| 107 | 136 | 1 | 4 | 4.7 | leaking badly | | 4 |
| 109 | 103 | 1 | 2 | | | fo2=3; 4%higher than surrounding points | |
| 109 | 111 | 1 | 3 | 3064.2 | Leaking | | 3 |
| 110 | 216 | 2 | 3 | 1939.3 | Leaking, * | no sal,o2,sil,ph;cfc=OK | 3 |
| 110 | 218 | 2 | 3 | 1440.5 | Spigot leaking | sal,o2,cfc,sil,ph=OK | 2 |
| 114 | 111 | 1 | 3 | 3191 | "Small leak, bottom cap | sal,o2.cfc.sil.ph+OK | 2 |
| 114 | 124 | 1 | 3 | 669 | Leaking | sal,o2.cfc.sil.ph+OK | 2 |
| 114 | 136 | 1 | 4 | 5.3 | Vent open | only sal, sil; OK | 2 |
| 115 | 126 | 1 | 3 | 524.1 | "Small leak, bottom cap | sal,o2,sil=OK | 2 |
| 116 | 210 | 2 | 3 | 3440.6 | no comment | sal,o2,=low | 3 |
| 117 | 116 | 1 | 3 | 1814.5 | Leaking | sal,o2,sil,ph=OK;no cfc | 2 |
| 118 | 131 | 1 | 3 | 120.4 | "Small leak, bottom cap | sal,o2,sil=OK | |
| 119 | 109 | 1 | 3 | 3561.9 | "Large leak, top cap" | sal,o2,ph,sil=OK;no cfc | 2 2 2 |
| 119 | 126 | 1 | 3 | 526.8 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 119 | 131 | 1 | 3 | 163.9 | "Large leak, bottom cap" | | 3 |
| 120 | 226 | 2 | 3 | 474.6 | "Small leak, bottom cap" | sal,o2,sil,cfc=OK | 2 |
| 120 | 231 | 2 | 3 | 140.1 | Slight leak | sal,o2,sil,cfc,ph=OK | 2 |
| 121 | 203 | 2 | 3 | 4565 | Vent left open | sal,o2,sil,ph=OK;no cfc | 2 |
| 121 | 209 | 2 | 3 | 3065.5 | Leaked before vent open | sal,o2,sil,ph=OK;no cfc | 2 |
| 121 | 218 | 2 | 3 | 1125.5 | Leaking | sal,o2,sil,ph=OK;no cfc | 2 |
| 123 | 133 | 1 | 3 | 80.5 | Slight leak | sal,o2,sil=OK;no cfc | 2 |
| 124 | 117 | | | | | fo2=3; high | |
| 124 | 124 | 1 | 3 | 677.8 | Leaking, * | no sal,cfc,sil,ph | 3 |
| 125 | 324 | 3 | 3 | 720.1 | Leaking | sil,ph=OK | 2 |
| 126 | 124 | 1 | 3 | 670.5 | "Small leak, bottom cap" | sal,cfc,sil=OK | 2 |
| 127 | 207 | 2 | 4 | 4316.1 | Stopcock pushed in | sal,o2,sil=OK | 2 |
| 127 | 209 | 2 | 3 | 3815.3 | Leaking | sal=BAD,no cfc,ph | 3 |
| 127 | 224 | 2 | 3 | 719.5 | Major leaker | | 3 |
| 129 | 104 | | | | | ph 10oks low ???? | |
| 129 | 111 | 1 | 3 | 3314.1 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 130 | 104 | | | | | phlooks low ???? | |
| 130 | 126 | 1 | 3 | 476.6 | Leaking | ctd-sal=-0.007;no cfc,ph | 3 |

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| Stn Samp Cast Fbtl | | | | Problem as annotated; | | fbtlnbr |
|--------------------|----|-----|--------|--------------------------|-------------------------------------|------------|
| Nbr no | no | nbr | Ctdprs | on deck logs | Comments | re-set to: |
| 131 104 | | | | | ph looks low ???? | |
| 131 136 | 1 | 3 | 3.6 | "Leaker, top cap", * | o2,ph=OK | 2 |
| 132 110 | 1 | 3 | 3437.4 | "Leaker, top cap" | sil,sal=OK | 2 |
| 132 112 | 1 | 3 | 2939.4 | "Small leak, top cap" | sil,sal=OK | 2 |
| 132 131 | 1 | 3 | 140.7 | Small leak | sal,o2,cfc,sil=OK | 2 |
| 133 104 | 1 | 3 | 5067.6 | Bottom leak | sal,o2,cfc,sil=OK | 2 |
| 133 107 | 1 | 3 | 4314.1 | Small bottom leak | sal,o2,cfc,sil=OK | 2 |
| 134 224 | 2 | 3 | 673.6 | Leaking | sal,o2,cfc,sil=OK | 2 |
| 135 209 | 2 | 3 | 3565.1 | Leaking | sal,o2,sil=OK | 2 |
| 136 109 | 1 | 3 | 3671.3 | "Leaker, top cap" | sal,o2,sil=OK | 2 |
| 136 130 | 1 | 3 | 190.4 | Small bottom leak | sal,o2,sil=OK | 2 |
| 137 124 | 1 | 3 | 726.1 | Major leak | sal,sil=OK;no cfc,o2,ph | 3 |
| 137 130 | 1 | 3 | 217.6 | "Large leak, bottom cap" | sal,sil=OK; no cfc,ph,o2 | 3 |
| 139 109 | 1 | 3 | 1814.7 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 140 109 | 1 | 3 | 3439.6 | "Small leak, bottom cap" | sal,o2,sil=OK;no cfc,ph | 2 2 |
| 140 135 | 1 | 3 | 18.5 | "Small leak, bottom cap" | sal,o2,sil=OK;no cfc,ph | 2 |
| 141 102 | 1 | 3 | 4814.8 | Small leak | sal,o2,sil=OK;no ph,cfc | 2 |
| 141 103 | 1 | 3 | 4566.3 | Small leak | sal,o2,cfc,sil=OK;no ph | 2 |
| 141 109 | 1 | 3 | 3065.8 | Small leakk | sal,o2,cfc,sil=OK;no ph | 2 |
| 141 131 | 1 | 3 | 129.3 | Leaking | sal,o2,sil=OK;no ph,cfc | 2 |
| 144 125 | 1 | 3 | 475.7 | Small leak | <pre>sal,cfc,sil=ok; no,ph.o2</pre> | 2 |
| 144 133 | 1 | 3 | 69.8 | Leaking | sal,sil=ok;o2=high?,no cfc,ph | 3 |
| 146 102 | 1 | 3 | 4940.2 | Leaking | sal,o2,cfc,sil,ph"OK | 2 |
| 147 133 | 1 | 3 | 79.2 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 147 135 | 1 | 3 | 28.4 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 152 126 | 1 | 4 | 375.1 | Did not trip properly, * | | 4 |
| 152 133 | 1 | 3 | 70.1 | "Small leak, bottom cap" | sal,o2,sil=OK;no cfc,ph | 2 |
| 152 136 | 1 | 3 | 4.3 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 153 133 | 1 | 3 | 78.6 | Leaking | sal,o2,sil=ok;no cfc,ph | 2 |
| 158 111 | 1 | 3 | 2441.2 | Stopcock pushed in | sal,o2,sil,ph=OK;no cfc | 2 |
| 160 102 | 1 | 4 | 5247.9 | Stopcock pushed in | sal,sil=OK;nocfc,o2,ph | 2 |
| 160 105 | 1 | 3 | 4866.2 | Stopcock pushed in | sal,o2,sil=OK; no cfc,ph | 2 |
| 160 106 | 1 | 3 | 4738.1 | Stopcock pushed in | sal,o2,sil=OK; no cfc,ph | 2 |
| 160 128 | 1 | 4 | 290.7 | Leaking | ctd-sal=-0.007,sil=OK;no cfc,ph,o2 | 4 |
| 160 136 | 1 | 4 | 5.1 | Vent left open | sal,sil=OK,no o2,cfc,ph | 2 |

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| Stn | Stn Samp Cast Fbtl | | | aı. | Problem as annotated; | | fbtlnbr |
|-----|--------------------|----|---|--------|-----------------------|-------------------------|------------|
| Nbr | no | no | | Ctdprs | on deck logs | Comments | re-set to: |
| 161 | 106 | 1 | 3 | 4288.5 | Stopcock pushed in | sal,o2,sil=OK;no cfc,ph | 2 |
| 163 | 206 | 2 | 3 | 4564.4 | Stopcock pushed in | sal,o2,sil=OK;no cfc,ph | 2 |
| 163 | 228 | 2 | 3 | 324.5 | Leaking from top | sal,o2,sil,ph=OK;no cfc | 2 |
| 163 | 232 | 2 | 3 | 117.1 | Leaking from top | sal,o2,sil,ph=OK;no cfc | 2 |
| 163 | 234 | 2 | 3 | 57.9 | Vent left open | sal,o2,sil,ph=OK;no cfc | 2 |
| 163 | 235 | 2 | 3 | 29.6 | Vent left open | sal,o2,sil,ph=OK;no cfc | 2 |
| 163 | 236 | 2 | 3 | 5.3 | Vent left open | sal,o2,sil,ph,cfc=OK | 2 |
| 164 | 102 | 1 | 3 | 5179.4 | Stopcock pushed in | sal,o2,sil=OK;no cfc,ph | 2 |
| 164 | 136 | 1 | 3 | 4 | Leaking | sal,sil=ok;no o2,cfc,ph | 3 |
| 165 | 102 | 1 | 3 | 5599.4 | Small bottom leak | sal,o2,sil=OK;no cfc,ph | 2 |
| 165 | 106 | 1 | 3 | 4564.3 | Stopcock pushed in | sal,o2,sil=OK;no cfc,ph | 2 |
| 165 | 129 | 1 | 3 | 265.1 | Stopcock pushed in | | 3 |
| 166 | 228 | 2 | 3 | 286.8 | Stopcock pushed in | sal,o2,sil,ph=OK;no cfc | 2 |
| 167 | 206 | 2 | 3 | 4566 | Stopcock pushed in | sal,o2,sil=OK no cfc,ph | 2 |
| 167 | 228 | 2 | 3 | 326.4 | Stopcock pushed in | sal,sil=OK;no o2,cfc,ph | 3 |
| 168 | 109 | 1 | 3 | 3686.8 | Small bottom leak | sal,o2,sil=OK;no cfc,ph | 2 |
| 168 | 131 | 1 | 3 | 140.1 | Small bottom leak | sal,o2,sil=OK;no cfc,ph | 2 |
| 171 | 112 | 1 | 3 | 2812.9 | Stopcock pushed in | sal,o2,sil=OK;no cfc,ph | 2 |
| 171 | 113 | 1 | 3 | 2562.7 | Stopcock pushed in | sal,o2,sil=OK;no cfc,ph | 2 |
| 171 | 117 | 1 | 3 | 1564 | Small bottom leak | sal,o2,sil,ph=OK;no cfc | 2 |
| 171 | 127 | 1 | 3 | 421.6 | Stopcock pushed in | sal,sil=OK;no o2,cfc,ph | 3 |
| 172 | 235 | 2 | 3 | 10 | Small bottom leak | sal,o2,sil=OK,no cfc,ph | 2 |
| 173 | 226 | 2 | 3 | 525.3 | Small bottom leak | sal,o2,cfc,sil=OK;no ph | 2 |
| 174 | 105 | 1 | 3 | 4689 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 174 | 117 | 1 | 3 | 1690.4 | Leaking | sal,o2,sil=OK;no cfc,ph | 2 |
| 174 | 127 | 1 | 3 | 374.2 | Stopcock pushed in | sal,sil=OK;no o2,cfc,ph | 3 |
| 174 | 135 | 1 | 3 | 20.4 | Small bottom leak | sal,o2,cfc,sil=OK;no ph | 2 |
| 175 | 205 | 2 | 3 | 4899.9 | Leaking from top | sal,o2,sil=OK;no cfc,ph | 2 |
| 178 | 110 | 1 | 3 | 4098.9 | Leaking stopcock | sal,o2,sil=OK;no cfc,ph | 2 |
| 181 | 110 | 1 | 3 | 3253 | Leaking, * | | 3 |

APPENDIX 9a: DQ Evaluation of WOCE P14S and P15S hydrographic data.

(Arnold Mantyla) 1998.NOV.18

The first leg, P14S, was along approximately 170E southward from Campbell Island to about 66S, providing an excellent section across the main flow of the Antarctic Circumpolar Current. Data from WOCE section S04 stations 769 to 783 could be tacked onto this section to complete the section to the Antarctic coast at Victoria Land. The cruise continued to 67S, 170W to start a long northward section, providing another crossing of the ACC; and then extending through the Samoan Passage on to the equator. There was considerable overlap with P15N. Crossings of P06, P21, p31 and S04 provided comparisons with other WOCE sections as well. The sampling density and data quality for this cruise was quite good on the stations where the 34 place rosette could be used. On the stations where the larger rosette could not be used because of rough weather, the 24 place rosette was still able to get a reasonable profile for the full water column.

The data originators have looked over the data quite thoroughly but they have flagged quite a bit more data as questionable than I would have. In the case of phosphate, many profile bumps of only .01, which is well within measurement uncertainty or even round off truncations, were flagged as uncertain. Unless there was some problem in the measurement, those values should have been accepted as ok.

In the case of salinity, most of the flagged values were in high gradient regions or near sharp extrema in the profiles. There are a number of reasons why the CTD and water samples may not agree perfectly, and yet neither may be "wrong". The two measurements are quite different snapshots of the water column. Ray Weiss's study on the flushing characteristics of oceanographic samplers (DSR) 18: 653-656) points out water samples are really "an integration of the water column through which the sampling bottle has been passed"; while the CTD is an instantaneous measure of the ocean that is in the wake of the rosette package. In high gradient regions either measurement can have problems. If the rosette bottle is tripped too quickly, some water will be entrained from below, so the operators usually wait a bit at each stop so as to collect a more representative sample from the target depth, but even a slightly smeared out sample with respect to depth will be acceptable to most data users. CTD processing routines have a number of checks to result in smoother data: pressure reversals (common when a rosette stops), gradient "spikes", statistical tests, and various averaging schemes that can result in a number that is not equivalent to what the rosette bottle is seeing, not to mention that the two types of samplers are usually physically separated in depth. Ideally, the CTD check should be an average of the CTD data just prior to the rosette trip so as to be equivalent to when the rosette sampler is integrating the water column (though stopped, the package moves up and down with the ship roll and changing wire angle).

