

Microstructure Mechanics

Crystal Mechanics

Dierk Raabe

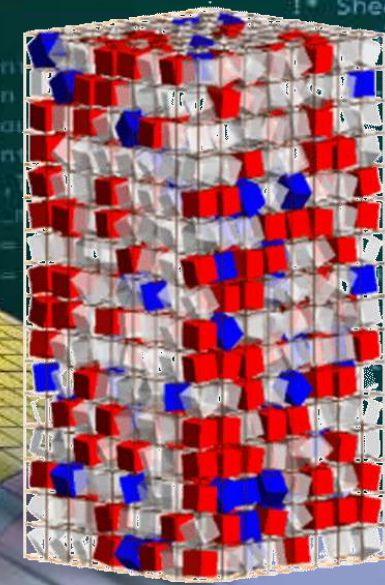
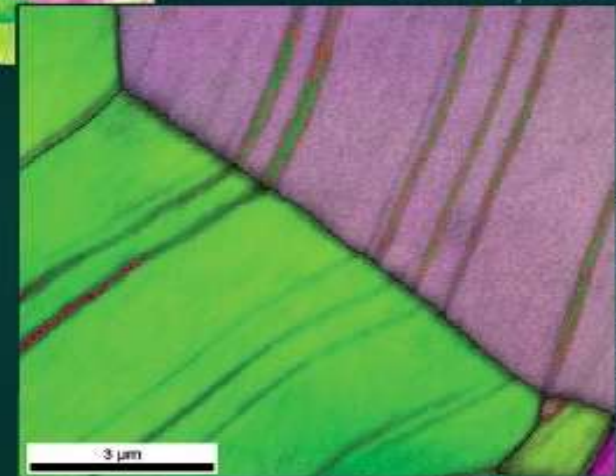
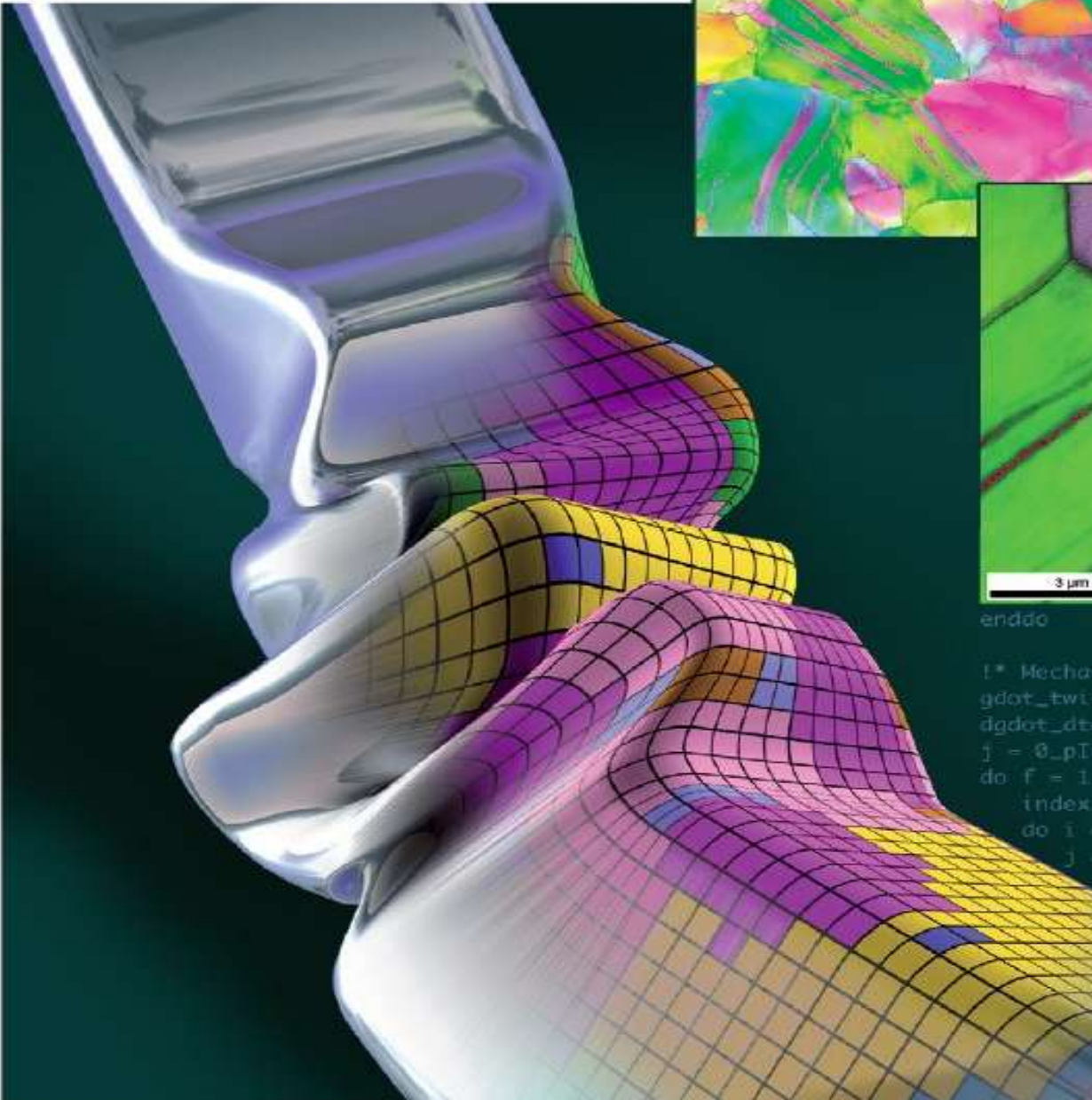


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```

Gamma0 = & !* Dislocation glide part
tate(g,lp,e,gdot_slip = 0.0_pReal
constitutive,dgdot_dtauslip = 0.0_pReal
j = 0_pInt
Shear rates do f = 1,lattice_maxNslipFamily
t_slip(j) = 0;index_myFamily = sum(lattice
do i = 1,constitutive_dislotwin

on of Lp
shear stress
= dot_product

tios
p = (abs(tau
pminus1 = (ab
ratio
io = constit
hear rates
&
,el)%p(j)*con
ve_dislotwin

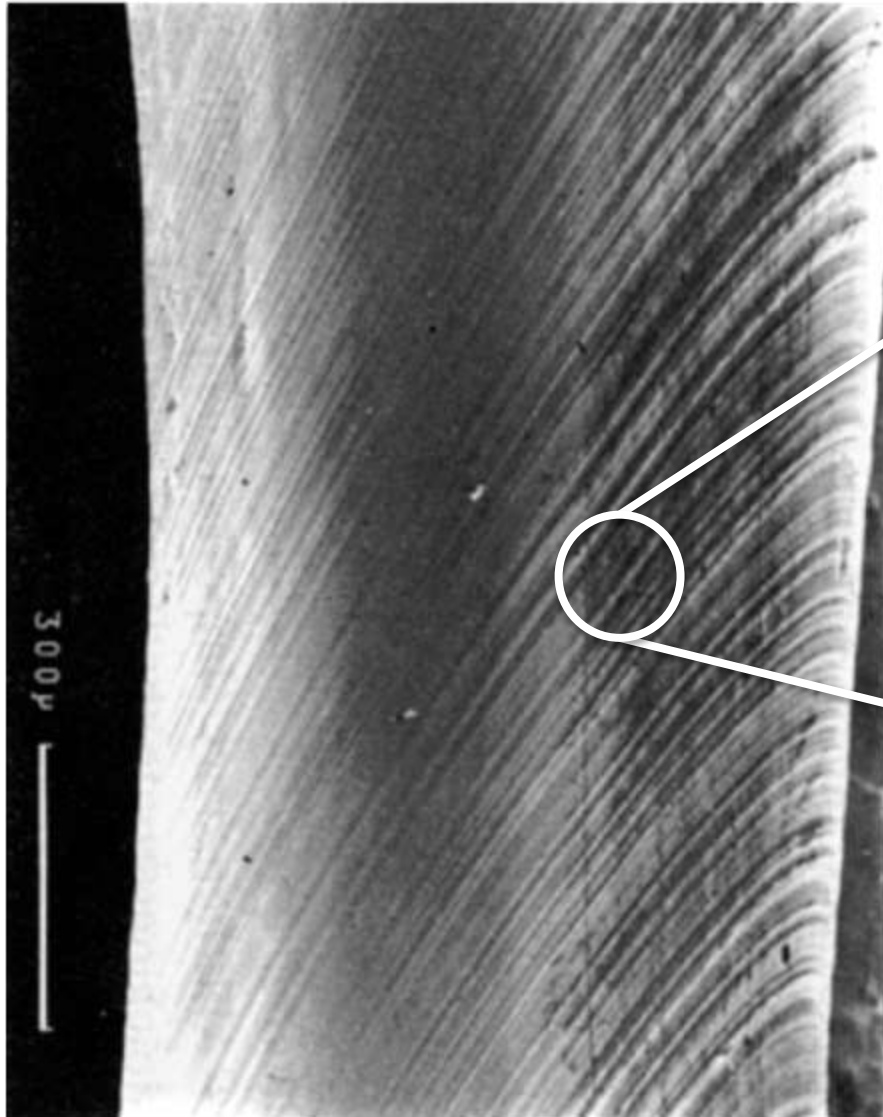
enddo

!* Shear rates due to slip
slip(j) = DotGamma0

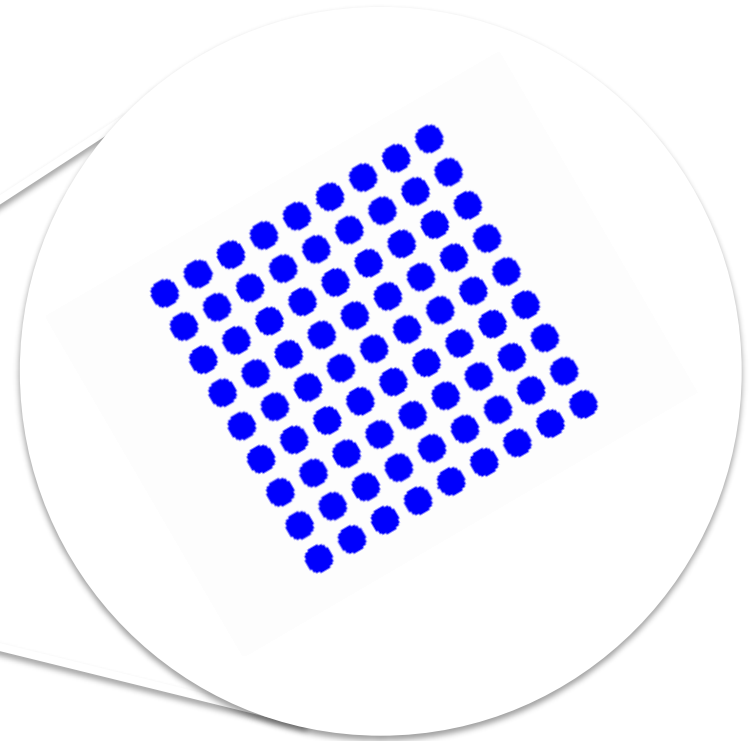
ivatives of shear r
dtauslip(j) = &
s(gdot_slip(j))*Bot
stitutive_dislotwin
ssRatio_pminus1*(1
stic velocity gradi
p + (1.0_pReal - su
ulation of the tar
(k=1:3,l=1:3,m=1:3
dTstar3333(k,l,m,n)
dTstar3333(k,l,m,n)

```

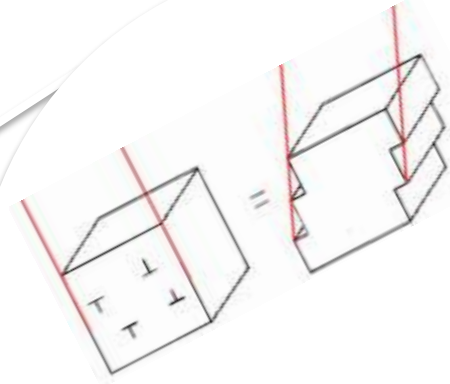
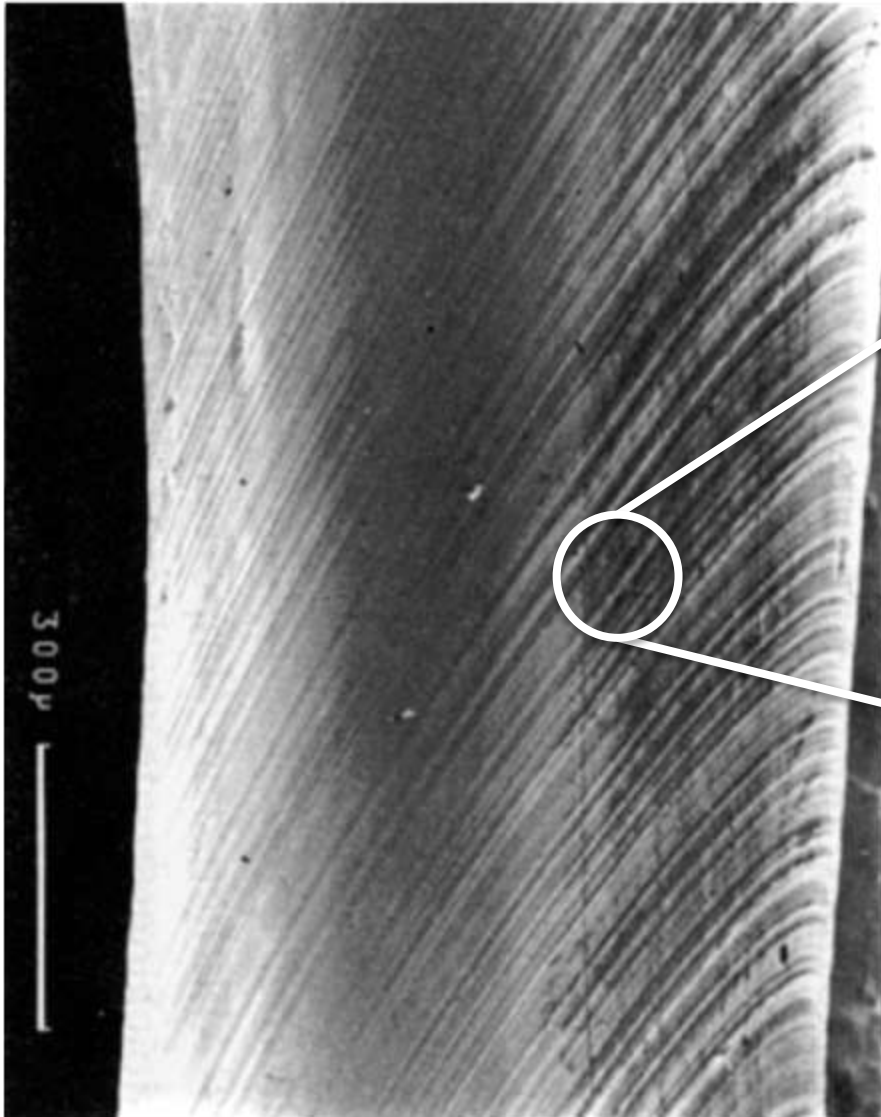