The purpose of the salinity samples from every rosette bottle is to confirm that the water samples really come from the target depth and verify correct trips and tight seals, or no leakage during the cast. Comparison of the salinometer salinity with the CTD salinity provides a very sensitive validation of the quality of the water samples, and they were usually very good on this cruise. Where differences are greater than that expected from the combined precisions of the two measurements, one looks to see if there could have been a trip problem, leakage, sample collection errors, or analytical errors. It's often a judgement call, but it is not reasonable to believe that sample handling errors occur primarily in the upper water column, where the majority of the u'd values were. A little more care should have been taken to evaluate those apparent salt errors to see if they were possible, given the local gradients.

I have not changed many of the quality flags, tending to accept the originator's call, but these data are clearly over-edited. The following are a few specific comments that should be looked into:

STATIONS 111-127:

Most have isolated mid-depth bottle salts flagged "u", but examination of the density curves and theta/s curves compared to adjacent stations indicate the bottle salinity is more likely to be correct and the CTD slightly off. I asked Mark Rosenberg to check out stations 116, 117, and 120 and he confirmed that the down CTD trace agreed with the bottle data, so I switched the flags on those stations. However, single values at depths between 1800 and 2400db on the other stations should also be changed to accept the bottle salts as ok (if verified by the down CTD trace).

STATIONS 100, 104, 139, and 163:

These stations have negative oxygen values, either -.78, -.88, or -.98, that may be just a computation residual from a busted analyses. They are flagged as "bad" data, but they are not data at all and should be omitted, and flagged missing or lost.

There are quite a few stations (listed below) that have lines without any data, not even a CTD pressure. Some have nutrients or a salinity, but without a location for the data, they have no value and should not be left in to clutter eventual global archives. I suggest the lines without any pressure information be deleted on stations 25, 26, 31, 36, 37, 39, 41 43-45, 48, 63, 66, 68, 69, 71, 73, 77, 78, 80-83, 91, 95-97, 106, 107, 114, 131, 134, 155, 160, 164, 170, 175-182. Most of these are single lines labeled sample 140 or 240, but others have numerous empty fields.

STATIONS 30-32 PO4's:

Station 32 phosphates below 970db were u'd, apparently because they differ from station 31. However, 32 agrees well with 30, so could station 31 be off instead? All are lower than WOCE S04 PO4's.

STATION 26:

Station 26 is an unusual one; it is in a mid ocean ridge fracture zone and the deep temperatures are much colder than the previous station, indicating the passage is open to the south to the next basin. All phosphates were flagged "u", but if there is not analytical reason to do so, I would change them to ok. They agree well at the same potential temperatures with nearby stations.

Low surface PO4's: Ten stations have zero surface phosphates, unlike any other cruise that I have seen and unlike the NODC Atlas NESDIS 1 for nutrients. Plots of PO4 vs NO3 usually have a positive PO4 intercept at zero NO3 around 0.2 PO4, although values of less than 0.1 (but non-zero) are seen in the western subtropical gyres of the northern hemisphere. PO4/NO3 plots for this cruise compare well with P06 and P15N, except at the surface. Could there be a low level detection problem with the Alpkem Autoanalyzer? The zero values are suspect, and should be flagged "u". The problem stations are between stations 79 and 147.

STATION 116, 3441db:

The water samples are clearly poor and are not from this level. Salt and 3 of 4 nutrients were u'd, but O2 and NO2 were accepted as ok. The CTD confirms the O2 is poor also, and even though the NO2 would "fit" at this level, the water did not come from this depth, so all water samples should be u'd.

Below is a list of the lines in the .sea file where the DQE has made changes to the QUALT2 flags.

| EXPOCODE 3 | 1DSCG96 | _1, 31DSCG96_2 | WHP-ID P14S | S & P15S DATE | 010596 | to 03109 | 96 19980: | 930WHPOS | SIOSA | | | | | | | | | | | |
|------------|---------|----------------|-------------|---------------|--------|----------|-----------|----------|--------|-------|-------|-------|--------|--------|------|------|------|------|----------------|---------------|
| | STN CAS | ST SAMP BTL CT | D | | | | | | | NIT | NIT | PHS | | | DEL | DEL | C14 | C13 | | |
| | NBR NO | O NO NBR RA | W CTDPRS CI | IDTMP CTDSAL | CTDOXY | THETA | SALNTY | OXYGEN | SILCAT | RAT | RIT | PHT | CFC-11 | CFC-12 | C14 | C13 | ERR | ERR | QUALT1 | QUALT2 |
| | | | | | | | | | | | | | | | | | | | | |
| c16 | 1 1 | 112 404 -9 | 1604.8 2. | .8508 34.5703 | 154.04 | 2.7359 | 34.5732 | 162.52 | -9.00 | -9.00 | -9.00 | -9.00 | 0.091 | 0.043 | -9.0 | -9.0 | -9.0 | -9.0 | 2212411916699 | 2212311916699 |
| c127 | 4 1 | 104 1003 -9 | 117.7 7. | .1622 34.3993 | 281.42 | 7.1512 | 34.3992 | 282.10 | 6.21 | 17.55 | 0.35 | 1.30 | 4.298 | 2.228 | -9.0 | -9.0 | -9.0 | -9.0 | 3222233332299 | 322222222299 |
| c153 | 5 1 | 101 1022 -9 | 730.0 6. | .1802 34.3576 | 237.54 | 6.1144 | 34.3574 | 32.62 | 15.77 | 24.36 | 0.02 | 1.67 | 2.780 | 1.395 | -9.0 | -9.0 | -9.0 | -9.0 | 2222423322299 | 2222422222299 |
| c180 | 7 1 | 127 1234 -9 | 8.4 7. | .3430 34.1401 | 301.74 | 7.3422 | 34.1480 | 298.43 | 3.36 | 18.71 | 0.20 | 1.28 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 222222229999 | 2223222229999 |
| c296 | 10 2 | 211 1114 -9 | | .6186 34.7383 | | | | | | | | | | | | | | | 2222266636299 | |
| c358 | 12 2 | 203 439 -9 | | | | | | | | | | | | | | | | | 4244333239999 | |
| c364 | 13 1 | 121 417 -9 | | .0008 34.2096 | | | | | | | | | | | | | | | 222222222299 | |
| c402 | 14 1 | | | .4670 34.5815 | | | | | | | | | - | | | | | | 3225299991199 | |
| c528 | 18 1 | | | .7880 34.1270 | | | | | | | | | | | | | | | 2222222229999 | |
| c532 | 18 1 | 771 777 7 | | | | | | | | | | | | | | | | | 2222222229999 | |
| c543 | 18 1 | | | | | | | | | | | | | | | | | | 2222232229999 | |
| c547 550 | 18 1 | | | .0807 34.7410 | | | | | | | | | | | | | | | 2222232229999 | |
| C347 330 | 18 1 | | | .9947 34.7139 | | | | | | | | | | | | | | | 2222232222299 | |
| | 18 1 | | | .9228 34.7104 | | | | | | | | | | | | | | | 22222322229999 | |
| | | | | | | | | | | | | | | | | | | | | |
| ~C15 | 18 1 | | | | | | | | | | | | | | | | | | 2222632222299 | |
| c645 | 22 2 | 206 441 -9 | | | | | | | | | | | | | | | | | 3223266629999 | |
| c881 | 31 2 | 240 -9 -9 | | | | | | | | | | | | | | | | | | |
| c1038 | 35 1 | | | | | | | | | | | | | | | | | | 222222222299 | |
| c1070 | 36 1 | | | | | | | | | | | | | | | | | | 3229266669991 | |
| c1084 | 37 1 | | | .8990 34.7181 | | | | | | | | | | | | | | | 2229222222499 | |
| c1118 1119 | | | | .6984 34.7055 | | | | | | | | | | | | | | | 2222266649999 | |
| | 38 1 | | | | | | | | | | | | | | | | | | 2222266669999 | |
| c1254 | 43 1 | | | | | | | | | | | | | | | | | | 222242222210 | |
| c1270 | 43 1 | | | | | | | | | | | | | | | | | | 3224233232410 | |
| c1315 1317 | 45 1 | 108 440 -9 | | | | | | | | | | | | | | | | | 222222232299 | |
| | 45 1 | | | .7051 34.7401 | | | | | | | | | 0.059 | | | | | | 222222232299 | |
| | 45 1 | | | | | | | | | | | | | | | | | | 222222232299 | |
| c1345 | 46 1 | | | | | | | | | | | | | | | | | | 222222232490 | |
| c1390 | 47 2 | 201 1022 -9 | | | | | | | | | | | | | | | | | 3222266669999 | |
| c1539 | 52 1 | 123 1250 -9 | | | | | | | | | | | | 0.927 | -9.0 | -9.0 | -9.0 | -9.0 | 2224422222290 | 222422222290 |
| c1922 | 63 1 | 105 423 -9 | | .2560 34.7237 | | | | | | | | | | | | | | | 3223233334499 | |
| c1935 | 64 1 | 116 409 -9 | 478.4 5. | .1715 34.2241 | 262.54 | 5.1331 | 34.2565 | 276.72 | | | | | | | | | | | 4223322229911 | |
| c2229 | 73 1 | 124 1218 -9 | 525.8 7. | .2659 34.4211 | 251.35 | 7.2149 | 34.4244 | 251.23 | 8.37 | 20.71 | 0.01 | 1.45 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2223222221199 | 222222221199 |
| c2286 | 74 2 | 201 1022 -9 | 5385.3 0. | .9691 34.7041 | 209.79 | 0.5060 | 34.6873 | 209.27 | 119.27 | 31.77 | 0.00 | -9.00 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 4224233659910 | 4224333659910 |
| c2492 | 80 2 | 201 1022 -9 | 3448.0 1. | .2375 34.7220 | 203.06 | 0.9829 | 34.7214 | 210.74 | 111.48 | 31.99 | 0.00 | 2.18 | 0.042 | 0.151 | -9.0 | -9.0 | -9.0 | -9.0 | 2222266662499 | 2222366662499 |
| c2512 | 81 1 | 116 1211 -9 | 564.0 7. | .8179 34.4918 | 235.88 | 7.7606 | 34.5526 | 229.52 | -9.00 | -9.00 | -9.00 | -9.00 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2224299999999 | 2224399999999 |
| c2843 | 92 2 | 202 1030 -9 | 4190.2 0. | .9208 34.7076 | 206.04 | 0.5978 | 34.7072 | 206.36 | 122.04 | 32.15 | 0.00 | 2.22 | 0.043 | 0.028 | -9.0 | -9.0 | -9.0 | -9.0 | 222222232299 | 222222222299 |
| c2845 | 92 2 | 201 1022 -9 | 4237.3 0. | .9014 34.7065 | 206.26 | 0.5738 | 34.7072 | 208.69 | 122.85 | 32.28 | 0.00 | 2.22 | 0.054 | 0.126 | -9.0 | -9.0 | -9.0 | -9.0 | 2222266636499 | 2222266626499 |
| c2968 | 96 1 | 122 1265 -9 | 673.0 7. | .4823 34.4927 | 210.85 | 7.4152 | 34.4913 | 211.30 | 11.27 | 23.17 | 0.00 | 1.57 | 1.218 | 0.613 | -9.0 | -9.0 | -9.0 | -9.0 | 2222422222299 | 222222222299 |
| c2970 | 96 1 | 120 1015 -9 | 872.8 6. | .4577 34.4489 | 198.18 | 6.3762 | 34.4482 | 199.99 | 20.43 | 26.40 | 0.00 | 1.79 | 0.548 | 0.288 | -9.0 | -9.0 | -9.0 | -9.0 | 2222422222299 | 222222222299 |
| c2989 | 96 1 | 101 1022 -9 | 4846.1 0. | .9441 34.7053 | 208.33 | 0.5467 | 34.7049 | 207.72 | 123.20 | 32.39 | 0.00 | 2.22 | 0.069 | 0.031 | -9.0 | -9.0 | -9.0 | -9.0 | 2222466622299 | 2222266622299 |
| c3167 3169 | 101 2 | 203 999 -9 | 4807.7 1. | .0028 34.7083 | 206.98 | 0.6078 | 34.7074 | 206.16 | 121.68 | 32.53 | 0.00 | 2.21 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2222263629910 | 2222262629910 |
| | 101 2 | 202 1030 -9 | 5063.7 1. | .0137 34.7072 | 207.80 | 0.5881 | 34.7064 | 202.95 | 122.18 | 32.56 | 0.00 | 2.21 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2222223229910 | 2222322229910 |
| | 101 2 | 201 1022 -9 | 5227.8 1. | .0189 34.7065 | 207.81 | 0.5733 | 34.7066 | 207.33 | 122.58 | 32.54 | 0.00 | 2.21 | -9.000 | -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2222263669910 | 2222262669910 |
| c3344 | 106 1 | 107 1263 -9 | 3443.7 1. | .6337 34.7153 | 184.89 | 1.3697 | 34.7159 | 190.60 | 108.72 | 32.38 | 0.00 | 2.23 | 0.003 | 0.002 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222299 | 2222322222299 |
| c3462 | 110 2 | 234 1216 -9 | 44.6 20. | .1116 35.6224 | 228.82 | 20.1034 | 35.6264 | 233.32 | 1.22 | 0.01 | 0.00 | 0.10 | 2.336 | 1.267 | -9.0 | -9.0 | -9.0 | -9.0 | 2222422226699 | 222222226699 |
| c3464 | 110 2 | 232 1039 -9 | 95.7 15. | .2980 35.4279 | 240.33 | 15.2833 | 35.4331 | 243.71 | 1.48 | 0.28 | 0.03 | 0.21 | 2.748 | 1.455 | -9.0 | -9.0 | -9.0 | -9.0 | 222222232299 | 222222222299 |
| c3536 | 112 1 | 132 1039 -9 | 94.1 15. | .8199 35.4880 | 217.81 | 15.8051 | 35.4889 | 240.41 | 1.91 | 0.40 | 0.05 | 0.22 | 2.632 | 1.398 | -9.0 | -9.0 | -9.0 | -9.0 | 222222236610 | 222222226610 |
| c3556 | 112 1 | 112 1217 -9 | | | | | | | | | | | | | | | | | 2222422222210 | |
| c3582 | 113 1 | 122 1265 -9 | | | | | | | | | | | | | | | | | 2224322229999 | |
| c3587 | 113 1 | 117 1267 -9 | | | | | | | | | | | | | | | | | 2222322229999 | |
| c3589 | 113 1 | 115 1041 -9 | | | | | | | | | | | | | | | | | 2222422229999 | |
| c3645 | 115 1 | 132 1039 -9 | | .2967 35.5503 | | | | | | | | | | | | | | | 222222232299 | |
| c3651 | 115 1 | 126 1025 -9 | | .6264 34.5883 | | | | | | 20.17 | | | | | | | | | 2223222229999 | |
| c3677 3678 | | 236 1245 -9 | | .5176 35.8167 | | | | | | 0.05 | | | | | | | | | 222222222210 | |
| | 116 2 | 235 1113 -9 | | .5276 35.8183 | | | | | | | | | | | | | | | 222222222299 | |
| | | | | | | | | | • | | | | | | | | | | | |

c5947

| LIII OCODE | STDSCO. | 77 CT | SAMP BTL CTI | WIII ID I | 1115 & 1135 D. | 41E 010330 | 00 0310 | JO 1JJ00 | J J O WIII O L | JIODA | NIT | NIT | PHS | | DET. | DEL | C14 | C13 | | |
|------------|---------|-------|--------------|-----------|----------------|------------|------------|----------|----------------|--------|-------|------|------|---------------|------|------|------|------|---------------|---------------|
| | NBR | | - | | CTDTMP CTDS. | AT CHDOVV | יים דיים א | CAIMTV | OVVCEN | CTTCNT | | | | CFC-11 CFC-12 | | | | | | OUALT2 |
| | NDK | 110 | NAN AGNI ONI | W CIDERS | CIDIMP CIDS. | | InelA | SALINII | OXIGEN | SILCAI | NAI | K11 | РПІ | | | | EKK | EKK | | QUALIZ |
| c3689 | 116 | 2 | 224 1013 -9 | 675 2 | 7 0551 34 4 | | 6 9900 | 34 4164 | 226 59 | 8 82 | 22 83 | 0 00 | 1 55 | 0.966 0.477 | | -9 O | -9 N | -9 N | 2222422222299 | 2222222222299 |
| c3698 | 116 | _ | 215 1041 -9 | | | | | | | | | | | -0.002 0.002 | | | | | | |
| c3703 | 116 | 2 | 210 1301 -9 | | | | | | | | | | | -0.001 0.003 | | | | | | |
| c3734 37 | | | 115 1041 -9 | | 2.2843 34.6 | | | | | | | | | -9.000 -9.000 | | | | | | |
| | 117 | 1 | 114 1017 -9 | | 2.1070 34.6 | | | | | | | | 2.51 | -9.000 -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2223222229990 | 232222229990 |
| c3744 | 117 | 1 | 105 1264 -9 | 4564.6 | 1.0366 34.7 | 103 206.04 | 0.6685 | 34.7127 | 205.87 | 119.61 | 32.11 | 0.00 | 2.21 | 0.009 0.006 | -9.0 | -9.0 | -9.0 | -9.0 | 222222232290 | 222222222290 |
| c3821 | 120 | 2 | 236 1245 -9 | 4.7 | 23.9467 35.8 | 507 213.93 | 23.9457 | 35.8641 | 211.66 | 1.30 | 0.02 | 0.00 | 0.03 | 1.933 1.119 | -9.0 | -9.0 | -9.0 | -9.0 | 22222222210 | 232322222210 |
| c3843 38 | 44 120 | 2 | 214 1017 -9 | | 2.1045 34.6 | | | | | | | 0.00 | 2.51 | -0.001 0.004 | -9.0 | -9.0 | -9.0 | -9.0 | 222322222299 | 222222222299 |
| | 120 | 2 | 213 1302 -9 | | 1.9871 34.6 | | | | | | | 0.00 | 2.51 | 0.001 0.003 | -9.0 | -9.0 | -9.0 | -9.0 | 222322222299 | 222222222299 |
| c3951 | 123 | 1 | 114 1017 -9 | | 2.1895 34.6 | | | | | | | 0.00 | 2.50 | -9.000 -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2223222229999 | 222222229999 |
| c4013 | 125 | 3 | 324 1013 -9 | | 6.9901 34.4 | | | | | | | | | -9.000 -9.000 | | | | | | |
| c4095 41 | 07 127 | 2 | 214 1017 -9 | 2559.0 | 1.8973 34.6 | 520 145.97 | 1.7135 | 34.6590 | 145.66 | 128.66 | 36.13 | 0.00 | 2.53 | -0.001 0.000 | -9.0 | -9.0 | -9.0 | -9.0 | 222322222290 | 232222222290 |
| | 127 | 2 | 213 1302 -9 | 2810.0 | 1.8188 34.6 | 502 146.34 | 1.6132 | 34.6661 | 146.63 | 131.92 | 36.18 | 0.00 | 2.52 | 0.002 0.002 | -9.0 | -9.0 | -9.0 | -9.0 | 222322222290 | 232222222290 |
| | 127 | 2 | 212 1217 -9 | | | | | | | | | | | 0.003 0.001 | | | | | | |
| | 127 | 2 | | | | | | | | | | | | 0.002 0.002 | | | | | | |
| | 127 | 2 | | | | | | | | | | | | 0.001 0.002 | | | | | | |
| | 127 | 2 | 209 1233 -9 | | | | | | | | | | | -9.000 -9.000 | | | | | | |
| | 127 | 2 | 208 1227 -9 | 3992.6 | 1.3077 34.7 | 164 198.57 | 0.9948 | 34.7185 | 199.26 | 112.17 | 31.94 | 0.00 | 2.20 | 0.005 0.003 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222290 | 232222222290 |
| | 127 | 2 | 207 1263 -9 | | | | | | | | | | | -9.000 -9.000 | | | | | | |
| | 127 | 2 | 206 1262 -9 | 4566.6 | 1.0717 34.7 | 095 205.05 | 0.7023 | 34.7111 | 205.58 | 118.71 | 32.16 | 0.00 | 2.21 | 0.011 0.005 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222290 | 232222222290 |
| | 127 | 2 | 205 1264 -9 | 4811.8 | 1.0511 34.7 | 077 205.50 | 0.6540 | 34.7093 | 206.36 | 119.83 | 32.19 | 0.00 | 2.21 | 0.012 0.006 | -9.0 | -9.0 | -9.0 | -9.0 | 2222622222290 | 2322622222290 |
| | 127 | 2 | 204 1003 -9 | 5061.5 | 1.0523 34.7 | 067 206.09 | 0.6257 | 34.7085 | 206.26 | 120.78 | 32.22 | 0.00 | 2.21 | 0.009 0.005 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222290 | 232222222290 |
| | 127 | 2 | 203 1035 -9 | 5321.2 | 1.0691 34.7 | 067 190.77 | 0.6103 | 34.7088 | 206.65 | 121.16 | 32.25 | 0.00 | 2.22 | 0.009 0.006 | -9.0 | -9.0 | -9.0 | -9.0 | 224222222290 | 234222222290 |
| | 127 | 2 | 202 1030 -9 | 5602.1 | 1.0978 34.7 | 062 206.37 | 0.6028 | 34.7089 | 208.01 | 121.36 | 32.27 | 0.00 | 2.21 | 0.012 0.007 | -9.0 | -9.0 | -9.0 | -9.0 | 224222222290 | 234222222290 |
| c4254 | 132 | 1 | 136 1245 -9 | 5.1 | 27.8460 34.7 | 999 -9.00 | 27.8448 | 34.8053 | 199.16 | 1.02 | 0.02 | 0.00 | 0.00 | 1.637 0.959 | -9.0 | -9.0 | -9.0 | -9.0 | 2292622222210 | 2293622222210 |
| c4373 43 | 74 135 | 2 | 226 1025 -9 | 527.7 | 8.4781 34.5 | 337 201.07 | 8.4221 | 34.5336 | 204.22 | 9.11 | 22.92 | 0.00 | 1.58 | 1.131 0.555 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222210 | 2222233332210 |
| | 135 | 2 | 225 1119 -9 | 625.5 | 6.9897 34.4 | 038 223.91 | 6.9299 | 34.4054 | 224.06 | 9.13 | 22.96 | 0.00 | 1.58 | 0.942 0.466 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222210 | 2222233332210 |
| c4793 | 146 | 1 | 102 1030 -9 | 4940.2 | 1.0523 34.7 | 090 206.05 | 0.6401 | 34.7097 | 207.91 | 120.70 | 32.25 | 0.00 | 2.21 | 0.007 0.003 | -9.0 | -9.0 | -9.0 | -9.0 | 222222226610 | 2222322226610 |
| c4811 | 147 | 1 | 120 1015 -9 | 829.0 | 4.7780 34.4 | 723 148.90 | 4.7114 | 34.4689 | 147.28 | 53.59 | 33.97 | 0.00 | 2.36 | 0.023 0.009 | -9.0 | -9.0 | -9.0 | -9.0 | 222322222299 | 222222222299 |
| c5059 | 154 | 1 | 124 1244 -9 | 575.5 | 6.6821 34.4 | 386 153.19 | 6.6285 | 34.4854 | 148.48 | 30.37 | 30.54 | 0.00 | 2.11 | -9.000 -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2223222229999 | 222222229999 |
| c5114 | 155 | 1 | 106 1262 -9 | 3815.6 | 1.4825 34.6 | 398 165.83 | 1.1838 | 34.6922 | 166.18 | 132.95 | 35.15 | 0.00 | 2.40 | -0.001 0.000 | -9.0 | -9.0 | -9.0 | -9.0 | 222222222299 | 222223222299 |
| c5452 | 165 | 1 | 130 1257 -9 | | 20.5119 35.8 | | | | | | | 0.01 | 0.71 | 1.965 1.055 | -9.0 | -9.0 | -9.0 | -9.0 | 222422222210 | 222322222210 |
| c5483 | 166 | 2 | 235 1113 -9 | 21.7 | 28.8105 35.4 | 380 194.94 | 28.8053 | 35.5323 | 196.00 | 1.52 | 0.10 | 0.01 | 0.22 | -9.000 -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 2223222229999 | 232222229999 |
| c5637 | 170 | 1 | 125 1119 -9 | 573.6 | 7.4558 34.6 | 053 47.04 | 7.3990 | 34.6018 | 44.01 | 44.91 | 39.55 | 0.00 | 2.75 | 0.011 0.005 | -9.0 | -9.0 | -9.0 | -9.0 | 2223622222299 | 2222622222299 |
| c5688 | 171 | 1 | 110 1301 -9 | 3314.3 | 1.5556 34.6 | 317 148.42 | 1.3068 | 34.6842 | 153.44 | 140.83 | 35.86 | 0.00 | 2.47 | -9.000 -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 222222221199 | 2223333331199 |
| c5699 | 172 | 2 | 235 1113 -9 | | 26.5125 35.3 | | | | | | | 0.32 | 0.48 | -9.000 -9.000 | -9.0 | -9.0 | -9.0 | -9.0 | 222222229910 | 2223222229910 |
| c5737 | 173 | 2 | 233 1021 -9 | 81.0 | 26.6480 35.5 | 076 200.63 | 26.6296 | 35.5114 | 200.45 | 2.55 | 4.02 | 0.32 | 0.49 | 1.719 1.101 | -9.0 | -9.0 | -9.0 | -9.0 | 2222322223399 | 222222223399 |
| c5742 | 173 | 2 | 228 1230 -9 | 326.4 | 10.8877 34.7 | 308 69.58 | 10.8475 | 34.7792 | 70.52 | 25.57 | 29.37 | 0.00 | 2.05 | 0.379 0.223 | -9.0 | -9.0 | -9.0 | -9.0 | 2222322222399 | 22222222399 |
| c5866 | 176 | 1 | 112 1217 -9 | 3648.1 | 1.4940 34.6 | 375 162.59 | 1.2126 | 34.6827 | 157.82 | 135.40 | 35.75 | 0.00 | 2.46 | -0.002 -0.001 | -9.0 | -9.0 | -9.0 | -9.0 | 2223666662499 | 2223366662499 |
| | | _ | | = | | | | | | | | | | | | | | | | |

178 1 103 1302 -9 5100.1 1.0852 34.7087 205.62 0.6528 34.7089 201.39 120.21 32.46 0.00 2.21 0.003 0.001 -9.0 -9.0 -9.0 -9.0 2222222222299 222322222299

APPENDIX 9b: Responses to WOCE DQE comments on initial .sea file

We have removed 4 oxygen values that were 'lost' data.

We have removed samples where no CTD pressures or other parameters were reported. We have left in some samples (typically sample '140') which were surface samples collected from the underway pumping system while on station. These samples we analysed for tcarbn and alkali, and although no CTD values are available, we feel it is useful to include them in th file for completeness.

We have adopted most of the suggested changes in the salnty, ctdsal and oxygen flags suggested by A. Mantyla.

The following response to the Nutrient DQE comments was provided by Calvin Mordy: Changes to Version 8 of P15/P14S Nutrient Data (6/8/00)

CWM initiated edits

| 45 | 102-105 | Changed PO4 flag from 2 to 6 (oversight) |
|-----|---------|--|
| 139 | 108 | Changed PO4 flag from 5 to 3 (typo) |

A. Mantyla initiated edits

| PO4 | | |
|--------|----------|--|
| 32 | REJECTED | Deep water remains flagged as 4 due to DOC phosphoric acid contamination |
| 26 | ACCEPTED | Changed flag to 2 or 6 except for bottle 3 (QF=3) |
| 83-142 | ACCEPTED | Shallow PO4s less than 0.4 umol/kg were flagged as questionable. |

ACCEPTED changes suggested by A. Mantyla (FLAG = SIL/NO3/NO2/PO4)

| STA | BOTTLE | OLD FLAG | NEW FLAG | |
|-----------------|-------------|-------------|-------------|--|
| 4 104 3333 2222 | | | | |
| 5 101 2332 2222 | | | | |
| 12 | 203 | 3323 | 3333 | |
| 13 | 121 | 2222 | 3333 | |
| 18 | 105-108,112 | 3222 | 2222 | Reruns due to bubble in flowcell look ok |
| 45 | 106-108 | 2223 | 2222 | |
| 46 | 112 | 2223 | 2222 | |
| 64 | 116 | 2222 | 3333 | |
| 92 | 201,202 | 2223 | 2222 | |
| 110 | 232 | 2223 | 2222 | |
| 112 | 132 | 2223 | 2222 | |
| 115 | 132 | 2223 | 2222 | |
| 116 | 210 | 3323 | 3333 | |
| 117 | 105 | 2223 | 2222 | |
| 135 | 225,226 | 2222 | 3333 | |
| 171 | 110 | 2222 | 3333 | |

REJECTED changes suggested by A. Mantyla (FLAG = SIL/NO3/NO2/PO4)

| STA | вот | FLAG | Rejected Flag | COMMENT |
|-----|-----|------|------------------|--|
| 10 | 211 | 6663 | 6662 | Air bubble in PO4 peak, rerun was suspect |
| 47 | 201 | 6666 | 3666 | No problem with silicic acid peak or concentraton |
| 101 | 201 | 6366 | 6266 | Peak corrected for severe bubble drift, still questionable |
| 101 | 202 | 2322 | 2222 | Peak corrected for severe bubble drift, still questionable |
| 101 | 203 | 6362 | 6262 | Peak corrected for severe bubble drift, still questionable |
| 155 | 106 | 2222 | 2322 | NO3 peak is ok, not a flier |

APPENDIX 10a: DQE Evaluation of CTD data for RV Discoverer Cruise CGC96

Mark Rosenberg (October 1998)

This report contains a data quality evaluation of the CTD data files for the Pacific sector cruise along WOCE meridional sections P14S and P15S (Figure 1) on the RV Discoverer in January to March, 1996. Bottle data are evaluated by Arnold Mantyla in a separate report. The data are in general of good quality, and help to fill a former sampling void for the Southern Ocean in particular. Notably, the P15S section provides a contiguous high density sampling through tropical, subtropical and Antarctic waters, crossing several major fronts. The most significant problem is the biasing of CTD salinity data for individual stations, as detailed below. Note that the comments in this report are offered as suggestions (hopefully helpful ones) from an outside perspective, focusing on various data and methodology problems. They are not intended to detract from the general high standard and usefulness of the data set.