- **Displacements and rotations in crystals**
- **Single crystal yield surface**
- **Taylor model for the mechanics of polycrystals**
- **Examples**



single slip in a single crystal



plastic anisotropy



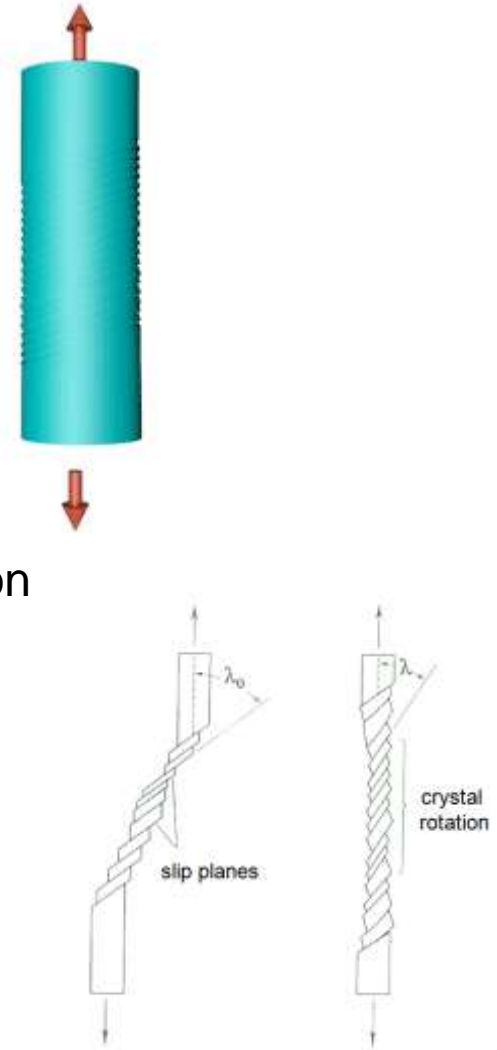
$$\dot{\gamma} = \frac{d\gamma}{dt} = n \frac{dx}{X} \frac{b}{Z} \frac{1}{dt} = \rho_m b v$$

Constraints lead to specific crystal rotations

Non-symmetric dislocation shear leads to rotation

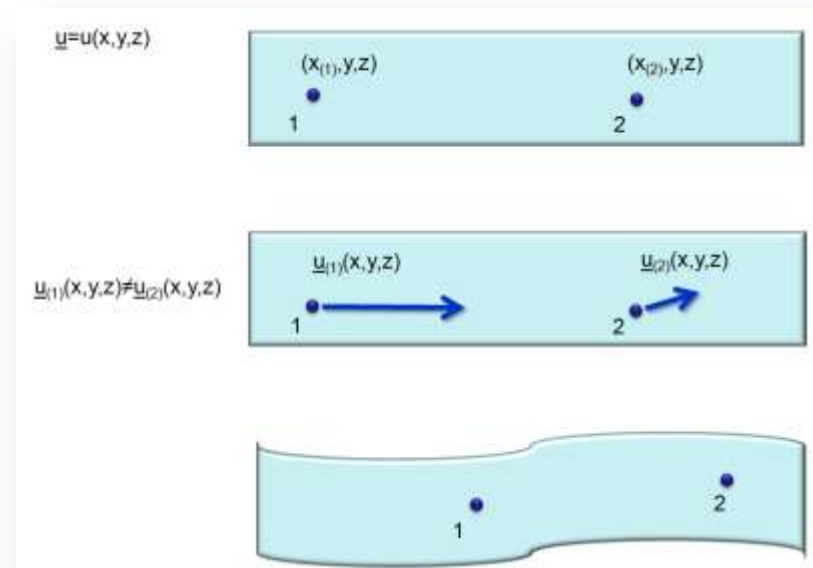
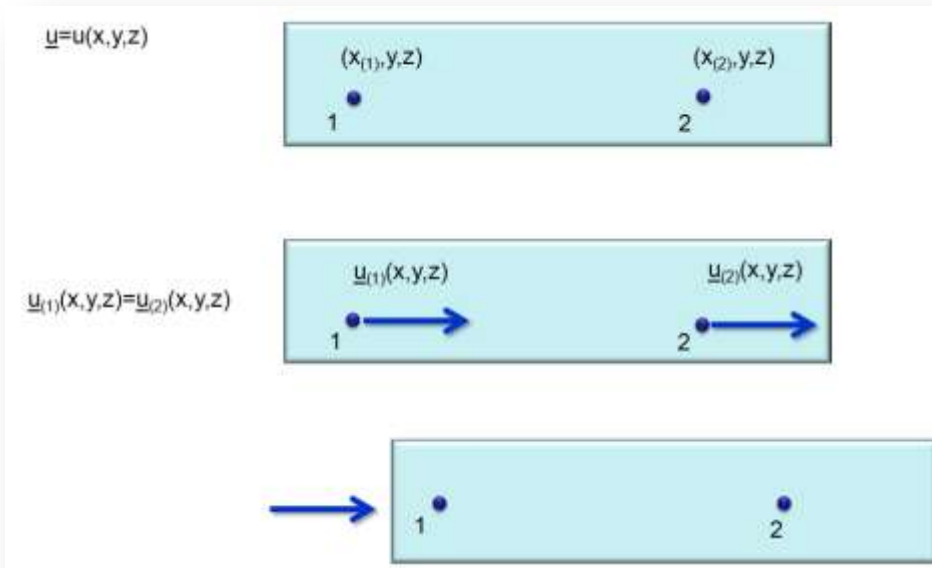
Symmetric-shear can lead to shape change without rotation

Change in local constraints leads to heterogeneity



strain rates and displacement gradients in crystals

$$\dot{\epsilon}_{ij}^K = D_{ij}^K = \frac{1}{2}(\dot{u}_{i,j}^K + \dot{u}_{j,i}^K) = \sum_{s=1}^N m_{ij}^{\text{sym},s} \dot{\gamma}^s \quad \text{mit} \quad m_{ij}^{\text{sym}} = m_{ji}^{\text{sym}} = \frac{1}{2}(n_i b_j + n_j b_i)$$



slip system s

$$n_i^s, b_i^s$$

orientation factor for s

$$m_{ij}^s = n_i^s b_j^s$$

symmetric part

$$m_{ij}^{\text{sym},s} = \frac{1}{2} (n_i^s b_j^s + n_j^s b_i^s)$$