STATION SUMMARY FILE (.sum)

- Stations 21 and 77 are listed as cast 2 in .sum and .ctd files, but cast 1 in .sea file needs clarification.
- The uncorrected sounder depth at the bottom of the cast appears wrong for stations 44 and 50, as follows (N.B. depth from CTD = altimeter reading + maximum pressure recalculated in meters):

| Station | depth from | wire out | sounder depth at |
|---------|------------|----------|--------------------|
| | CTD (m) | (m) | bottom of cast (m) |
| 44 | 4134 | 4114 | 3630 |
| 50 | 4409 | 4423 | 4140 |

• Sound speed and transducer depth information for the ship s sounder were not provided in the documentation. Corrected depth in the .sum file was therefore calculated from the CTD at the bottom of the cast i.e. altimeter reading + maximum CTD pressure recalculated in meters (using the method of Saunders and Fofonoff, 1976). For stations with no altimeter reading, no corrected depth was calculated. These corrected depth values are in an ascii file corrdepth.dat, and have not been merged into the .sum file.

SALINITY

In the following discussion, only CTD and bottle values with a quality flag of 2 are considered (i.e. QUALT1=2 for CTDSAL and SALNTY in the .sea file). See Table 3 for a station by station summary of data problems.

Scatter of salinity residuals

The salinity residual data ΔS (where ΔS = bottle — CTD salinity difference) for all depths is shown in Figure 2. Outliers were rejected iteratively by the data processors, as described in the cruise report. Below 500 dbar, scatter of ΔS is greatly reduced (Figure 3), so the outliers are from samples shallower than 500 dbar. Much of the scatter for the shallower samples is no doubt due to sampling errors in steep vertical gradients. However, the sign of ΔS can not always be reconciled with the direction of the vertical salinity gradient (assuming here that the CTD sensors are below the Niskin bottles on the rosette package). It may be possible to improve this scatter by increasing the averaging period for the upcast CTD burst data from 2 seconds to 10 seconds. This larger averaging period more closely matches the swell wave period, and may better average out the effect of the rolling ship during bottle stops.

Biasing of CTD salinity data for individual stations

Standard deviations for ΔS for the whole cruise were calculated from data in the .sea file (uncorrected data in Table 1). The value of 0.0018, calculated using all sampling depths and $|\Delta S| \leq 0.008$, is a reasonable estimate of the salinity accuracy for the cruise (note that 0.008 ~ 2.8*0.0029, where 0.0029 is the standard deviation for all bottles from Table 1). When the cruise is viewed as a whole, this salinity accuracy meets WOCE requirements and ΔS varies about a mean of zero (Figures 2 and 3). However when individual stations are examined, there is a significant problem with biasing of the CTD salinity data (Table 3). This is clearly evident through visual examination of Figures 2 and 3: the mean value of ΔS for each station varies (a good example is for stations 46 to 53, where ΔS is clearly negative).

The biasing is a direct result of the conductivity calibration method as described in the cruise report, where the whole cruise is fitted in one group and the fourth order station dependent slope correction fails to fully track the variation of conductivity sensor behaviour over the cruise. Breaking down the stations into smaller calibration groups is strongly recommended — this would allow the station dependent slope correction to remove the bias for individual stations.

To prove this point, I ve done an extra fit to the ΔS data to minimize the residuals and biasing, as follows. Note that back-calculating conductivity made no difference to the resulting corrections, so salinity was used. Firstly, Figure 3 was examined and station groups formed to reflect the variation through the cruise of mean ΔS for each station (Table 2). Next, samples for which $|\Delta S| > 0.008$ were rejected. A linear fit of CTD to bottle salinity (i.e. S_{ctd} to S_{btl}) was then found for each station group:

$$S_{ctd} = a_1 S_{btl} + a_2$$

for fit coefficients a₁ and a₂. Lastly, corrected salinity S_{cor} was calculated for each station group:

$$S_{cor} = (S_{ctd} - a) / a_1$$

The resulting S_{btl} — S_{or} residuals are plotted in Figure 4 (all depths) and Figure 5 (deeper than 500 dbar). Standard deviation calculations for these corrected data are shown in Table 1.

As expected, there is only a small improvement to standard deviations calculated for the whole cruise (Table 1). The important point is the marked improvement to the biasing of individual stations, revealed by comparing Figure 5 to Figure 3. Corrected and uncorrected ΔS vertical profiles for a few example stations are plotted in Figure 6. Stations for which the correction improves salinity biasing are indicated in Table 3.

I hope this does not put too fine a point on the conductivity calibration. True, the salinity biasing errors for the submitted data are less than 0.002, however ΔS values for each station ought to be scattered around a mean value of zero. Clearly, breaking down a cruise into smaller station groups for the calibration of CTD conductivity significantly improves the calibration. Note that the correction done here is only a rough version — for a real calibration on selected station groups, groups would be selected with a linear variation of station mean ΔS , allowing the station dependent slope correction to take effect within each group and giving even better calibration results.

Table 1: Standard deviations for salinity residuals ΔS (using only bottle and CTD data for which the quality flag=2), where uncorrected data are as submitted to WHPO, and corrected data are with additional ΔS fit applied.

| data | standard deviation of | standard deviation of |
|------------------------------------|-------------------------------|-----------------------------|
| | ΔS , uncorrected data | ΔS , corrected data |
| all depths | 0.0029 | 0.0028 |
| deeper than 500 dbar | 0.0010 | 0.0009 |
| all depths, $ \Delta S \le 0.008$ | 0.0018 | 0.0017 |

Table 2: Station grouping used for additional fit of salinity residuals.

| 1-3 | 41-45 | 75-80 | 133-137 | 162-174 |
|-------|-------|---------|---------|---------|
| 4-8 | 46-53 | 81-99 | 138-146 | 175-182 |
| 9-18 | 54-59 | 100-105 | 147-148 | |
| 19-25 | 60-62 | 106-109 | 149-151 | |
| 26-30 | 63-65 | 110-121 | 152-154 | |
| 31-35 | 66-70 | 122-129 | 155-157 | |
| 36-40 | 71-74 | 130-132 | 158-161 | |

Problem salinity bottle data

Comparing bottle salinity values for adjacent stations on deepwater θ -S curves, the following problems were found:

| station | problem | recommendation |
|---------|----------------------------------|--------------------------|
| 19 | bottle salts high by ~0.002 | don t use in calibration |
| 49 | bottle salts low by ~ 0.001 | don t use in calibration |
| 117 | bottle salts high by ~0.002 | don t use in calibration |
| 164 | bottle salts low by ~ 0.001 | don t use in calibration |

OXYGEN

The CTD oxygen data are of the highest quality. Calibration results are excellent, and oxygen profiles are remarkably free of noise. The Seabird design of constant flow past the oxygen sensor membrane appears to have merit. Due to the inherent small scale variability of membrane-type oxygen sensors, I do not believe the concerns expressed about data despiking later in this report are relevant here. Oxygen residual data are plotted in Figure 7, noting that large outliers lie beyond the axis limits on the graph.

Many stations appear to have suspicious oxygen data for the top few bins, due to transient sensor errors as the instrument enters the water and the pump winds up, combined with the despiking errors discussed below. Stations where these errors are greater than \sim 4 μ mol/kg, and where there is no matching T/S feature, are summarised in Table 4, and a quality flag of 3 is recommended for bins not already flagged as 7 in the .ctd files. Also listed in Table 4 are a few stations where most of the CTD oxygen profile has a constant offset from the bottle values. In all cases the offset is small (\sim 1%), however given the high quality of the CTD oxygen data set these stations are worth pointing out.

TEMPERATURE

The following temperature spikes were identified in the .ctd files:

| station 43: | very spikey T structure between 100 and 300 dbar on downcast, not reflected in |
|--------------|---|
| | salinity — would like to confirm with upcast CTD temperature |
| station 45: | temperature spike at 9 dbar, flag as 3 in .ctd file |
| station 49: | temperature spike at 8-11 dbar, flag as 3 in .ctd file |
| station 54: | small temperature spike at 7 dbar, status uncertain due to despiking of salinity data |
| station 60: | small temperature spike at 5-6 dbar, status uncertain due to despiking of salinity data |
| station 64: | small temperature spike at 7-8 dbar, status uncertain due to despiking of salinity data |
| station 106: | small temperature spike at 7 dbar, status uncertain due to despiking of salinity data |
| station 108: | small temperature spike at 4 dbar, status uncertain due to despiking of salinity data |

DESPIKING AND INTERPOLATION

There is a large number of interpolated CTD temperature and salinity values in the .ctd files, flagged as 6. This needs an explanation i.e. is it due to fouling of the pump line, data dropouts from the instrument or some other electronic problem? Or is it mainly due to interpolations from the program DELOOP mentioned in the cruise report?

I have concerns about despiking of the temperature and salinity data (program DESPIKE mentioned in the cruise report). In particular, salinity data near the surface is often continued to the surface as an identical value from the first good data bin a few decibars down, and flagged as 7 (program FILLSFC mentioned in the cruise report). As a result, temperature features are often not relected in the salinity data (e.g. Figure 8), and density inversions can occur. In some instances, erroneous salinity features may appear (e.g. station 159, top 9 dbar in Figure 8). Rather than inserting these fictional salinity data near the surface, it might be preferable to leave the original bad data there and flag as 3 or 4, or else remove the data entirely. In general, all data in the top 15 dbar with a 7 flag should be regarded as questionable.

DENSITY INVERSIONS

Locations of unstable vertical density gradients are shown in Figure 9; only gradients more unstable than -0.003 kg/m³/dbar are shown. Unstable density gradient values are summarised in Table 5. All except for station 40 occur in the top 20 dbar. In addition, almost all occur where the CTD salinity data has been despiked (flag 7 in the .ctd file). The worst instance is for station 78 at 9 dbar: a temperature feature occurs at this level, however the salinity data has been artificially smoothed, leaving a large density instability.

INTRA-CRUISE COMPARISON

Deepwater θ -S and θ -oxygen curves compare well for the coincident station pair 93/94. More variability is evident for the station pair 159/179.

COMPARISONS WITH OTHER CRUISES

Deepwater θ -S and θ -oxygen curves were compared for P15S stations coincident with other cruise data sets, as follows. In general, there is reasonable consistency between the different data sets.

P15S and P15N (P.I. H. Freeland) (Figure 10) P15N salinity lower than P15S by on average 0.001. No CTD oxygen data for P15N.

P15S and P31 (P.I. D. Roemmich) (Figure 11)

P31 salinity lower than P15S by on average 0.001. Oxygen data compare well.

P15S and P21 (P.I. H. Bryden on western leg) (Figure 12)

Limited data only for comparison, and stations separated longitudinally by 19 miles. P21 salinity higher than P15S by ~0.001 above θ =1.3°; compare well at bottom. Oxygen data compare well below θ =1.25°

P15S and P6 (P.I. M.McCartney on central leg) (Figure 12)

Limited data only for comparison, and stations separated longitudinally by up to 12 miles. Salinity data compare well.

Oxygen data compare well around the oxygen minimum; at the bottom, P6 is higher by ~2µmol/kg

P15S and S4P (P.I. Koshlyakov) (Figure 12)

Limited data only for comparison, and stations separated longitudinally by up to 17.5 miles. S4P salinity lower by ~ 0.0015 .

Oxygen data a bit variable, but within ~1%.

DOCUMENTATION

The documentation is good and thorough. It would be useful to add the following information:

- PDR sound speed used for sounder readings, and whether or not readings have been corrected for transducer depth below the waterline;
- criteria used for despiking.