rotate crystal into sample

$$m_{kl}^s = a_{ki}^c n_i^s a_{lj}^c b_j^s$$

symmetric part

$$m_{kl}^{\text{sym},s} = \frac{1}{2} (a_{ki}^c n_i^s a_{lj}^c b_j^s + a_{lj}^c n_j^s a_{ki}^c b_i^s)$$

yield surface

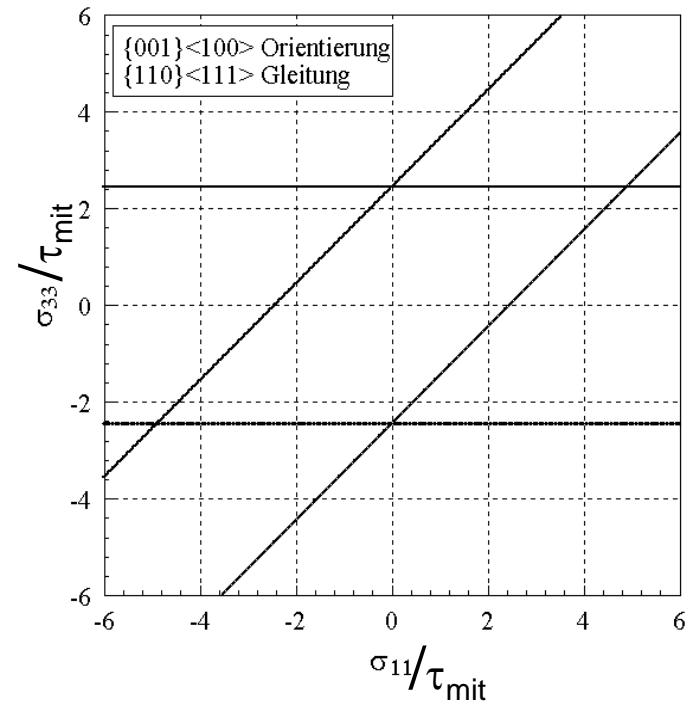
(active systems)

$$m_{kl}^{\text{sym},s=\text{aktiv}} \sigma_{kl} = \sigma_{\text{aufg}}^s = \tau_{\text{krit},(+)}^{s=\text{aktiv}}$$

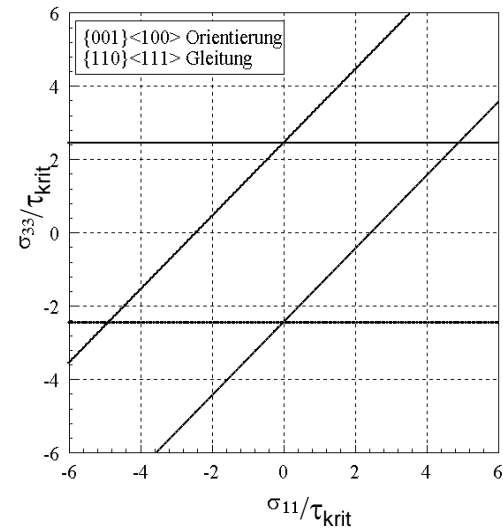
$$m_{kl}^{\text{sym},s=\text{aktiv}} \sigma_{kl} = \sigma_{\text{aufg}}^s = \tau_{\text{krit},(-)}^{s=\text{aktiv}}$$

(non-active systems)

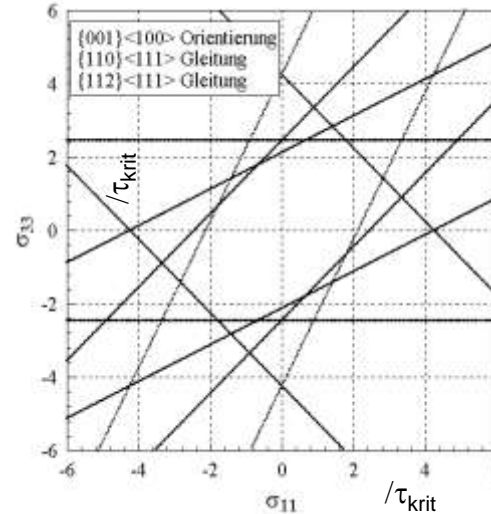
$$m_{kl}^{\text{sym},s=\text{inaktiv}} \sigma_{kl} = \sigma_{\text{aufg}}^s < \tau_{\text{krit},(\pm)}^{s=\text{inaktiv}}$$



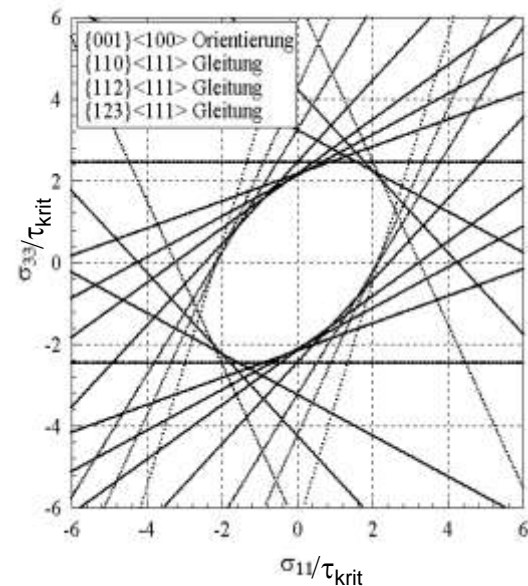
Single crystal plasticity: constructing the yield surface



FCC, BCC
12 systems
section



BCC
24 systems
section



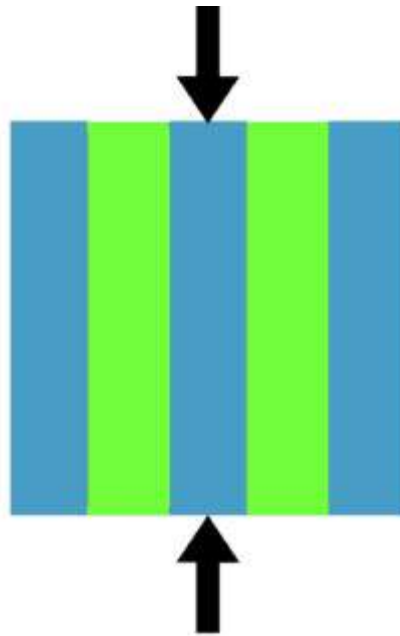
BCC
48 systems
section

YIELD SURFACE, BCC

SINGLE CRYSTAL, BCC, (001)[100]

- How does that work for bicrystals ?
- Two extreme cases :
- iso-strain (Taylor)
- iso-stress (Schmid)

Iso-stress and iso-strain



Isostrain

$$\varepsilon = \varepsilon_s = \varepsilon_d$$

$$\sigma = \sigma_s + \sigma_d$$

Displacement continuity
across layers



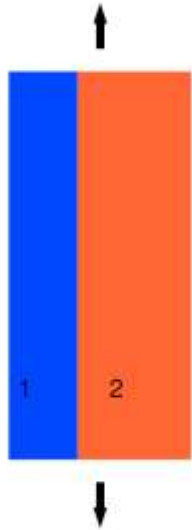
Isostress

$$\varepsilon = \varepsilon_s + \varepsilon_d$$

$$\sigma = \sigma_s = \sigma_d$$

Stress continuity
across layers

Bounding Case - Isostrain



$$\epsilon_1 = \epsilon_2 = \epsilon_{tot}$$

$$\sigma_1 = E_1 \epsilon_1 = E_1 \epsilon_{tot} \quad ; \quad \sigma_2 = E_2 \epsilon_2 = E_2 \epsilon_{tot}$$

$$P_1 = A_1 \sigma_1 = A_1 E_1 \epsilon_{tot} \quad ; \quad P_2 = A_2 \sigma_2 = A_2 E_2 \epsilon_{tot}$$

$$P_{tot} = P_1 + P_2 = \epsilon_{tot} (A_1 E_1 + A_2 E_2)$$

$$\sigma_{tot} = \frac{P_{tot}}{A_1 + A_2} = \epsilon_{tot} \left(\frac{A_1}{A_1 + A_2} E_1 + \frac{A_2}{A_1 + A_2} E_2 \right)$$

$$\sigma_{tot} = (f_1 E_1 + f_2 E_2) \epsilon_{tot}$$

$$E_{tot} = f_1 E_1 + f_2 E_2$$

P_1, P_2 are the loads on 1 and 2.

f_1, f_2 are the volume fractions of 1 and 2.

Bounding Case - Isostress



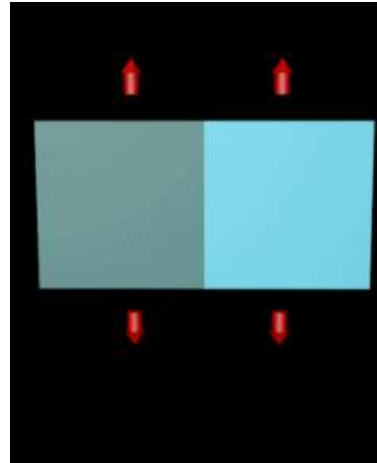
$$\sigma_1 = \sigma_2 = \sigma_{tot}$$

$$\sigma_1 = E_1 \epsilon_1 \quad ; \quad \sigma_2 = E_2 \epsilon_2$$

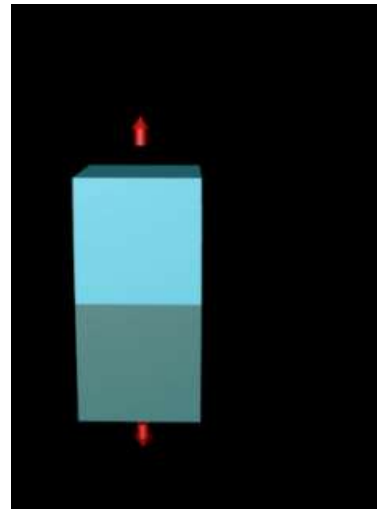
$$\epsilon_{tot} = f_1 \epsilon_1 + f_2 \epsilon_2 = f_1 \frac{\sigma_{tot}}{E_1} + f_2 \frac{\sigma_{tot}}{E_2}$$

$$E = \frac{\sigma_{tot}}{\epsilon_{tot}} = \frac{1}{\frac{f_1}{E_1} + \frac{f_2}{E_2}} = \frac{E_1 E_2}{f_1 E_2 + f_2 E_1}$$

- iso-strain (Taylor-model)



- iso-stress (Sachs-model)



Sachs Model (previous lecture on single crystal):

- All grains with aggregate or polycrystal experience the same state of stress;
- Equilibrium condition across the grain boundaries satisfied;
- Compatibility conditions between the grains violated, thus, finite strains will lead to gaps and overlaps between grains;
- Generally most successful for single crystal deformation with *stress boundary conditions on each grain*.



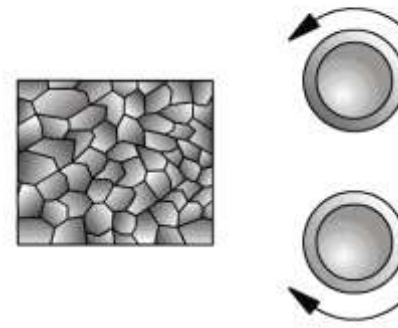
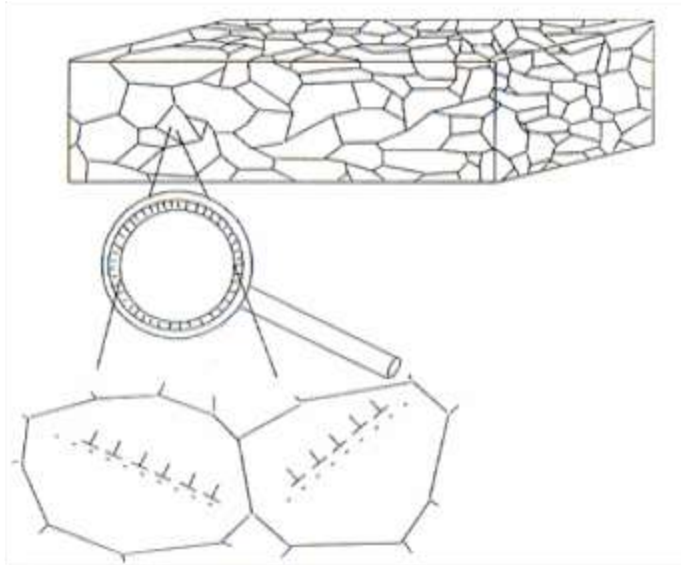
Taylor Model (this lecture):

- All single-crystal grains within the aggregate experience the same state of deformation (strain);
- Equilibrium condition across the grain boundaries violated, because the vertex stress states required to activate multiple slip in each grain vary from grain to grain;
- Compatibility conditions between the grains satisfied;
- Generally most successful for polycrystals with strain boundary conditions on each grain.