REFERENCES

Saunders, P.M. and Fofonoff, N.P., 1976. Conversion of pressure to depth in the ocean. Deep Sea Research, 23:109-111.

| station | comment | recommendation |
|---------|--|-------------------------------|
| *8 | S _{ctd} high by ~0.001 below 1500 dbar (impressive interfingering for this station!) | use smaller station groupings |
| *9 | S _{ctd} high by ~0.0015 for whole profile | use smaller station groupings |
| *10 | S_{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *11 | S _{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *13 | S _{ctd} high by ~0.001 below 1500 dbar | use smaller station groupings |
| *15 | S _{ctd} high by ~0.001 below 2000 dbar | use smaller station groupings |
| *16 | S _{ctd} high by ~0.001 below 2000 dbar | use smaller station groupings |
| *17 | S_{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *18 | S_{ctd} high by ~0.0015 for whole profile | use smaller station groupings |
| 23 | S _{ctd} high by ~0.001 below 1000 dbar | possibly due to bottles |
| *26 | S _{ctd} high by ~0.001 for whole profile (interesting T feature at 2600 dbar on downcast) | use smaller station groupings |
| *27 | S _{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *29 | S _{ctd} high by ~0.001 below 800 dbar, low at surface | |
| 37 | S _{ctd} low by ~0.001 below 1000 dbar | Bank S |
| 38 | S _{ctd} low by ~0.001 for whole profile | |
| *41 | S _{ctd} high by ~0.001 below 500 dbar, low at surface | use smaller station groupings |
| *46 | S _{ctd} high by ~0.001 below 1000 dbar | use smaller station groupings |
| *47 | S _{ctd} high by ~0.001 below 1000 dbar | use smaller station groupings |
| *48 | S _{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *50 | S _{ctd} high by ~0.001 below 1000 dbar | use smaller station groupings |
| *51 | S_{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *52 | S_{ctd} high by ~ 0.001 for 1000 to 4000 dbar | use smaller station groupings |
| *53 | S _{ctd} high by ~0.001 below 2000 dbar | use smaller station groupings |
| *54 | S_{ctd} low by ~0.001 below 2000 dbar | use smaller station groupings |
| *57 | S_{ctd} low by ~ 0.001 for whole profile | use smaller station groupings |
| *58 | S_{ctd} low by ~0.001 for whole profile | use smaller station groupings |
| 61 | 1 to 5 dbar transient/despiking error in S _{ctd} | |
| 63 | 1 to 10 dbar transient/despiking error in S _{ctd} | |
| *63 | S_{ctd} low by ~0.001 for whole profile | use smaller station groupings |
| *64 | S_{ctd} low by ~ 0.001 for whole profile | use smaller station groupings |
| *65 | S_{ctd} low by ~ 0.001 for whole profile | use smaller station groupings |
| 69 | S_{ctd} high by ~0.001 below 1500 dbar | |
| 70 | S_{ctd} low by ~ 0.001 for whole profile | |
| 73 | S_{ctd} high by ~0.001 below 1500 dbar | |
| 74 | S _{ctd} high by ~0.001 below 2500 dbar (interesting S in top 120 m) | |
| 75 | S _{ctd} high by ~0.001 for whole profile | |
| *76 | S _{ctd} high by ~0.001 below 1000 dbar | use smaller station grouping |
| | ···· · · · · · · · · · · · · · · · · · | - 6 - T |

| Table 3: | (continued) | |
|----------|--|-----------------------------------|
| *77 | S _{ctd} high by ~0.001 below 2000 dbar | use smaller station grouping |
| *79 | S _{ctd} high by ~0.001 below 1000 dbar | use smaller station grouping |
| *80 | S_{ctd} high by ~ 0.001 for 2500 to 3500 dbar | use smaller station grouping |
| 90 | S _{ctd} low by ~0.001 for whole profile | ase smarrer station grouping |
| 95 | S_{ctd} high by ~ 0.001 for whole profile | |
| 96 | S _{ctd} high by ~0.001 for top 3000 dbar | |
| *100 | S_{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *101 | S _{ctd} high by ~0.001 below 500 dbar | use smaller station groupings |
| *102 | S_{ctd} high by ~ 0.001 below 500 dbar | use smaller station groupings |
| *103 | S _{ctd} high by ~0.001 below 500 dbar | use smaller station groupings |
| *105 | S _{ctd} high by ~0.001 below 500 dbar | use smaller station groupings |
| *111 | S _{ctd} low by ~0.0008 for whole profile | use smaller station groupings |
| *112 | S _{ctd} low by ~0.000 for whole profile | use smaller station groupings |
| *115 | S _{ctd} low by ~0.001 for whole profile | use smaller station groupings |
| *119 | S _{ctd} low by ~0.001 for whole profile S _{ctd} low by ~0.001 below 3500 dbar | use smaller station groupings |
| *120 | S _{ctd} low by ~0.001 below 3500 dbar S _{ctd} low by ~0.001 below 1200 dbar | use smaller station groupings |
| *121 | S _{ctd} low by ~0.001 below 1200 dbar | use smaller station groupings |
| 121 | S _{ctd} low by ~0.0015 below 2000 dbar S _{ctd} low by ~0.001 below 3000 dbar | use smaller station groupings |
| 124 | 1 to 13 dbar transient/despiking error in S _{ctd} | |
| 126 | S _{ctd} low by ~0.001 for whole profile | |
| 120 | upcast CTDSAL values in .sea file bad | flag as 3 in .sea file the CTDSAL |
| 127 | below 2500 dbar (possible fouling) | values for samples 202 to 214 |
| | below 2300 dour (possible fouring) | values for samples 202 to 214 |
| 128 | S_{ctd} high by ~ 0.001 for 1000 to 5000 dbar | |
| *130 | S _{ctd} high by ~0.001 for whole profile | use smaller station groupings |
| *132 | S _{ctd} high by ~0.001 for 2000 to 5000 dbar | use smaller station groupings |
| 133 | S_{ctd} low by ~ 0.001 below 1500 dbar | |
| *138 | S _{ctd} high by ~0.0008 below 2000 dbar | use smaller station groupings |
| *140 | S _{ctd} high by ~0.001 for 1000 to 4000 dbar | use smaller station groupings |
| *143 | S _{ctd} high by ~0.001 for 1500 to 4000 dbar | use smaller station groupings |
| 144 | S _{ctd} high by ~0.0015 below 2000 dbar | |
| 146 | 1 to 6 dbar transient/despiking error in S _{ctd} | |
| *147 | S _{ctd} high by ~0.0015 for whole profile | use smaller station groupings |
| *148 | S _{ctd} high by ~0.001 below 500 dbar | use smaller station groupings |
| *154 | S _{ctd} high by ~0.001 for 1200 to 3500 dbar | use smaller station groupings |
| *155 | S_{ctd} low by ~0.001 below 1000 dbar | use smaller station groupings |
| *156 | S_{ctd} low by ~0.001 below 1000 dbar | use smaller station groupings |
| *158 | S _{ctd} high by ~0.001 below 500 dbar | use smaller station groupings |
| 159 | 1 to 9 dbar transient/despiking error in S _{ctd} | |
| 160 | 1 to 10 dbar transient/despiking error in S _{ctd} | |
| 160 | S_{ctd} high by ~0.001 for 500 to 4000 dbar, | |
| | low below 4000 dbar | |
| 1.66 | | |
| 168 | S_{ctd} high by ~ 0.001 for 800 to 4500 dbar | |
| 173 | S_{ctd} low by ~0.001 below 1000 dbar | |

Table 4: Suspicious CTD oxygen data

| station | comment | recommendation |
|----------|---|--------------------------------|
| 8 | high by ~2 μmol/kg below 500 dbar | calibrate station individually |
| 10 | high by ~2 μmol/kg below 1000 dbar | calibrate station individually |
| 13 | 1 to 5 dbar transient/despiking error | |
| 16 | 1 to 8 dbar transient/despiking error | |
| 17 | 1 to 7 dbar transient/despiking error | |
| 18 | 1 to 8 dbar transient/despiking error | |
| 19 | 1 to 7 dbar transient/despiking error | |
| 21 | 1 to 7 dbar transient/despiking error | |
| 22 to 25 | 1 to 8 dbar transient/despiking error | |
| 27 | 55 to 57 dbar spike | flag as 3 in .ctd file |
| 29 | 1 to 8 dbar transient/despiking error | |
| 32 | 1 to 11 dbar transient/despiking error | |
| 40 | 1 to 8 dbar transient/despiking error | |
| 43 | 1 to 10 dbar transient/despiking error | |
| 44 | 1 to 11 dbar transient/despiking error | |
| 45 | 1 to 12 dbar transient/despiking error | |
| 46, 47 | 1 to 10 dbar transient/despiking error | |
| 52 | 1 to 11 dbar transient/despiking error | |
| 54 | 1 to 10 dbar transient/despiking error | |
| 55 | 1 to 11 dbar transient/despiking error | |
| 63 | 1 to 11 dbar transient/despiking error | |
| 112 | 1 to 12 dbar transient/despiking error | |
| 119 | 12 dbar spike | flag as 3 in .ctd file |
| 135 | high by $\sim 2.5 \mu$ mol/kg for whole profile | calibrate station individually |
| 148 | 1 to 5 dbar transient/despiking error | |
| 152, 153 | 1 to 4 dbar transient/despiking error | |
| 155 | 1 to 4 dbar transient/despiking error | |
| 161 | 1 to 11 dbar transient/despiking error | |
| 164 | 1 to 3 dbar transient/despiking error | |
| 165 | 1 to 6 dbar transient/despiking error | |

Table 5: Density inversions < -0.003 kg/m 3 /dbar, and quality flag for salinity in .ctd file for the pressure bin.

| atn | progguro | density sal | | atn | proceuro | density | co1 | atn n | roggur | e density sa | o.1 |
|-----|-----------------|--------------|---------------|------|-----------------|----------|-----|-------|--------|--------------|-----|
| Sui | pressure (dbar) | gradient fla | | SIII | pressure (dbar) | gradient | | - | dbar) | gradient fl | |
| | (ubai) | gradient ma | B | | (ubai) | gradient | mag | (1 | ioai) | gradient in | ag |
| 8 | 7 | -0.0057 | 7 | 106 | 8 | -0.016 | 3 7 | 155 | 10 | -0.0048 | 6 |
| 8 | 8 | | <i>.</i> 7 | 107 | 2 | -0.005 | | 155 | 11 | -0.0048 | 2 |
| 10 | 7 | | 7 | 107 | 3 | -0.004 | | 157 | 5 | -0.0099 | 7 |
| 20 | 4 | | 7 | 107 | 9 | -0.019 | | 159 | 6 | -0.0052 | 7 |
| 22 | 6 | | 7 | 107 | 12 | -0.009 | | 162 | 5 | -0.0036 | 7 |
| 40 | 105 | | 6 | 107 | 13 | -0.009 | | 162 | 12 | -0.0030 | 6 |
| 40 | 106 | -0.0031 | 6 | 107 | 14 | -0.010 | 0 2 | 162 | 13 | -0.0030 | 6 |
| 40 | 107 | -0.0032 | 2 | 108 | 5 | -0.010 | 8 7 | 162 | 14 | -0.0030 | 2 |
| 45 | 9 | -0.0102 | 7 | 109 | | -0.019 | 3 7 | 165 | 4 | -0.0050 | 7 |
| 49 | 8 | -0.0181 | 7 | 110 | 2 | -0.003 | 7 7 | 167 | 4 | -0.0125 | 7 |
| 54 | 8 | -0.0044 | 7 | 111 | 2 | -0.009 | 4 7 | 169 | 3 | -0.0053 | 7 |
| 57 | 2 | -0.0041 | 7 | 112 | 2 | -0.012 | 2 7 | 169 | 5 | -0.0034 | 7 |
| 60 | 7 | -0.0114 | 7 | 113 | 3 | -0.003 | 7 7 | 170 | 2 | -0.0035 | 7 |
| 64 | 8 | -0.0054 | 7 | 113 | 4 | -0.003 | 4 7 | 174 | 4 | -0.0036 | 7 |
| 64 | 9 | -0.0040 | 7 | 117 | 3 | -0.004 | 6 7 | 176 | 2 | -0.0130 | 7 |
| 68 | 2 | -0.0052 | 7 | 117 | 7 | -0.005 | 9 7 | 176 | 5 | -0.0033 | 7 |
| 69 | 11 | -0.0061 | 7 | 120 | 2 | -0.003 | 2 7 | 177 | 3 | -0.0049 | 7 |
| 69 | 12 | -0.0030 | 6 | 121 | 2 | -0.004 | 0 7 | 177 | 4 | -0.0035 | 7 |
| 69 | 13 | -0.0030 | 6 | 124 | | -0.013 | 5 7 | 180 | 2 | -0.0108 | 7 |
| 69 | 14 | -0.0031 | 2 | 124 | 4 | -0.004 | 7 7 | 181 | 2 | -0.0073 | 7 |
| 70 | 4 | -0.0058 | 7 | 125 | 2 | -0.004 | 2 7 | 182 | 2 | -0.0034 | 7 |
| 70 | 6 | -0.0046 | 7 | 126 | 2 | -0.005 | 5 7 | 182 | 3 | -0.0078 | 7 |
| 71 | 7 | -0.0054 | 7 | 131 | 7 | -0.003 | 3 7 | | | | |
| 78 | 5 | -0.0094 | 7 | 131 | 11 | -0.005 | 3 7 | | | | |
| 78 | 8 | -0.0080 | 7 | 132 | 2 | -0.003 | 4 7 | | | | |
| 78 | 9 | -0.0254 | 7 | 134 | 4 | -0.003 | 0 7 | | | | |
| 82 | 3 | -0.0032 | 7 | 134 | 7 | -0.003 | 3 7 | | | | |
| 83 | 8 | -0.0089 | 7 | 135 | 2 | -0.006 | 3 7 | | | | |
| 84 | 2 | | 7 | 136 | 2 | -0.012 | 5 7 | | | | |
| 85 | 5 | | 7 | 139 | 9 | -0.010 | | | | | |
| 86 | 2 | | 7 | 140 | 6 | -0.013 | | | | | |
| 87 | 2 | | 7 | 143 | 2 | -0.007 | | | | | |
| 88 | 5 | | 7 | 143 | 3 | -0.006 | | | | | |
| 89 | 4 | | 7 | 143 | 4 | -0.003 | | | | | |
| 89 | 5 | | 7 | 144 | | -0.006 | | | | | |
| 90 | 5 | | 7 | 148 | 2 | -0.008 | | | | | |
| 90 | 9 | | 7 | 152 | | -0.004 | | | | | |
| 91 | 4 | | 7 | 153 | 2 | -0.013 | | | | | |
| 99 | 3 | | 7 | 154 | | -0.005 | | | | | |
| 101 | 4 | | 7 | 154 | | -0.005 | | | | | |
| 101 | 8 | | 7 | 155 | | -0.004 | | | | | |
| 102 | | | 7 | 155 | | -0.004 | | | | | |
| 105 | | | 7 | 155 | | -0.004 | | | | | |
| 106 | 4 | -0.0038 | 7 | 155 | 9 | -0.004 | 8 6 | | | | |

Table 6: Summary of flag changes recommended in .ctd (i.e. .wct) files. Note that for all cases shallower than 15 dbar, all data above the reflagged values was already flagged as 7 (i.e. despiked) - 7 flags were not changed.

| station | parameter | pressure | old flag | new flag |
|---------|-----------|----------|----------|----------|
| 45 | T | 9 | 2 | 3 |
| 49 | T | 8 to 11 | 2 | 3 |
| 61 | S | 5 | 2 | 3 |
| 63 | S | 6 to 10 | 2 | 3 |
| 126 | S | 11 | 2 | 3 |
| 126 | S | 12 to 13 | 6 | 3 |
| 146 | S | 6 | 2 | 3 |
| 159 | S | 8 to 9 | 2 | 3 |
| 160 | S | 11 | 6 | 3 |
| 13 | O | 5 | 2 | 3 |
| 19 | O | 7 | 2 | 3 |
| 25 | O | 8 | 2 | 3 |
| 27 | O | 55 to 57 | 2 | 3 |
| 52 | O | 11 | 2 | 3 |
| 63 | O | 11 | 2 | 3 |
| 119 | O | 12 | 2 | 3 |
| | | | | |