- Taylor model for the mechanics of polycrystals

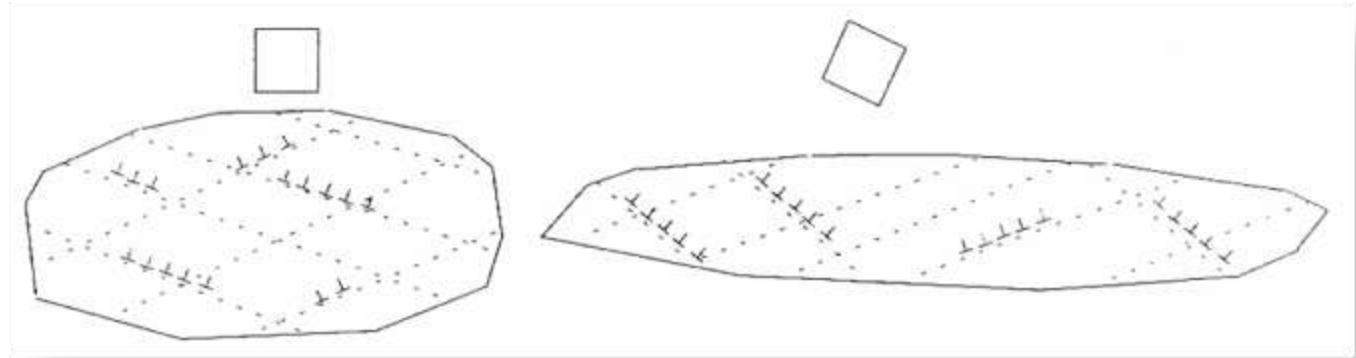
The Taylor Model



Cold Rolling

$$\epsilon_{ij} = \frac{1}{2} \sum_{s=1}^5 (n_i^s b_j^s + n_j^s b_i^s) \gamma^s$$

$$\varepsilon_{ij} = \frac{1}{2} \sum_{s=1}^5 (n_i^s b_j^s + n_j^s b_i^s) \gamma^s$$