WOCE LEGS P14S AND P15S CTD STATION POSITIONS

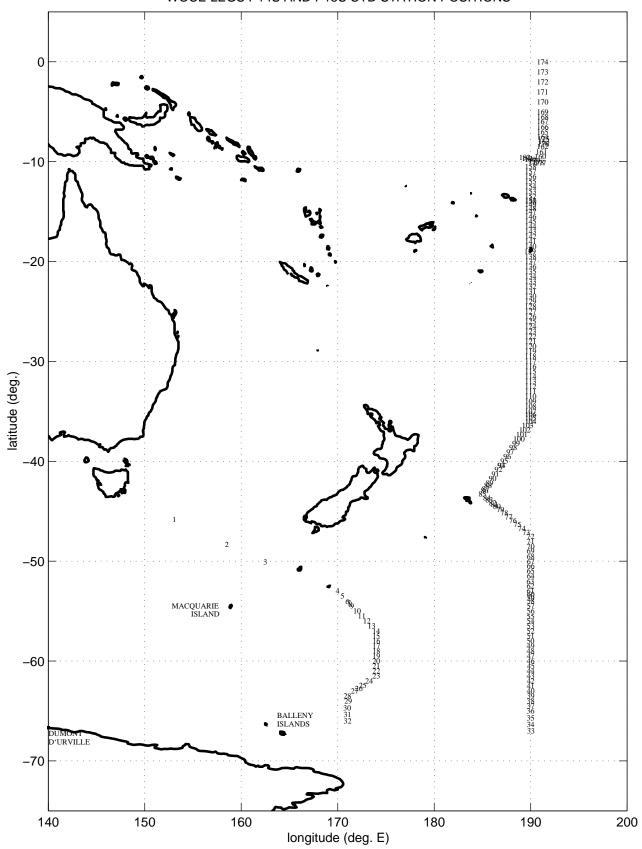


Figure 1

Figure 2

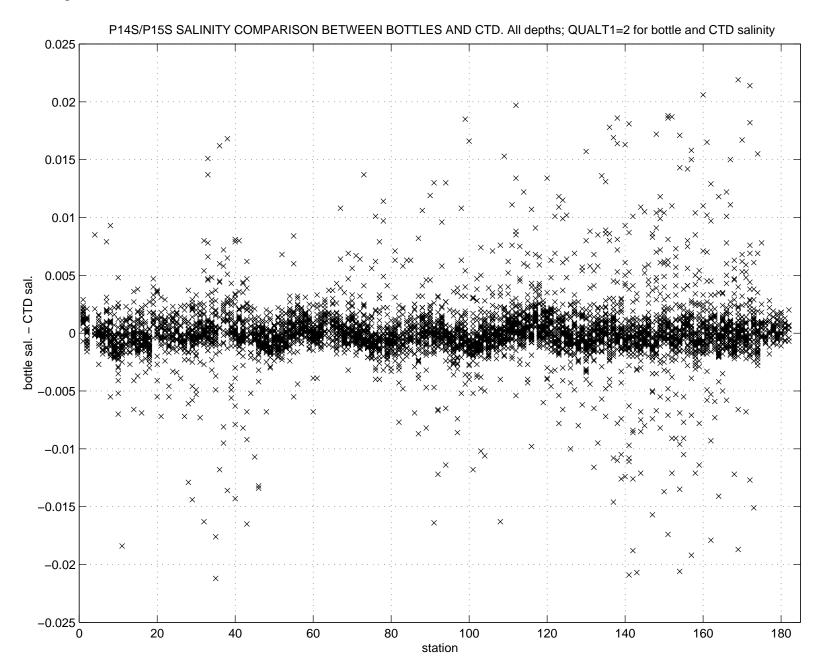
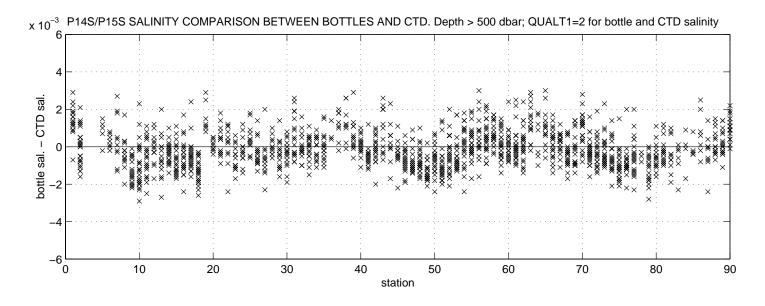


Figure 3



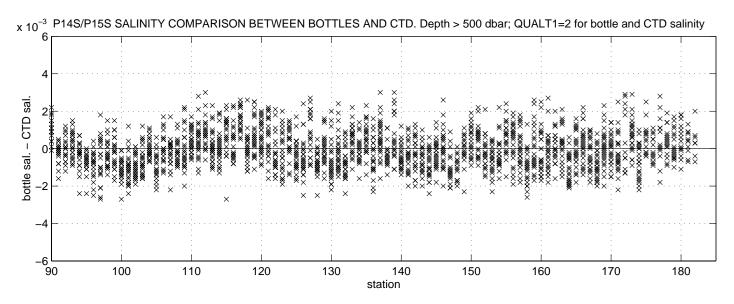
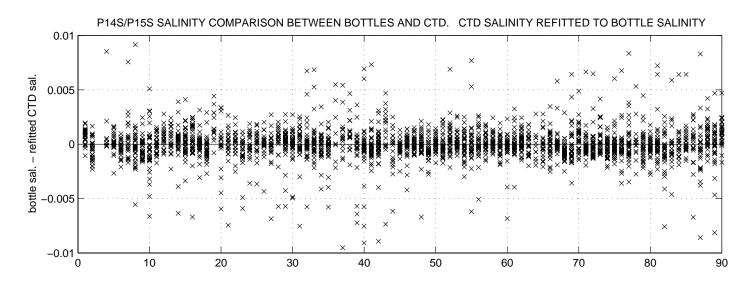


Figure 4: Corrected salinities



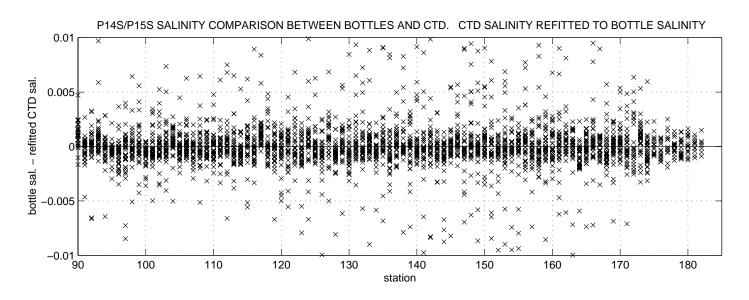
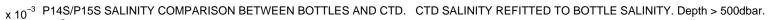
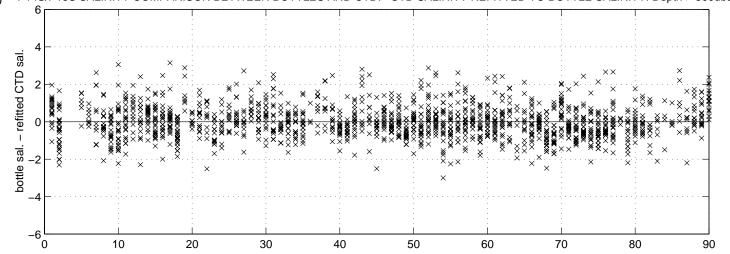


Figure 5: Corrected salinities







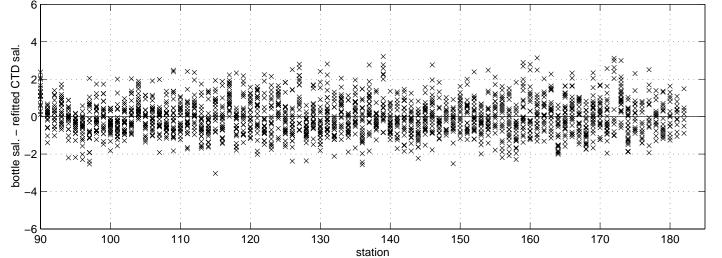
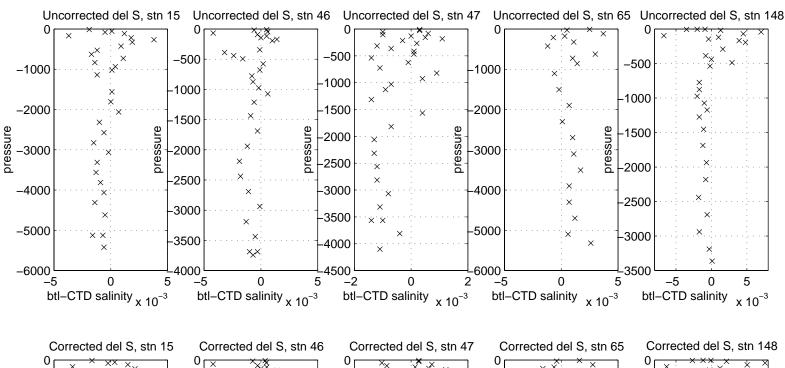


Figure 6



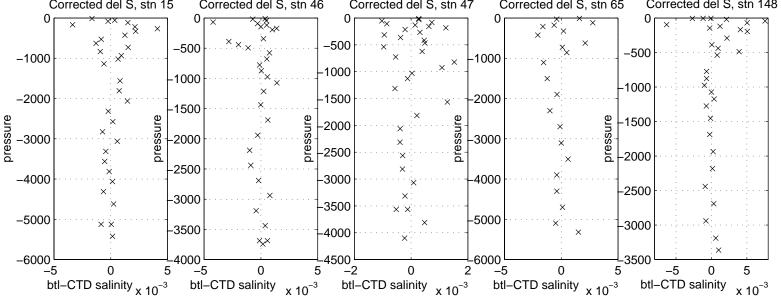
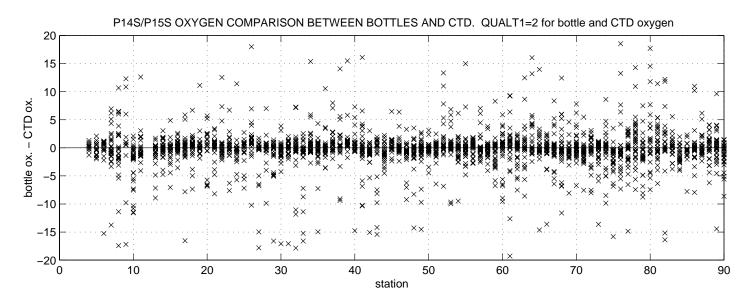
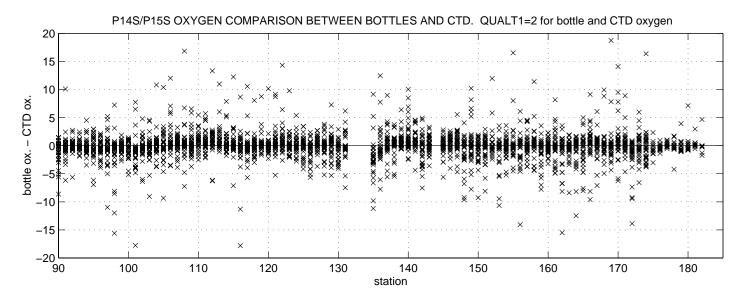
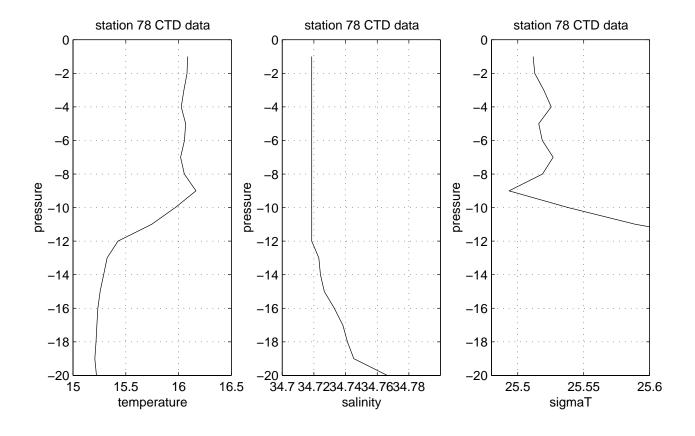


Figure 7







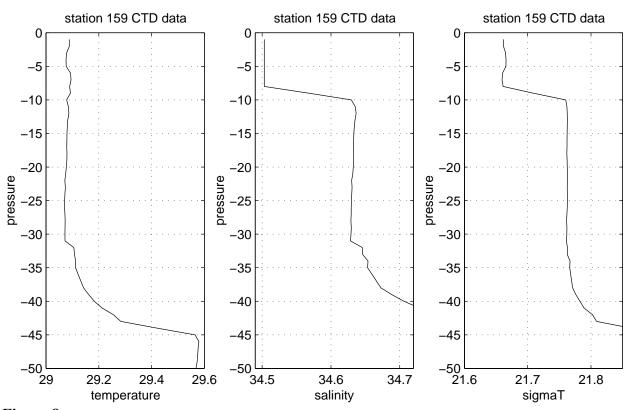
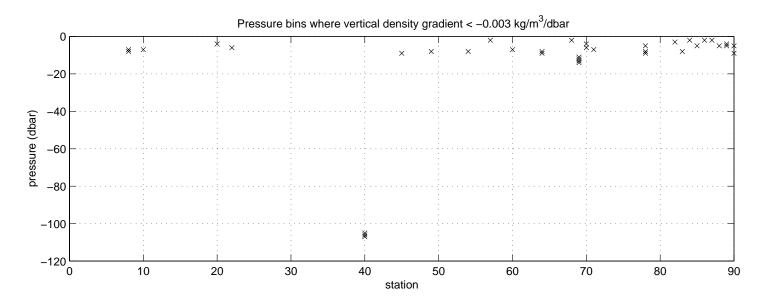