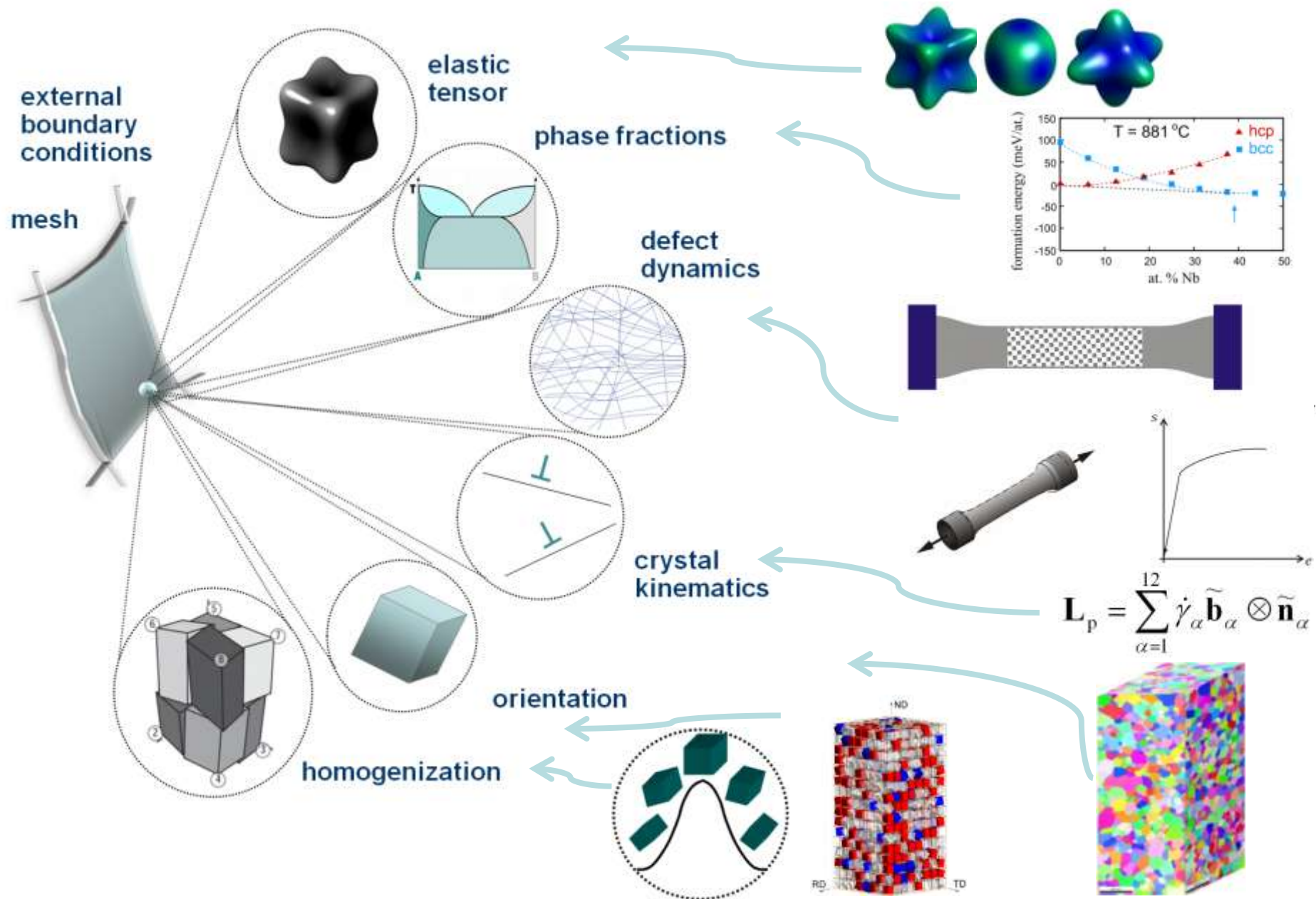


plastic spin from polar decomposition

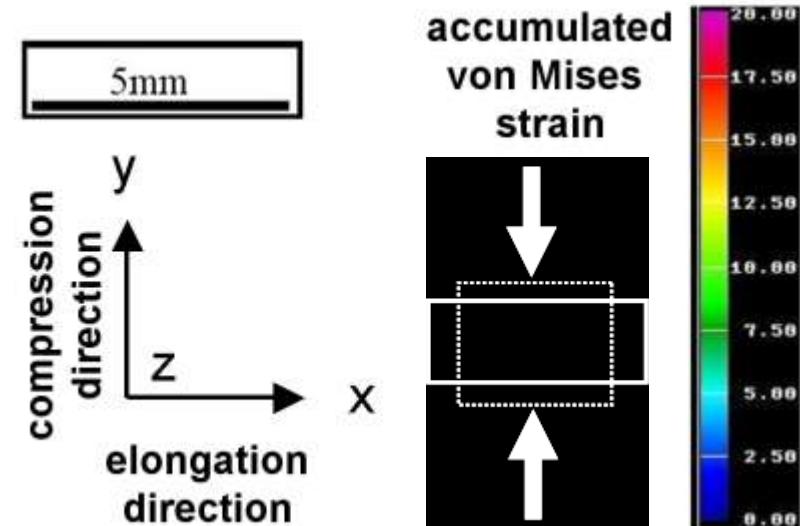
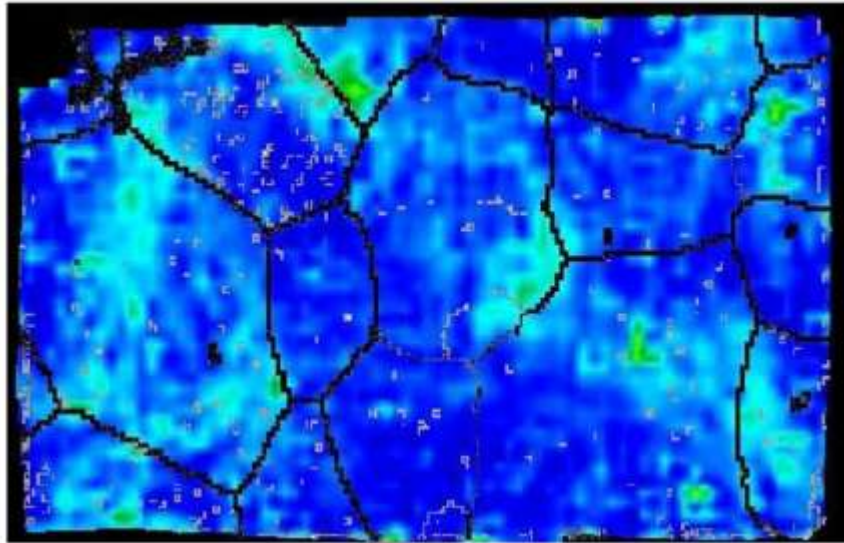
$$\dot{\omega}_{ij}^K = W_{ij}^K = \frac{1}{2} (\dot{u}_{i,j}^K - \dot{u}_{j,i}^K) = \sum_{s=1}^N m_{ij}^{\text{asym},s} \dot{\gamma}^s$$