Figure 8

Figure 9



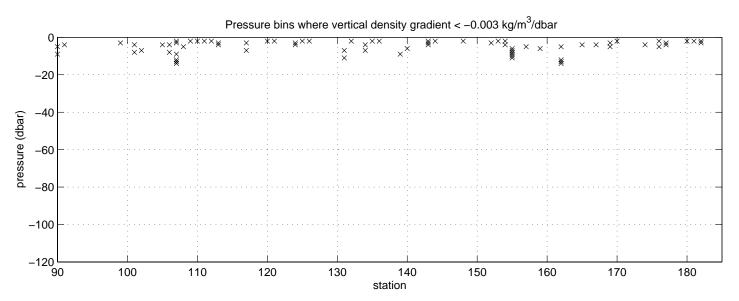


Figure 10: P15S and P15N comparison

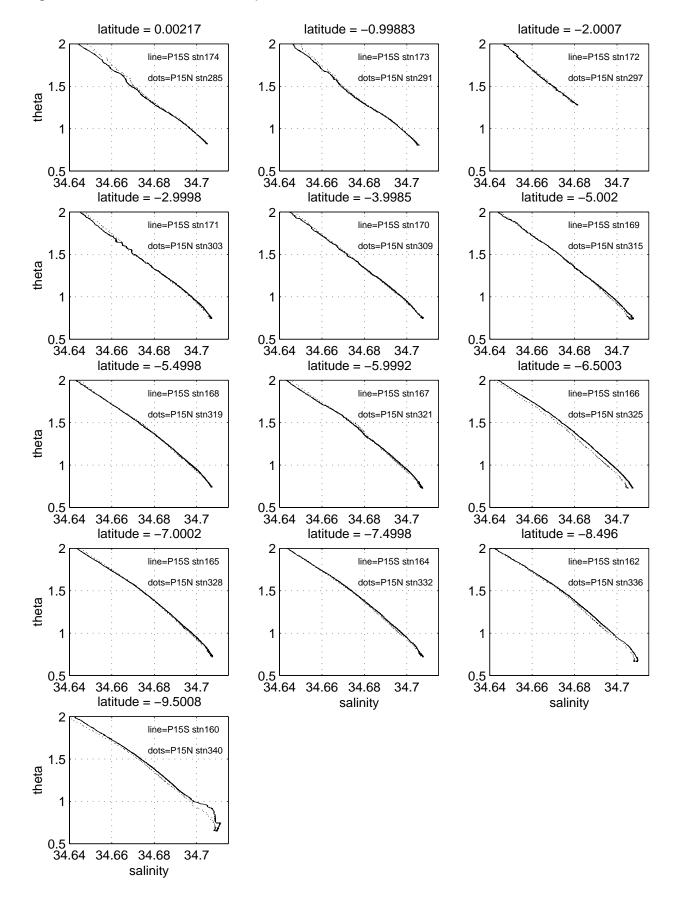


Figure 11: P15S and P31 comparison

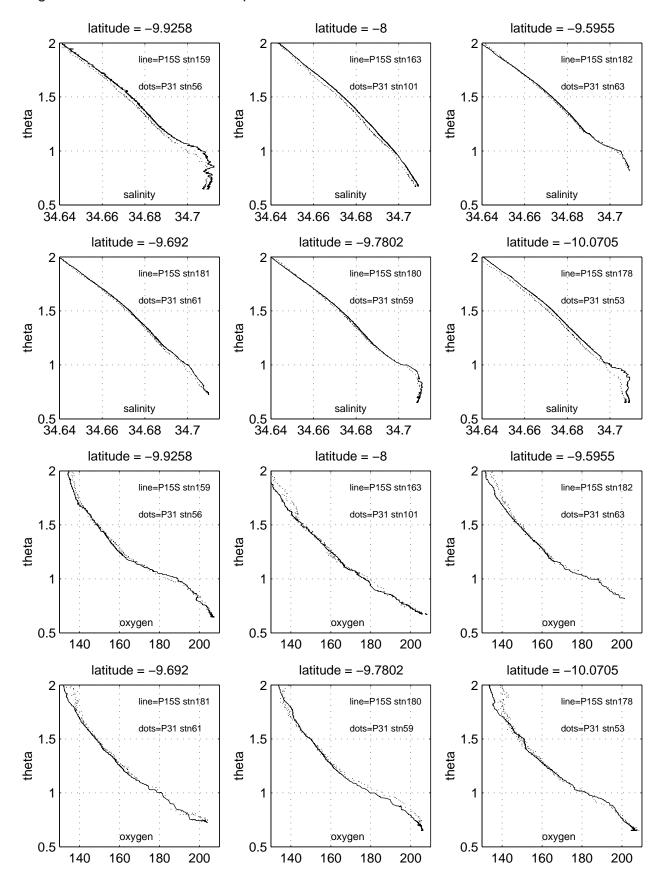
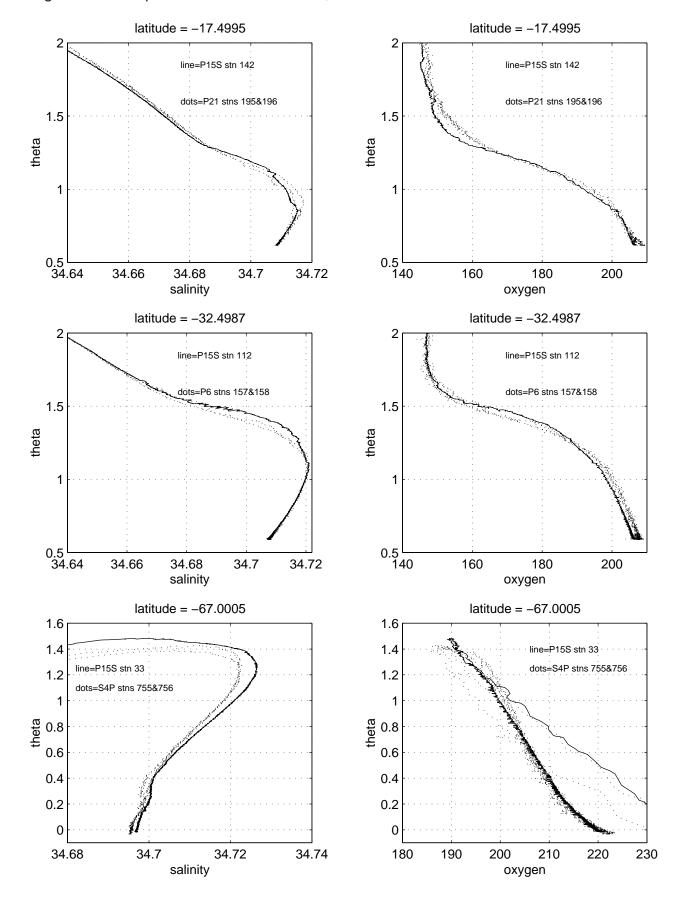


Figure 12: Comparison of P15S with P21, P6 and S4P



APPENDIX 10b: Response to DQE Evaluation of CTD data for RV Discoverer Cruise CGC96 (Kristy McTaggart and Greg Johnson)

We considered each of the suggestions and the following is an itemized explanation of what we did or didn't change in our data files, as well as answers to DQE's questions.

STATION SUMMARY FILE (.sum)

Stations 21 and 77 should be listed as cast 1. The .sum and .ctd files should be corrected. We've corrected our files here.

The uncorrected sounder depth at the bottom of the cast for stations 44 and 55 may appear erroneous. However, these are not typos. They are the values calculated from the ship's PDR during acquisition. The bottom at station 44 in particular was noted to be strongly sloping. We did not change these values in our files.

The PDR sound speed used for sounder readings was 1500 m/s. The readings were not corrected for transducer depth below the waterline. The depth of the transducer would've been about 5.5 +/- 0.6 m. We would prefer to use the PDR depths as listed and correct them using Carter's tables so that they serve as independent measurements and can be used as a check on CTD pressure.

SALINITY

'Scatter of salinity residuals'

There is an incompatibility between the General Oceanics rosette sampler and the Sea-Bird 911plus CTD system that generates a spike in the data stream at the moment a bottle is confirmed as tripped. Because of this, upcast CTD burst data had to be averaged prior to the bottle confirm bit. Two-second averages were chosen over a longer interval because the CTD operators did not always let the package sit at bottle depth for at least 10 seconds before firing the rosette. Hence no changes were made.

'Biasing of CTD salinity data for individual stations'

Of course one can seemingly make a (very slight) improvement in the CTD-bottle residual statistics by allowing more degrees of freedom in the fit as the DQE has suggested (that is, breaking up the fit into small station groupings). One could get the best statistics by individually fitting each station to its bottles, but most experts would argue that this would be a bad choice, because one would not be taking advantage of the CTD calibration as a way to average out station-to-station bottle salinity noise.

We believe that the SBE-9/11 CTD conductivity slope drifts gradually, and is actually more stable than the day-to-day fluctuations in the autosal- inometer salinities owing to small temperature drifts in the laboratory and the fact that severe budgetary constraints on these cruises forced us to economize even on such things as standard sea water. We suspect that the "biasing of the CTD salinity data" mentioned in the DQE evaluations is actually noise in the bottle data. Somewhat suspicious is that the station groupings recommended by the DQE of the correct size (most often 3-5 stations per group) that they could easily be

owing to daily drift problems in the autosalinometer. For our original calibrations we deliberately chose to model the conductivity slope adjustments of the entire data sets for P14S/P15S and P18 using 4th-order polynomial functions of station number to average out bottle salinity noise. We did this because we saw no obvious jumps in the CTD calibration for either cruise, just gradual drifts.

Statistical support for our philosophy over that of the DQE is given by the following exercise: The 2°C potential isotherm is well within the oldest Pacific Deep Water, and has some of the tightest Theta-S relation- ships in the Pacific Ocean (and probably the world). For both P18 and P14S/P15S, we looked at the absolute values of station-to-station changes in CTD salinity on Theta=2.0°C (Figure 1) for our original calibration, creating a histogram of station-to-station differences for each cruise in 0.001 bins. We then applied the DQE's suggested ad-hoc calibrations for smaller station groupings to the data and conducted the same analysis. When the histograms are differenced (Figure 2), one can see that the Theta-S relations at 2°C after the DQE's corrections are noisier for both cruises. For P18, after the DQE's suggested correction there are four less station pairs in the 0.000 difference bin and one less in the 0.001 difference bin whereas there are three more in the 0.002 difference bin and two more in the 0.003 difference bin. For P15S/P15S there are four less stations in the 0.000 difference bin after the DQE's suggested correction, with one more in the 0.001 difference bin and three more in the 0.002 difference bin. Since the DQE's "corrections" actually introduce more noise in the CTD Theta-S relation at 2°C than our original calibration, we decline application of them. The small groups do not improve the calibraiton, they degrade, perhaps by introducing autosalinometer drift noise.

Regarding suspicious CTD salinity data listed in Table 3, no changes were made to any profile data (see above) nor flags associated with "transient/ despiking errors". As for CTDSAL values in the .sea file for station 127, we agree that they should be flagged as 3 for samples 202 to 214. Also, BOTSAL flags for samples 209, 210, 213, and 214 should then be changed to 2.

'Problem salinity bottle data'

Excluding stations 19, 49, 117, and 164 bottle salinity values from the calibration of this data set as a whole would not significantly change the fit as we have done it, thus we didn't make this adjustment.

OXYGEN

Quality flags should be ammended as suggested in Table 4. However, stations 8, 10, and 135 will not be recalibrated individually as they are among the first casts with a new sensor module. As a rule, the first few casts with a new module are problematic, and this cruise was no exception.

TEMPERATURE

The very spikey temperature structure between 100 and 300 dbar at station 43 is also seen in salinity and has been identified as Antarctic Intermediate Water interleaving at the front. It is also seen at adjacent stations 42 and 44. Nothing should be done to this profile.

Temperature spikes listed were examined but not changed. Neither were their flags changed.

DESPIKING AND INTERPOLATION

Interpolated temperature and salinity data are the result of processing programs and not instrument or electronic problems. In program DESPIKE salinity profiles are viewed and interactively despiked using linear interpolation. Conductivity, theta, and sigma-theta are recomputed for the interpolated records. Only the salinity quality flag is ammended to 6. In program DELOOP Brunt-Vaisala Frequency squared (N^2) is computed at the mid depths and bracketed between two vectors, one padded with zeros at the surface and one padded with zeros at depth. If the first and second points of a -N^2 fail the criteria (<=-1e-05), then temperature and conductivity are linearly interpolated and salinity, theta, and sigma- theta are recomputed. The quantity of interpolated points is large because we were working with a large package off the stern of the ship, often in the Southern Ocean. Hence, there was a lot of wake problems.

As for the filled surface records flagged as 7, we maintain that this is more useful than leaving flagged bad or questionable data or removing the data entirely. It should be noted in the documentation that all data in the top 15 dbar with a flag of 7 should be regarded as questionable.

DENSITY INVERSIONS

Density inversions listed in Table 5 were examined and salinity quality flags were changed to '3' for the following records.

| Stn | Pressure | Stn | Pressure | Stn | Pressure | Stn | Pressure |
|-----|----------|-----|-------------|-----|----------|-----|----------|
| 8 | 5-7 | 85 | 4 | 113 | 1-3 | 152 | 1-2 |
| 10 | 1-7 | 86 | 1 | 117 | 1-6 | 153 | 1-2 |
| 20 | 1-3 | 87 | 1 | 120 | 1 | 154 | 1-3 |
| 22 | 1-5 | 88 | 3,4 | 121 | 1 | 155 | 1-15 |
| 45 | 1-8 | 89 | 3,4 | 124 | 1-3 | 157 | 1-4 |
| 49 | 1-7 | 90 | 4,8 | 125 | 1-3 | 159 | 1-6 |
| 54 | 7 | 91 | 1-4 | 126 | 1-13 | 160 | 1-12 |
| 57 | 1 | 99 | 1-2 | 131 | 3,5,6,10 | 162 | 1-13 |
| 60 | 5-6 | 101 | 1,3,7 | 132 | 1-9 | 165 | 1-3 |
| 64 | 7-8 | 102 | 6 | 134 | 1-3,6 | 167 | 1-3 |
| 68 | 1 | 105 | 1-3 | 135 | 1 | 169 | 1-7 |
| 69 | 1-14 | 107 | 1-2,8,11-13 | 136 | 1 | 170 | 1-3 |
| 70 | 3,5 | 106 | 1-3,6,7 | 139 | 8 | 174 | 1-3 |
| 71 | 6 | 108 | 4 | 140 | 4,5 | 176 | 1-4 |
| 78 | 1-9 | 109 | 1 | 143 | 1-3 | 177 | 1-3 |
| 82 | 1-4 | 110 | 1 | 144 | 1 | 180 | 1-3 |
| 83 | 7 | 111 | 1 | 146 | 1-6 | 181 | 1 |
| 84 | 1-2 | 112 | 1 | 148 | 1-3 | 182 | 1-2 |

DOCUMENTATION

Again, the PDR sound speed was 1500 m/s, and the readings have not been corrected for transducer depth (5.5 +/- 0.6 m) below the waterline.

The criteria used for despiking is explained above under DESPIKING AND INTERPOLATION.

APPENDIX 11: FINAL CFC DATA QUALITY EVALUATION (DQE) COMMENTS ON P14SP15S.