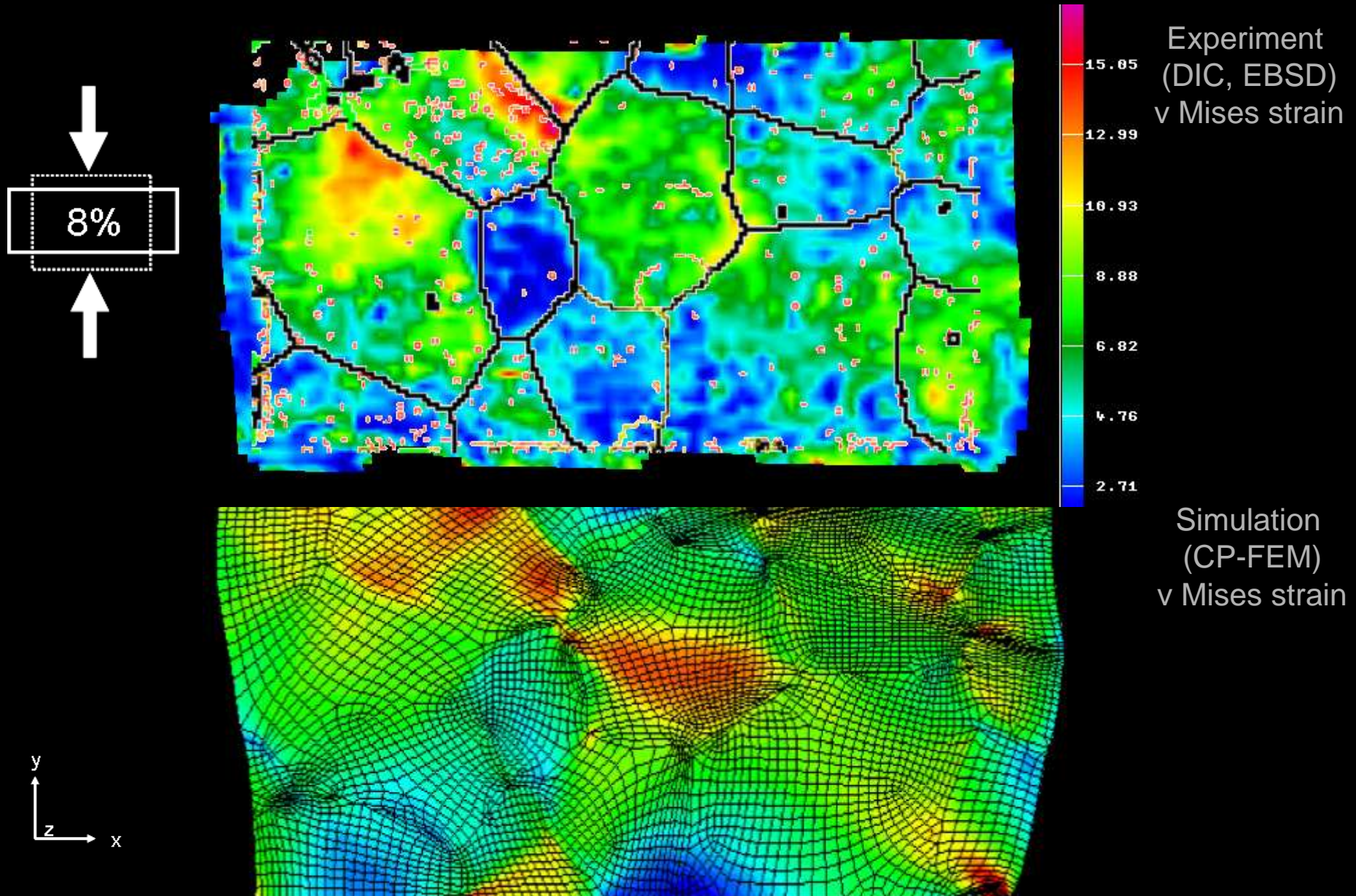


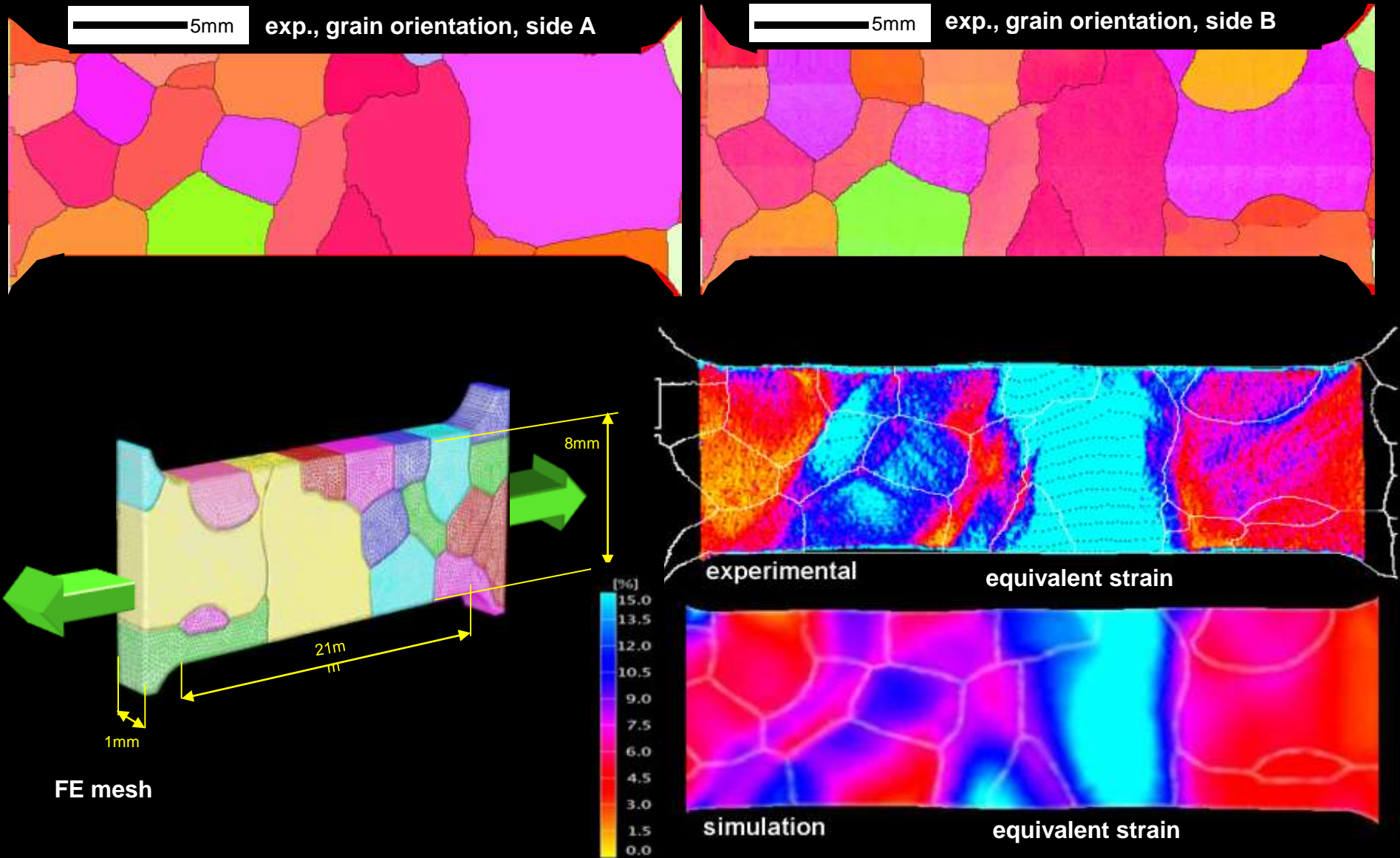
- **Examples**

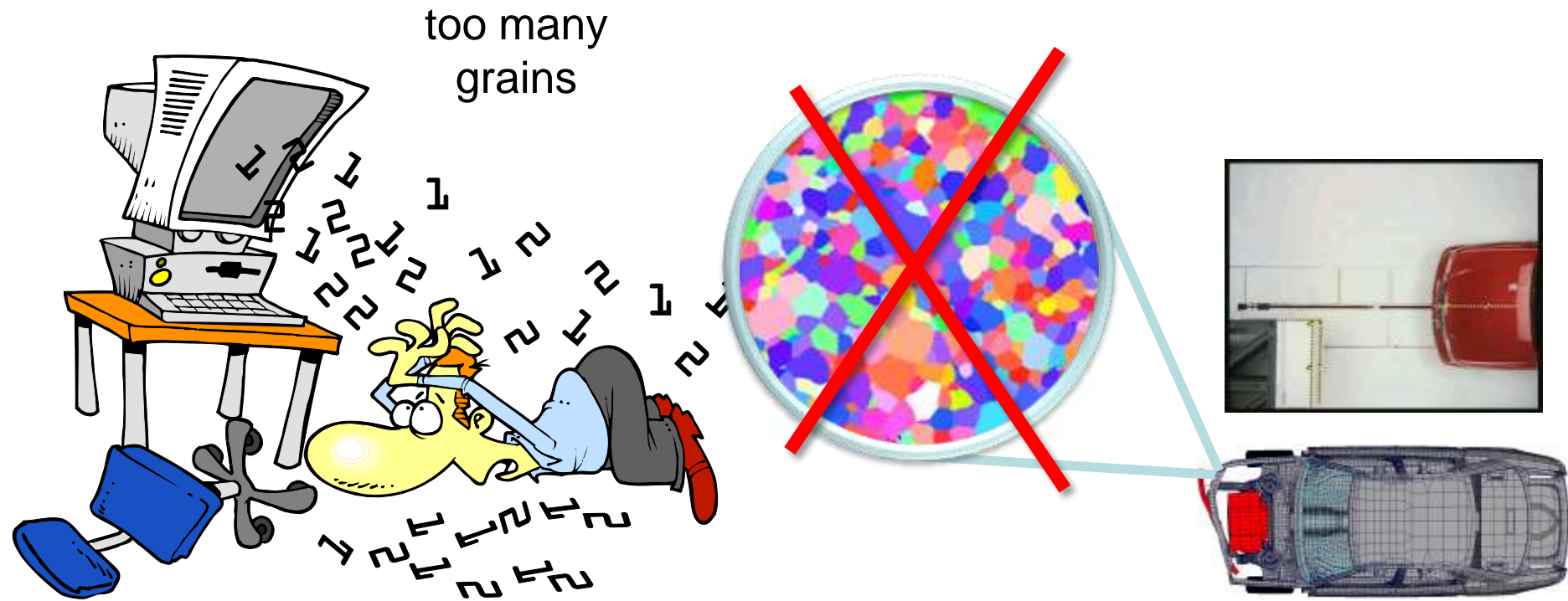


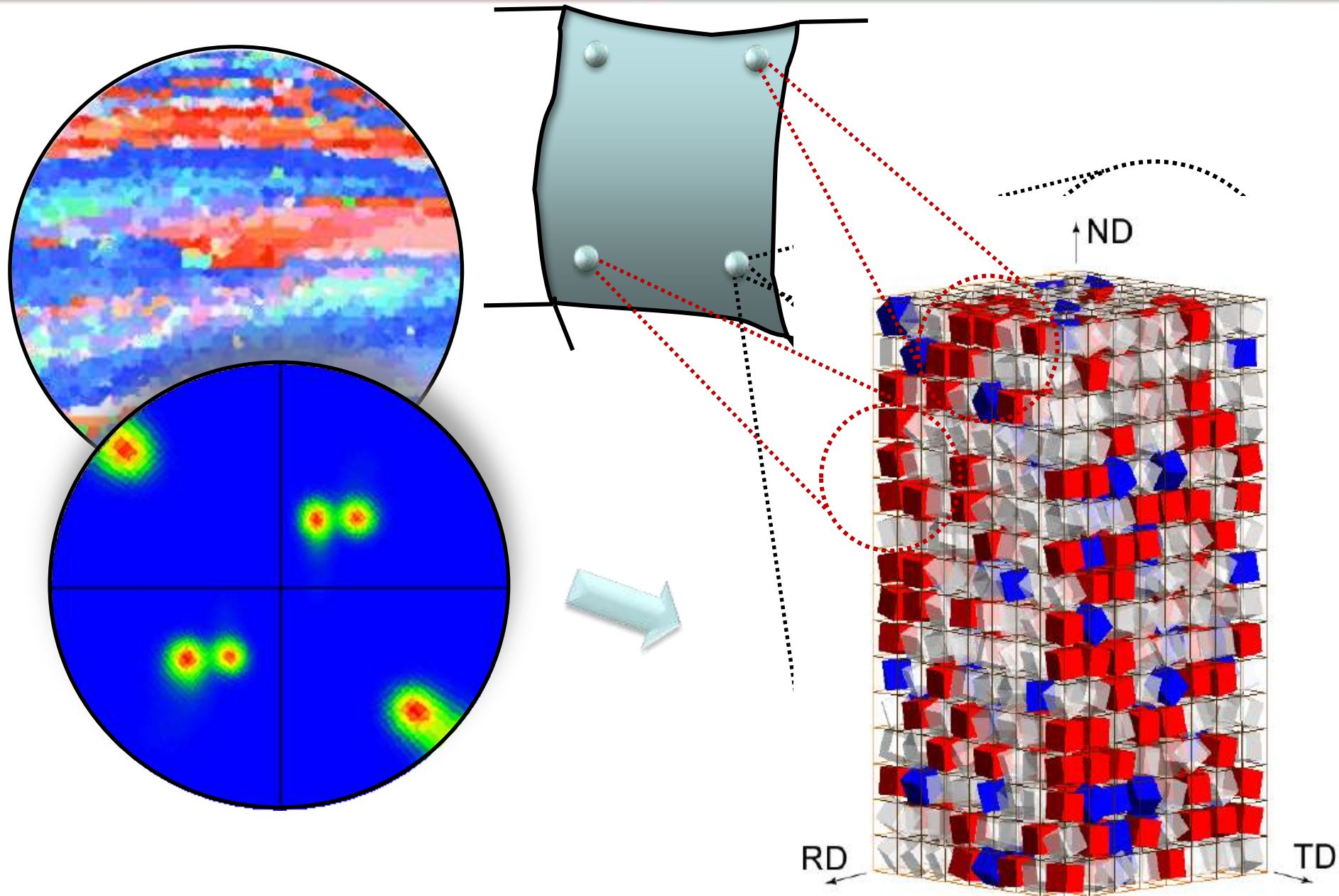
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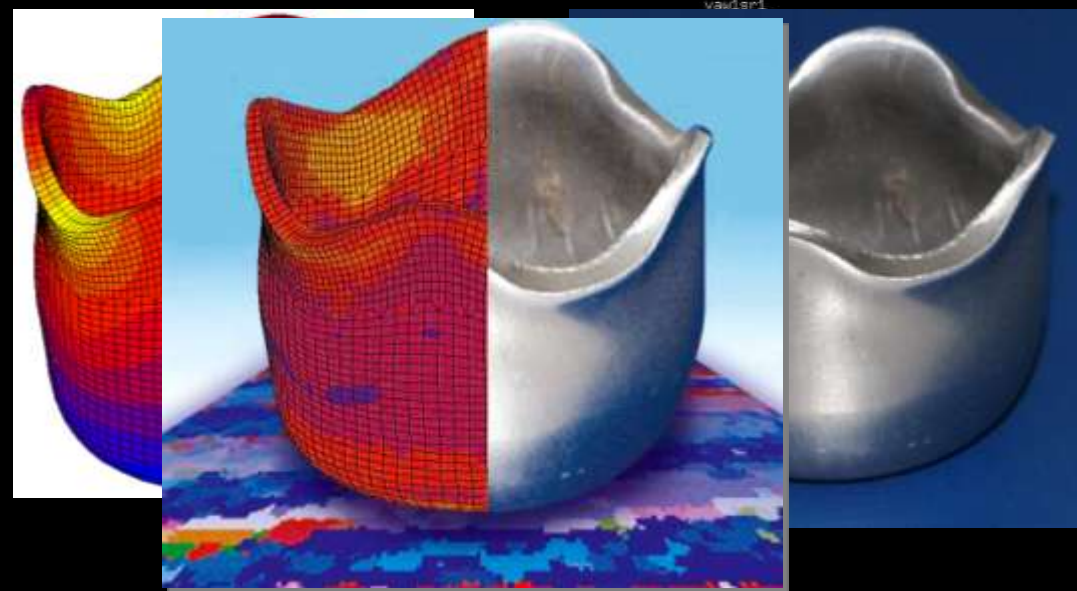
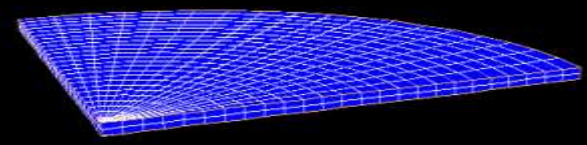
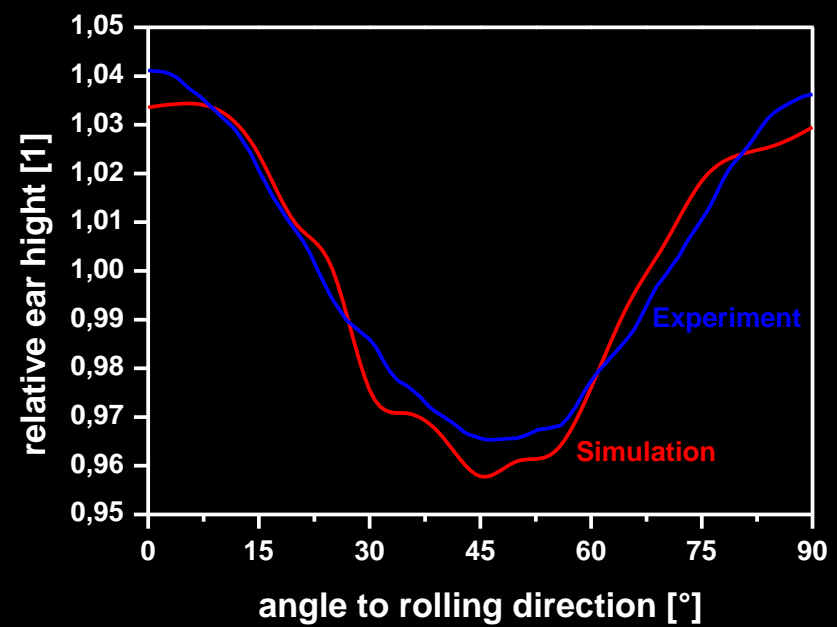


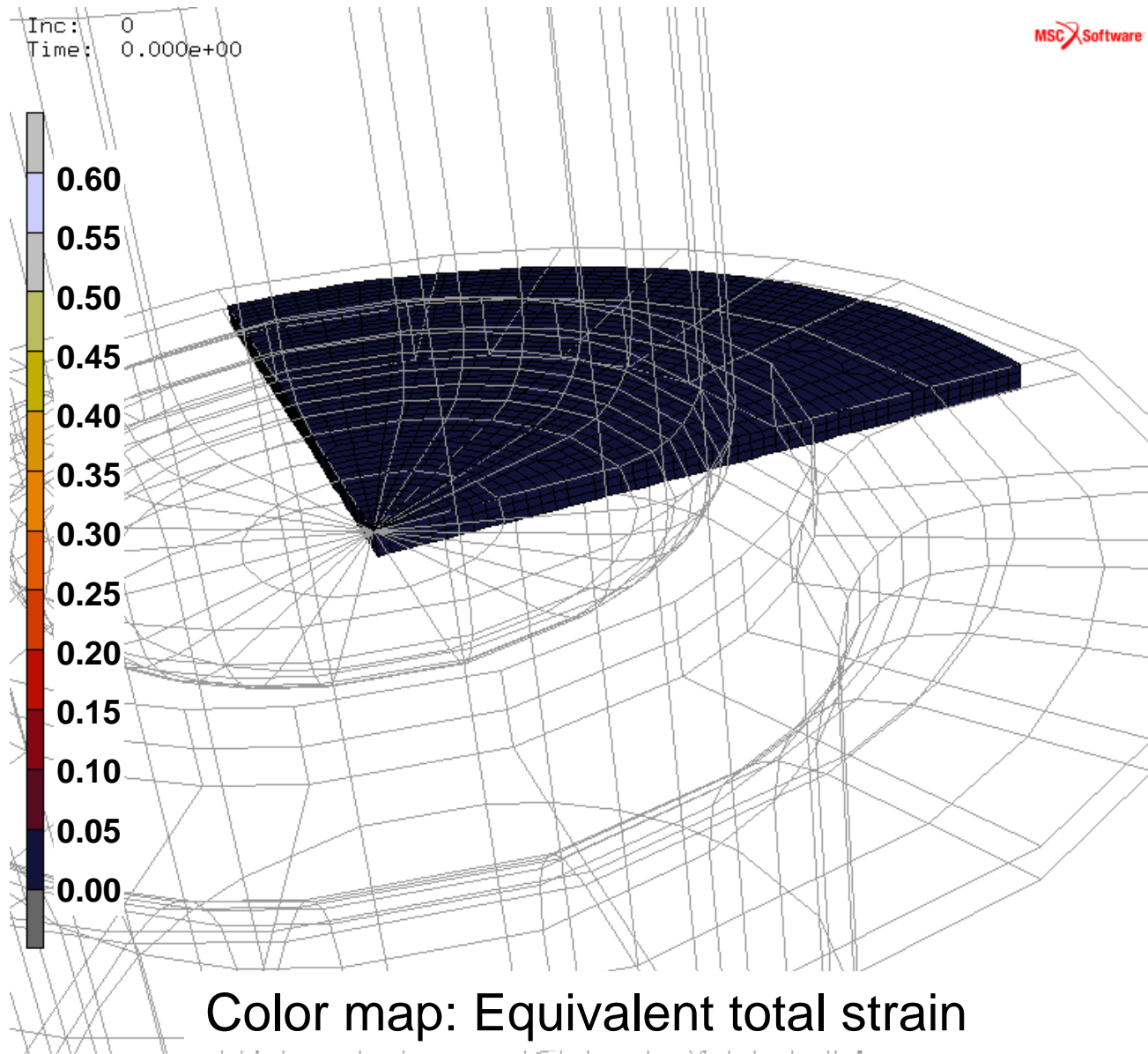


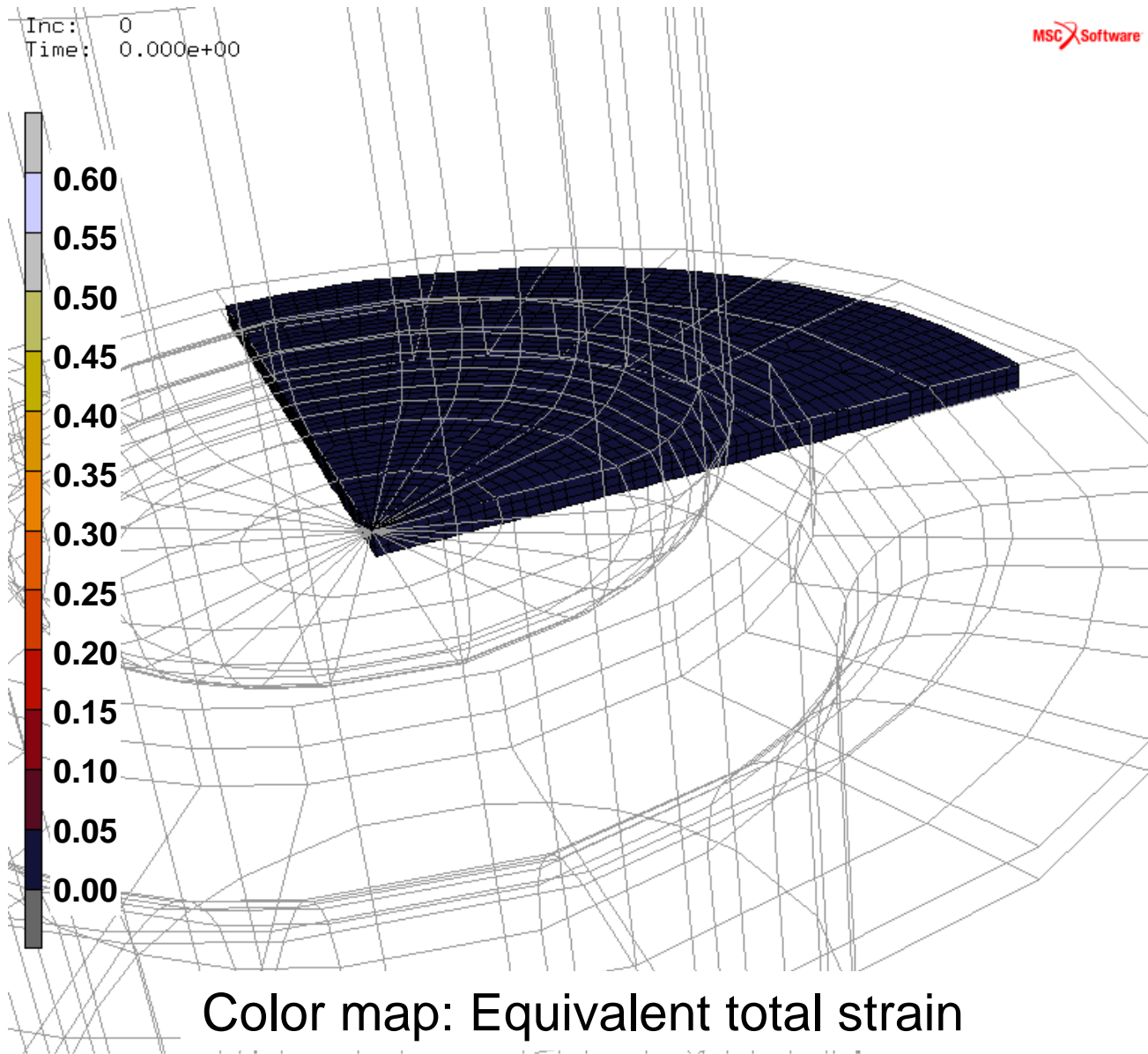




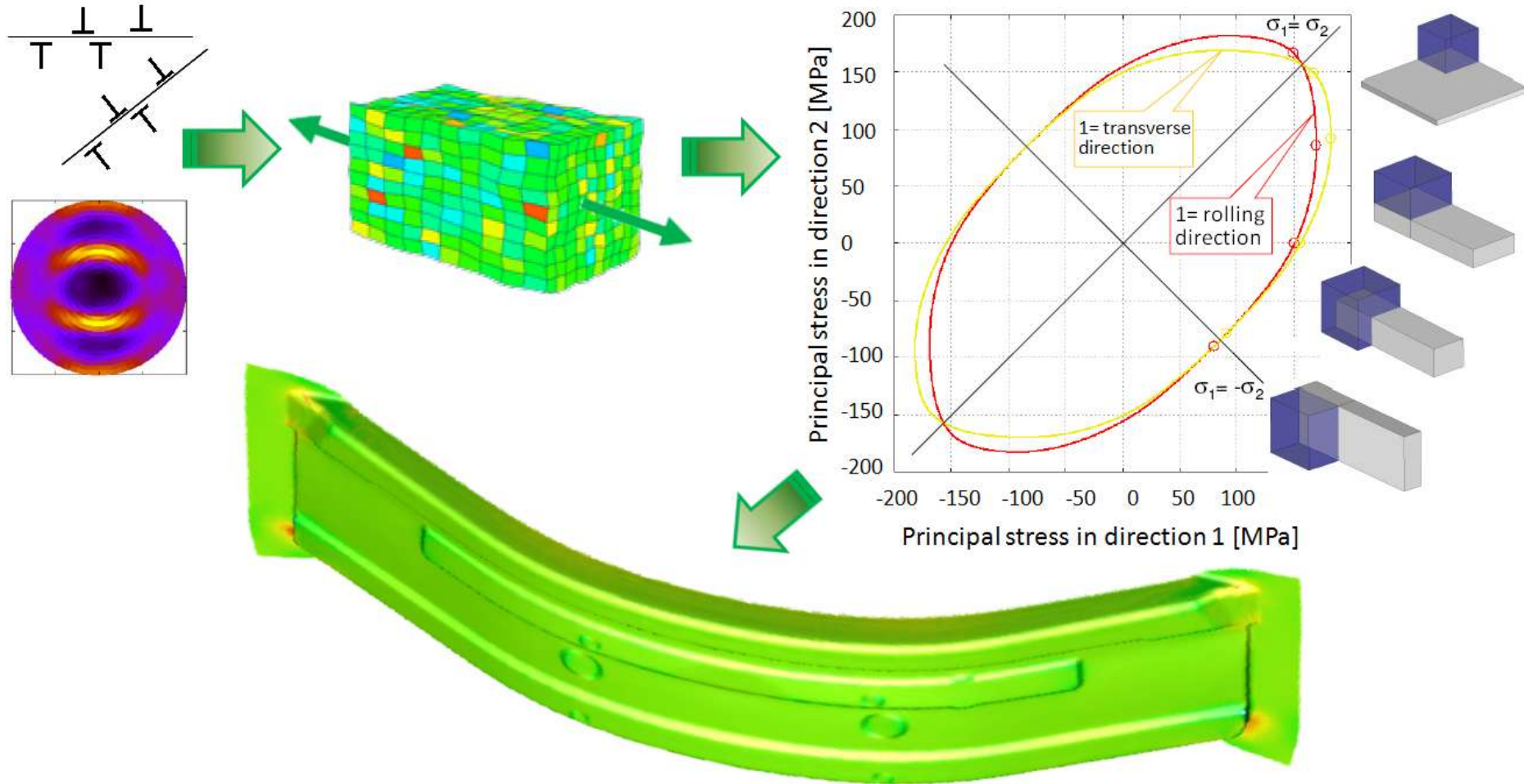








Numerical Laboratory: From CPFEM to yield surface (engineering)



DC04 study with Mercedes, Volkswagen, Audi, Inpro