David Wisegarver (Dec 2000)

During the initial DQE review of the CFC data, a small number of samples were given QUALT2 flags which differed from the initial QUALT1 flags assigned by the PI. After discussion, the PI concurred with the DQE assigned flags and updated the QUAL1 flags for these samples.

The CFC concentrations have been adjusted to the SIO98 calibration Scale (Prinn et al. 2000) so that all of the Pacific WOCE CFC data will be on a common calibration scale.

For further information, comments or questions, please, contact the CFC PI for this section

(J. Bullister, johnb@pmel.noaa.gov) or David Wisegarver (wise@pmel.noaa.gov).

Additional information on WOCE CFC synthesis may be available at: http://www.pmel.noaa.gov/cfc.

Prinn, R. G., R. F. Weiss, P. J. Fraser, P. G. Simmonds, D. M. Cunnold, F. N. Alyea, S. O'Doherty, P. Salameh, B. R. Miller, J. Huang, R. H. J. Wang, D. E. Hartley, C. Harth, L. P. Steele, G. Sturrock, P. M. Midgley, and A. McCulloch, A history of chemically and radiatively important gases in air deduced from ALE/GAGE/AGAGE. Journal of Geophysical Research, 105, 17,751-17,792, 2000.

APPENDIX 12: Discrete fCO2 (fugacity of CO2) measurements during CGC-96

Principal Investigator: Rik Wanninkhof (Wanninkhof@aoml.noaa.gov)

Analysts: Dana Greeley and Hua Chen

Note: all data is fCO2 data but labeled as pCO2

Approximately 2900 discrete fCO2 samples from 168 station were taken and analyzed on the cruise using an analysis system based on gas chromatography (Neill et al., 1997). The measurement was performed by equilibrating 10-mL headspace with 120-mL seawater sample at 20 C in a bottle with crimp seal and Teflon lined cap. The headspace was injected into a gas chromatographic column that separates CO2 from the other gases in the headspace. The CO2 is subsequently quantitatively converted to methane using a ruthenium catalyst. The methane is measured at high sensitivity with a flame ionization detector.

The data obtained from the cruise has an uncertainty proportional to the gas concentration in contrast to our previous system that was based on infrared analysis using larger samples (Wanninkhof and Thoning, 1993). The current system has slightly worse precision for surface water samples but better precision for samples with high pCO2. During leg 1, 38 duplicate samples had a precision of 0.9 % (1- st. dev.); during leg 2, 41 duplicates yielded a precision of 1%.

The quality control steps were as follows. All samples that had sampling irregularities such as leakage, detachment of the sample bottle from the intake line etc. were flagged as questionable during analysis on the cruise. During data reduction the following checks were performed:

- (1) Plotting fCO2 against depth
- (2) Plotting fCO2 against DIC
- (3) Plotting fCO2 against pH
- (4) Performing internal consistency calculations using the Lewis and Wallace (1998) program and calculating TA(TC,fCO2) and TA(TC,pH) and {TA(meas)- TA(TC,pH)}. These differences were then plotted for four consecutive stations against depth.

Based on these comparisons a subjective assessment was made as to the quality of the data and quality control flags were adjusted as deemed proper.

References:

- Lewis, E., and D.W.R. Wallace, Program developed for CO2 system calculations, Oak Ridge National Laboratory, Oak Ridge, 1998.
- Neill, C., K.M. Johnson, E. Lewis, and D.W.R. Wallace, Small volume, batch equilibration measurement of fCO2 in discrete water samples., Limnol. Oceanogr., 42, 1774-1783, 1997.
- Wanninkhof, R., and K. Thoning, Measurement of fugacity of CO2 in surface water using continuous and discrete sampling methods, Mar. Chem., 44 (2-4), 189-205, 1993.

| | Data Processing Notes |
|----------|--|
| Date | Contact Data Type Data Status Summary |
| 05/06/98 | Bullister SUM/SEA/DOC Submitted for DQE P14S & P15S data is combined |
| 10/06/98 | Anderson CTD/BTL/SUM Reformatted by WHPO Reformatted .sum file: Changed EXPOCODE from 31DICG96/1 to 31DSCG96_1 and |
| | 31DICG96/2 to 31DSCG96_2. |
| | Ran over sumchk, no problemssea file ok except for first header. |
| | Changed EXPCODE to EXPOCODE. Changed 31DICG96/1 to 31DSCG96_1 and 31DSCG96_2 to 31DSCG96_2. |
| | Reordered pressures so they are shallowest to deepest. |
| | For stas. 21 and 77 .sum file had only cast 2, .sea file had only cast 1. I don't know which i correct so I did not change. |
| | Ran over wocecvt, only problem above mentioned cast number discrepancies. |
| | CTD - ctd data was ok except for EXPOCODE. Changed from 31DICG96/1 and 31DSCG96_2 to 31DSCG96_1 and 31DSCG96_2. |
| | Dates in .sum and .wct files for sta/cast 13/1, 16/1, 29/2, 32/1, 39/1, 43/1, 52/1, 74/2, 89/2 110/2, 121/2, 128/2, 135/2, 167/2, 173/2, and 175/2 do not agree. In all cases the BE time is before midnight and the BO time is after midnight so the day is different. The originator used the BE dates for the ctd's. I did not change the .wct files. |
| 10/15/98 | Mantyla NUTs/S/O DQE Begun |
| 10/15/98 | Rosenberg CTD DQE Begun at WHPO/SIO |
| 11/16/98 | Rosenberg CTD DQE Report rcvd @ WHPO |
| 11/18/98 | Rosenberg CTD DQE Report sent to PI |
| 11/18/98 | Mantyla NUTs/S/O DQE Report rcvd @ WHPO |
| 01/11/99 | Bullister CTD/BTL*/CFC Data are Public NUTs, S/O, c14 collected and sent to AMS/WHOI. Checking w/ Quay re c14 data status |
| 01/11/99 | Johnson CTD/S/O DQE Report sent to PI ctdoxy is public, all else in nonpublic |
| 04/29/99 | Quay DELC13 Data and/or Status info Requested by dmb |
| 07/15/99 | Johnson CTD/HYD DQE Reports rcvd by PI Kristy will be mailing you our responses to both reports (and submitting some revised data shortly. Please don't make any changes to the CTD data for these cruises until you have our replies in hand. |
| 08/17/99 | Anderson SUM/HYD Data Update |
| | p14ssu.txt: Reformatted to conform with the WHPO standard .sum format. Mostly adding and/or deleting spaces. p14shy.txt: |
| | Reordered pressures that were not in descending order. Changed station 21 cast 1 to cast 2 to conform with the |
| | sum file: Changed station 77 cast 1 to cast 2 to conform with the .sum file. |
| | Ran over wocecvt and sumchk without any errors. Diggs SUM/HVD Website Undated |

Diggs SUM/HYD Website Updated SUM and HYD files are now out on the website, and all tables have been updated. 03/20/00

04/19/00 Bartolacci DELC14 Website Updated: no samples collected

However I'd like to clarify this with you, because the DOC file that we have indicates that some 900 or so samples were taken for both C14 and C113, did they not get processed? (There are columns in the data file for both of these parameters that will need to be edited out.) When I first started working for Lynne on the atlas I emailed Paul Quay about this but never got a reply.

04/20/00 Key DELC14 No Data Submitted See note:

P14S15S is problematic. Paul did collect samples which could have been used for C-13 and C-14. I'm pretty sure that many of the C-13 samples have been analyzed. Unfortunately, in his proposal, Paul did not request funding for C-14 analysis. Paul saved an aliquot of the extracted CO2 gas which can be analyzed for C-14 if we can get the funds. We plan on submitting a proposal which, if funded, will cover C-14 analysis costs on a few cruises including:

P14S15S

EqPac (Fall and Spring; NOAA) P1 (Japanese E-W transect) Unnamed German cruise in the upwelling region west of S. Am.

06/13/00 Bullister BTL/SUM/DOC Final Data Rcvd @ WHPO

DQE-related and other updates. See note: I just re-sent p14sp15s .sea, .sum and .doc files to the WHPO ftp site.

The file names are:

p14sp15s.doc.senttoWHPO12jun2000

p14sp15s.sea.senttoWHPO12jun2000

p14sp15s.sum.senttoWHPO12jun2000

These files have a number of updates compared to the 'p14s' files now posted at the WHPO web site. Please note that the data in these files (and in the old 'p14s' posted at the WHPO web site) are for both p14s AND p15s- both sections were done on the same expedition.

The .sea file now ncludes tcarbn, alkali and pH data; the CFC data are reported on the SI093 calibration scale.

We have incorporated most of the changes recommended in A. Mantyla's DQE recommendations. Details of these changes are included at the end of the p14sp15s.doc file sent to WHPO 12 jun 2000.

PS: Please note that the formatting instructions given for delc13 in the WHPO 90-1 manual posted at the WHPO web site still ask for F8.1. This should be F8.2. A lot of the value of the delc13 data is lost if they are only reported to 1 decimal precision.

06/17/00 Bartolacci BTL/SUM/DOC Website Updated files added to website

I have updated the current sumfile and doc file for this cruise as well as the bottle file.

The new bottle file contains:

CTDRAW CTDPRS CTDTMP CTDSAL CTDOXY THETA **OXYGEN** SALNTY SILCAT **NITRAT NITRIT PHSPHT** CFC-11 CFC-12 DELC14 DELC13 C14ERR C13ERR TCARBN **ALKALI** PCO₂ PCO2TMP PH **PHTEMP**

There is no data in the columns for DELC14, DELC13 C14ERR, C13ERR, PCO2TMP and PHTEMP

06/20/00 Bartolacci BTL/SUM Website Updated; See note:

I have replaced the summary, bottle and added an additional documentation file. All entries and references to this line have been updated. Columns for DELC14/13 and C14ER/C13ER PCO2TMP and PHTMP are filled with missing data values. Bullister has been notified via email that the above changes have been made.

| 0010:::: | |
|----------|--|
| 06/24/00 | Bullister PCO2 Submitted; Need to be merged into BTL file; See note: I just received a revised pCO2 data file for the P14SP15S cruise, along with a short description of the analytical methods used, all from the PI (Rik Wanninkhof; wanninkhof@aoml.noaa.gov) |
| | I just put 2 files at the WHPO INCOMING ftp site: p14sp15spco2.dat p14sp15spco2.txt |
| | Could you please merge the pco2 data into the p14sp15shy.txt file at your site, and include the text of p14sp15spco2.txt in the cruise documentation file? |
| 07/05/00 | McNichol DELC13 Submitted csv for p15s leg only I have just uploaded three files p15sbmt2.csv, p15submt.des, and p13submt.des to your ftp site. The csv file contains the following fields in a comma-delimited file: LabID, Trackline, Station, cast, niskin, del13C, QC The LabID is to distinguish between the two laboratories where the majority of the measurements were madeUniversity of Washington and NOSAMS, WHOI. |
| | The files labelled des describe the samples flagged with a "6" in greater detail. Can you accept these as well? |
| | Paul Quay and I would like to append a statement *somewhere* indicating the status of our laboratory data comparisons. Do you have an appropriate place for this? |
| 09/29/00 | McNichol DELC13 Data are Public; See Note: All the Pacific data (most of which I still need to send you) is public. I should be sending you a pile of data next month. |
| | Also, if the future, if you have a question that you need answered immediately, the best person to get in contact with besides me is Dana Stuart. Her contact info is dstuart@whoi.edu |
| 11/21/00 | Uribe DOC Submitted See Note: 2000.11.21 KJU File contained here is CRUISE SUMMARIES and NOT sumfiles. Files listed below should be considered WHP DOC files. Documention is online. |
| | 2000.10.11 KJU Files were found in incoming directory under whp_reports. This directory was zipped, files were separated and placed under proper cruise. All of them are sumfiles. Received 1997 August 15th. |
| 03/15/01 | Key DELC14 Measured as per .DOC Funding now available to analyze Got word from Eric this A.M. that he will fund NOSAMS at the rate of 1000/year to analyze previously collected, but unfunded C14 samples. Highest priority will be to fill in Pacific "holes" starting with P14S15S (NOAA), P15N (Wong) and P1 (Japan). Policy decision supported by WOCE SSC. Eric would, if possible, like these data to be included in the atlas. In reality I don't know if this is possible/practical, but I will do everything possible to expedite. Scheduling at NOSAMS will be complicated, but order listed above is the "scientific" priority as of now. |
| 06/22/01 | Uribe CTD/BTL Website Updated; CSV File Added CTD and Bottle files in exchange format have been put online. |

10/01/01 Muus CFC/BTL/SUM Data Merged into BTL file

CFCs merged into BTL (July), SUM file modified, CSV file updated 2001 CFCs into bottle file, modified SUM file WOCE SECT column to allow conversion to exchange format, made new exchange file and place all on web.

Notes on P14S CFC merging Sept 26, 2001.

D. Muus

1. New CFC-11 and CFC-12 from:

/usr/export/html-public/data/onetime/pacific/p14/p14s/original/20010709_CFC_UPDT_WISEGARVER_P14SP15S/20010709.173406_WISEGARVER_P14SP15S/20010709.173406_WISEGARVER_P14SP15S_p14s_ CFC_DQE.dat merged into SEA file taken from web Sept 26, 2001 (20000616SIOWHPODMB)

Most "1"s in QUALT1 changed to "9"s and QUALT2 replaced by new QUALT1 prior to merging. CTDOXY has values for Stations 1 through 3 but QUALT1 code is "1". Bottle oxygens taken on Station 1 and from Station 4 on. No bottle oxygens on Stations 2 and 3. QUALT1 code for CTDOXY is "2" from Station 4 on. Left "1"s as quality codes for Station 1 - 3 CTDOXY as caution to users.

- Conversion from woce bottle format to exchange format failed using the web SUMMARY file (20000616SIOWHPODMB). Modified SUM file by replacing blanks in WOCE SECT columns for Stations 1 - 3 with "x"s. Moved WOCE SECT header so column is left justified. Conversion to exchange file worked after these modifications made.
- 3. Exchange file checked using Java Ocean Atlas.

01/22/02 Uribe CTD Website Updated CSV File Added; see note:
CTD has been converted to exchange using the new code and put online. Files for station 21 and 77 has a mismatch in the cast number in the sumfile. The sumfile contained data for a cast 1 but the CTD files said cast 2 so the CTD files were modified for the purpose of the conversion.

06/21/02 Kappa Doc PDF & TXT files updted, new sections added:

New sections include a CTD cast summary and CTD oxygen algorithm parameters tables, HYD DQE report, CTD DQE report, PI response to CTD DQE report, CFC DQE report, Report on CO2fugacity Measurements, and WHPO data processing notes.

PDF Cruise Report includes all the above, plus figures and internal links between figures and table of contents and relevant text.